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DISCOVERING THOUGHTS AND INVENTING FUTURE

HIGHLIGHTS

Electromagnetic Fuel Saver

Ethanol Emulsion

Multi-objective Optimisation

SWET Technique

Assembly Line

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Electromagnetic Fuel Saver for Enhanching The Performance of The Diesel Engine

By Houtman P. Siregar & Rufinus Nainggolan

Department of Mechatronics Engineering, Institute Technology of Indonesia

Abstract - This article is devoted to the production and testing of the performance of electromagnetic fuel saver. Purpose of the work is to analysis effect of varying of core of electromagnetic fuel saver to the performance of the internal combustion diesel engine. Materials for core of electromagnetic fuel saver are made of plain carbon steel and copper. Diameters of the wire winding, which is used in the research, are 0.25 mm and 0.35 mm. Speed of the engine, and number of coil which is coiled in the winding core of the fuel saver are chosen as the testing variables. The produced fuel saver is tested in the laboratory and on the road in the traffic jam condition and in the highway. Measured variables in the laboratory is the specific fuel consumption and measured variable for road testing is fuel consumption. From this work is obtained that the performance of the electromagnetic fuel saver which use copper core is better than the electromagnetic fuel saver which use steel core and permanent magnet.

Keywords : Electromagnetic fuel saver, specific fuel consumption, number of coil, core material, wire winding diameter.

GJRE-A Classification : FOR Code: 091305



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Electromagnetic Fuel Saver for Enhanching The Performance of The Diesel Engine

Houtman P. Siregar ^{α} & Rufinus Nainggolan ^{σ}

Abstract - This article is devoted to the production and testing of the performance of electromagnetic fuel saver. Purpose of the work is to analysis effect of varying of core of electromagnetic fuel saver to the performance of the internal combustion diesel engine. Materials for core of electromagnetic fuel saver are made of plain carbon steel and copper. Diameters of the wire winding, which is used in the research, are 0.25 mm and 0.35 mm. Speed of the engine, and number of coil which is coiled in the winding core of the fuel saver are chosen as the testing variables. The produced fuel saver is tested in the laboratory and on the road in the traffic jam condition and in the highway. Measured variables in the laboratory is the specific fuel consumption and measured variable for road testing is fuel consumption. From this work is obtained that the performance of the electromagnetic fuel saver which use copper core is better than the electromagnetic fuel saver which use steel core and permanent magnet.

Keywords : *Electromagnetic fuel saver, specific fuel consumption, number of coil, core material, wire winding diameter.*

I. INTRODUCTION

owadays for solving the crisis of energy in Indonesia, many works are done to search the alternative source of energy. Simultaneously the researcher tries to create the gadget which can save the fuel consumption for automobile.

Purpose of the work is to produce and analysis the performance of the electromagnetic fuel saver for automotive diesel engine and to analysis effect of the change of the core of electromagnetic fuel saver to the performance of the diesel engine.

The fuel saver which is based on permanent magnet has sold in the market and its performance has tested [4, 5]. In comparison to the former fuel saver, in the considered work is produced fuel saver which is based on electromagnetic induction. The considered work is the continuation of former works [1, 2, 3].

II. Working Theory Of The Electromagnetic Fuel Saver

The combustion engine vehicle efficiency is about 9 %. This means that our car consume more

energy than it converts in to movement. In other words, we pay more energy than we use. In the article we describe method and gadget for improving the combustion of fuel in the internal combustion diesel engine of automobiles where the fuel employed is liquid [4, 5].

Applying a magnetic field to ionizing fuel to be fed to combustion devices we can ensure more complete combustion, obtaining a maximization of the fuel economy, improving the fuel efficiency and reducing polluting emissions. The fuel is subject to the lines of forces from electromagnetic magnet mounted on fuel inlet lines. Most fuels for internal combustion engines are liquid. But liquid fuels don't combust till they are vaporized and mixed with air. Currently regulated gas emissions from motor vehicles are unburned hydrocarbon (HC), carbon monoxide (CO), and oxides of nitrogen (NOx).

Fuel mainly consists hydrocarbons. of Groupings of hydrocarbons, when flowing through a magnetic field, change their orientations of magnetization in a direction opposite to that of the magnetic field. The molecules of hydrocarbon change their configuration. At the same time intermolecular force is considerably reduced or depressed. These mechanisms are believed to help to disperse oil particles and to become finely divided. The resultant conditioned fuel electromagnetized burns more completely, producing higher engine output, better fuel economy, more power and most importantly reduces the amount of hydrocarbons, carbon monoxide and oxides of nitrogen in the exhaust. Another benefits if these devices is that magnetically charged fuel molecules with opposite polarities dissolve carbon build-up in carburettor jets, fuel injectors, and combustion chambers help to clean up the engine and maintain the clean condition.

III. METHODOLOGY

In figure 1 is shown flowchart of the considered work. First of all it is designed the fuel saver which is based on electromagnetic and then it is produced according to the determined specification. Speed of the engine, diameter of the wire winding, core materials, and number of coil of winding of fuel saver are chosen as the testing variables. The performance of fuel saver, which has produced, is tested in the laboratory of the

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internal combustion engine rig. Performance of the produced fuel saver which is installed in the fuel line of internal combustion engine rig is compared to the performance of the standard internal combustion engine rig (without installing fuel saver in the fuel line). Performance of the produced fuel saver is compared to the performance of the permanent magnet fuel saver, which has sold in the market. And then results of the work are discussed and finally the conclusions are drawn.

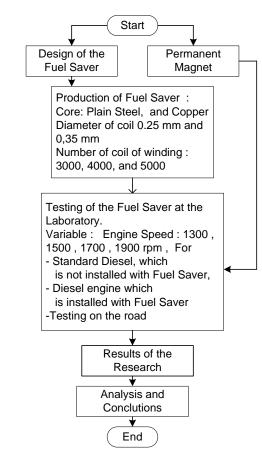


Fig. 1 : Flowchart of the proposed research

IV. Results and Discussion

In the considered work, terminology of fuel saving means fuel consumption of fuel saver which is based on electromagnetic induction minus fuel consumption of diesel engine which is not installed with fuel saver (standard). Difference of the fuel consumption between e standard diesel engine and diesel engine which is installed with fuel saver may be positive and negative value. Negative value means more consume fuel and positive value means less consume fuel than standard diesel engine.

In the figures use some abbreviations. The meanings of each abbreviation are as follows. Cu-35/5000 means that the electromagnetic fuel saver use core of copper, diameter of wire 0.35 mm and number

tion engine turns. PM means permanent magnet. fuel line). In the figure 2 up to figure 6 are drawn results of propared to laboratory test of diesel engine. And in the figure 7 is

laboratory test of diesel engine. And in the figure 7 is drawn result of the road test for the best gadget and permanent magnet.

of coil 5000 turns. St-25/5000 means that the

electromagnetic fuel saver use core of plain carbon

steel, diameter of wire 0.25 mm and number of coil 5000

In the figure 2 is drawn results of laboratory test for diesel engine which relate the percentage of specific fuel consumption (SFC) saving for average speed of rotation of engine for electromagnetic fuel saver, which use diameter of wire 0.25 mm and steel core versus number of winding. As it is shown in figure 2 that electromagnetic fuel saver which use number of coil or winding 5000 turns is better in fuel saving than the fuel saver which uses number of coil 3000 and 4000 turns. Electromagnetic fuel saver which uses number of coil or winding 5000 can save specific fuel consumption 9.80 %. For number of winding 3000 and 4000 turns can save SFC, respectively, 7.55% and 4.76%.

In the figure 3 is drawn results of laboratory test for diesel engine which relate the percentage of specific fuel consumption (SFC) saving for average speed of rotation of engine for electromagnetic fuel saver which uses diameter of wire 0.35 mm and steel core versus number of winding. As it is shown in figure 3 that electromagnetic fuel saver which uses number of coil or winding 3000 turns is better in fuel saving than the fuel saver which uses number of coil 4000 and 5000 turns. Electromagnetic fuel saver which uses number of winding 3000 turns can save specific fuel consumption 6.77 %. For number of winding 4000 and 5000 turns can save SFC, respectively, 6.14% and 5.93%.

In the figure 4 is drawn results of laboratory test for diesel engine which relate the percentage of specific fuel consumption (SFC) saving for average speed of rotation of engine for electromagnetic fuel saver which uses diameter of wire 0.25 mm and copper core versus number of winding. As it is shown in figure 4 that electromagnetic fuel saver which uses number of coil or winding 5000 turns is better in fuel saving than the fuel saver which use number of coil 3000 and 4000 turns. Electromagnetic fuel saver which uses number of winding 5000 can save specific fuel consumption 9.54 %. For number of winding 3000 and 4000 turns can save SFC, respectively, 4.77% and 7.95%.

In the figure 5 is drawn results of laboratory test for diesel engine which relate the percentage of specific fuel consumption (SFC) saving for average speed of rotation of engine for electromagnetic fuel saver which uses diameter of wire 0.35 mm and copper core versus number of winding. As it is shown in figure 5 that electromagnetic fuel saver which uses number of coil or winding 5000 turns is better in fuel saving than the fuel saver which uses number of coil 3000 and 4000 turns. Electromagnetic fuel saver which uses number of winding 5000 turns can save specific fuel consumption 11.53 %. For number of winding 3000 and 4000 turns can save SFC, respectively, 6.76% and 8.35%.

In the figure 6 is drawn graph of comparison of optimal percentage of specific fuel consumption (SFC) saving for average speed of rotation of engine versus type of gadget. As it is shown in figure 6 that gadget which uses copper core is better in fuel saving than the gadget which uses steel core and permanent magnet. Once more the electromagnetic fuel saver is better in fuel saving than the permanent magnet. As shown in figure 6 that the electromagnetic fuel saver which uses copper core, number of coil 5000, and diameter of wire winding 0.35 mm can save specific fuel consumption 11.53 %. Electromagnetic fuel saver which uses steel core, number of coil 5000 turns, and diameter of wire winding 0.25 mm can save specific fuel consumption 9.80 %. But gadget which uses permanent magnet just can save specific fuel consumption 8.53%.

In the figure 7 is drawn results of road test for diesel engine which relate the percentage of fuel consumption saving for optimal electromagnetic fuel saver and permanent magnet. It is seen from figure 7 that the electromagnetic fuel saver which uses copper core, number of coil 5000 turns, and diameter of wire winding 0.35 mm can save fuel consumption 31.50 %. Electromagnetic fuel saver which uses steel core, number of coil 5000 turns, and diameter of wire winding 0.25 mm can save fuel consumption 28.40 %. But gadget which uses permanent magnet just can save specific fuel consumption 25.30%. In this case, the best gadget is the electromagnetic fuel saver which uses copper core.

As we know that the more the number of winding the stronger the magnetic force. So the stronger magnetic force will give stronger induction to solar fuel and resulting in complete combustion process. So the cluster of solar fuel is fully oriented and the configuration of fuel is changed. At the same time intermolecular force is considerably reduced or depressed. These mechanisms are believed to help to disperse oil particles in this case and to become finely divided and make easy to mix compressed air with solar fuel and resulting in complete combustion process. The resultant conditioned fuel burns more completely, producing higher engine output, better fuel economy, and more power.

In the work, electromagnetic fuel saver which uses copper core is better than electromagnetic fuel saver which uses steel core and permanent magnet. It seems that the copper core is more effective in inducing magnetic force than steel core. This phenomenon is an anomaly in this work, because according to the theory of magnet that ferrous material (steel) is better in inducing magnetic force than nonferrous material (copper). In this case, it seems that the strength of the magnetic force of electromagnetic fuel saver is stronger than permanent magnet fuel saver. So, the stronger magnetic force results in more complete combustion process than permanent magnet fuel saver.

So the produced electromagnetic fuel saver can significantly save consumption of fuel. Saving the fuel consumption means that the heat of combustion which is released to the atmosfere diminishing. Consequently the produced fuel saver can reduce and overcoming global warming.

In conclusion we have succeeded to produce good prototype of electromagnetic fuel saver and it has good performance. The produced fuel saver can significantly save fuel consumption for diesel engine. In addition the proposed fuel saver can improve quality of environmental and overcoming global warming.

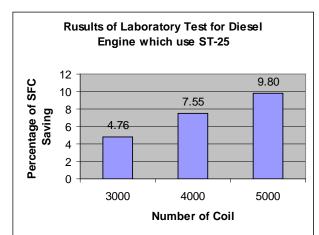


Fig. 2: Results of laboratory test for steel core and diameter of wire 0.25 mm.

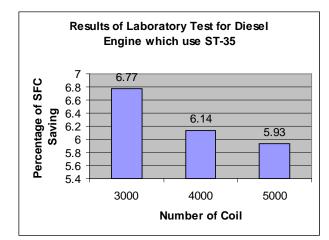


Fig. 3 : Results of laboratory test for steel core and diameter of wire 0.35 mm.

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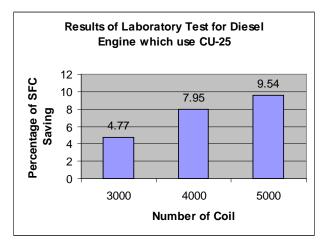


Fig. 4 : Results of laboratory test for copper core and diameter of wire 0.25 mm.

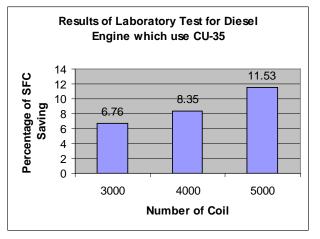


Fig. 5: Results of laboratory test for copper core and diameter of wire 0.35 mm.

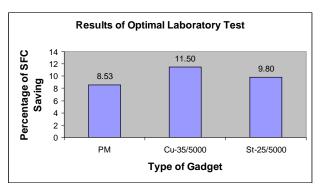


Fig. 6 : Comparison of the optimal saving in relation to the type of gadget

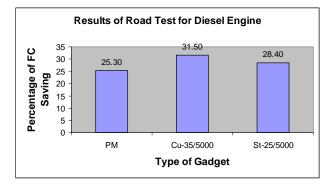


Fig. 7: Results of road test versus type of gadget

V. Conclusions

- 1. The considered work has succeeded to produce fuel saver which is based on electromagnetic induction for saving the fuel consumption of diesel engine.
- 2. Wire diameter and number of winding of the produced fuel saver effect fuel consumption of diesel engine.
- 3. Laboratory testing shows that the produced fuel saver can save specific fuel consumption about 11.53 % which use diameter of wire 0.35 mm and number of winding 5000 turns, for copper core.
- 4. Road testing shows that the produced fuel saver can save fuel consumption about 31.53% which uses diameter of wire 0.35 mm and number of winding 5000 turns, for copper core.

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Weighted Sum Method for Multi-Objective Optimisation for Aluminium Metal Casting

By Kuldeepak & Ravi K. Sharma

Jaypee University of Engineering & Technology, Guna.

Abstract - An optimisation technique for design of gating system parameters of a cylindrical aluminium casting based on the Taguchi method is proposed in this paper. The various gating systems for a casting model of aluminium are designed. Mould filling and solidification processes of the Aluminium casting were simulated with the PROCAST, AUTOCAST, and MAGMASOFT etc. The simulation results indicated that gating system parameters significantly affect the quality of the Aluminium casting. In an effort to obtain the optimal process parameters of gating system, an orthogonal array, the signal-to- noise (S/N) ratio, and analysis of variance (ANOVA) were used to analyze the effect of various gating designs on cavity filling and casting quality using a weighting method.

Keywords : Taguchi method, Computational simulation, Optimisation, Gating system, Aluminium casting. GJRE-A Classification : FOR Code: 091307



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Kuldeepak^a & Ravi K. Sharma^o

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Keywords : Taguchi method, Computational simulation, Optimisation, Gating system, Aluminium casting.

I. INTRODUCTION

large number of experimental investigations linking gating parameters with casting quality have been carried out by researchers and foundry engineers over the past few decades (Campbell, 2003; Yang et al., 2000). Since all liquid melt required filling up the casting cavity needs to be introduced through the gating system, it has been long recognized that gating system design plays one of the key elements in casting guality. Although there are general casting design guidelines and empirical equations for the gating ratio, pouring time, and gating system dimensions, the variations in casting parameters chosen by different researchers have led to significant variations in empirical guidelines (Campbell, 1998). This also forces foundries to carry out a number of trial and error runs and create guidelines based on their own experience. Traditionally, gating system design is performed by casting process engineers based on their individual knowledge and experience. In many cases, the gating system design is not optimal and often based on trial and error practice. This leads to not only a long casting development cycle but also a low reliability of casting design due to variation of individual knowledge and experience.

The use of a good gating system is even more important if a casting is produced by a gravity process. Since oxide formation is instantaneous in Aluminium, the design of gating system plays more important role on minimising the entrance of oxides on the surface of the molten metal into the casting and also to prevent turbulence in the metal stream caused by excessive velocities of the molten metal, free-falling of the stream while passing from one level to another, vortices formed, or abrupt changes in the flow direction (Hu and Yu, 2002; Green and Campbell, 1994). Therefore, Aluminium castings are vulnerable to certain defects such as porosity, oxide inclusions, which are known to be attributed to the faulty design of gating system with incorrect mould filling. In order to achieve a good gating system, it is necessary to start from fundamental hydraulic principles. Computer-aided casting design and simulation gives a much better and faster insight for optimising the feeder and gating design of castings (B.Ravi, 2009).

The first research showing an effect to apply a numerical optimisation methodology to optimise a gating system is due to Bradley and Heinemann in 1993 (Bradley and Heinemann, 1993). They used simple hydraulic models to simulate the optimisation of gating during filling of moulds. In 1997, MacDavid and Dantzig used a mathematical development addressing the design sensitivity within two-dimensional mould geometry. By the end of the 1990s, the computer modeling enabled visualization of mould filling to be carried out cost-effectively in casting design and optimisation of gating system. Numerical simulators based on FDM and FEM methods provide powerful means of analyzing various phenomena occurring during the casting process (McDavid and Dantzig, 1998a.b).

Dr. Genichi Taguchi has introduced several new statistical tools and concepts of quality improvement that depend heavily on the statistical theory of experimental design (Taguchi, 1998; Byrne and Taguchi, 1987). Some applications of Taguchi's methods in the foundry industry have shown that the variation in casting quality caused by uncontrollable process variables can be minimized. The casting process has a large number of parameters that may affect the quality of castings. Some of these parameters are controllable while others are noise factors. Therefore, the optimisation of casting

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parameters using the Taguchi method is the better choice for rapid casting quality improvement.

The purpose of this paper is to demonstrate the application of numerical optimisation how techniques can be used to develop an effective optimisation process for gating system design. Mould filling and solidification processes of the castings can be the PROCAST. AUTOCAST. simulated with MAGMASOFT etc. The simulation results indicated that gating system parameters significantly affect the casting quality. This virtual approach and optimisation technique can be applied to the foundry industry, which is evidently superior to typical trial-and-error approaches.

II. Design of Experiment Based on the Taguchi Method

A large number of experiments have to be carried out when the number of the process parameters increases. To solve this task, the Taguchi method uses a special design of orthogonal arrays to study the entire parameter space with a small number of experiments only. The S/N ratio for each level of process parameters is computed based on the S/N analysis. Regardless of the category of the performance characteristic, the larger S/N ratio corresponds to the better performance characteristic. Therefore, the optimal level of the process parameters is the level with the highest S/N ratio. Furthermore, a statistical analysis of variance (ANOVA) is performed to see which process parameters are statistically significant. With the S/N and ANOVA analyses, the optimal combination of the process parameters can be predicted. Finally, a confirmation experiment is conducted to verify the optimal process parameters obtained from the parameter design. In this paper, the gating parameter design by the Taguchi method is adopted to obtain optimal gating system in aluminium casting. The experimental layout for the four gating parameters used L9 orthogonal array.

III. GATING SYSTEM PARAMETERS AND OBJECTIVES DESIGN

The objective of the parameter design is to optimise (D.C. Montgomery, 1991) the settings of the process parameter values for improving performance characteristics and to identify the product parameter values under the optimal process parameter values. In addition, it is expected that the optimal process parameter values obtained from the parameter design are insensitive to the variation of environmental conditions and other noise factors. A cubical housing model was used as the test sand casting to understand the numerical optimisation. The three-dimensional CAD model of the test casting is shown in Fig. 1. The casting material is defined Aluminium. The process used for preparing mould cavity is sand casting. A pouring basin and tapered sprue were used and metal was introduced into the casting cavity through one runner and one ingate of rectangular cross-section. Single blind riser is used at top of the housing model.

Since the lower and wide geometry help to reduce the metal velocity and get a smooth flow into mould, the parameter ranges of the design variables. In this work gating parameters like runner height, runner width, ingate height and ingate width were changed. Remaining parameters kept constant for all the experiments. In this study, in order to evaluate the sound casting comprehensively, the optimisation criteria for the housing casting sample were defined as:(1) casting quality, and (2) casting cost. The molten metal filling velocity and casting shrinkage

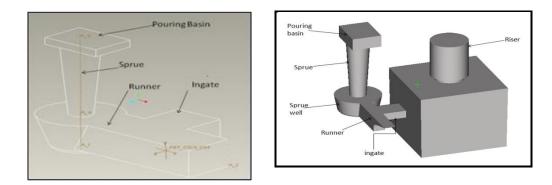


Fig.1 : 3-D Model of gating system

porosity can demonstrate the casting quality; and the casting cost characteristic can be indicated by product yield. These three characteristics acting as multiple performance objectives for evaluating different gating system designs are defined as the Eqs. (1) - (3):

$$Velocit \dot{\mathbf{y}} \mathbf{v}) = \sqrt{\mathbf{v}_{\mathbf{x}}^2 + \mathbf{v}_{\mathbf{y}}^2 + \mathbf{v}_{\mathbf{z}}^2} \tag{1}$$

ShrinkagePorosity(%) =
$$\frac{\text{pores}}{\text{vol}_{cast}}$$
 (2)

Casting Yield (%)= $\frac{\text{weight}_{cast}}{\text{weight}_{cast} + \text{weight}_{gating+risersystem}}$ (3)

Where v_x , v_y , v_z are three component of vector velocity.

IV. Analysis of the S/N Ratio With Multiple-Performance Characteristics

The Taguchi method uses signal-to-noise (S/N) ratio instead of the average value to interpret the trial results data into a value for the evaluation characteristic in the optimum setting analysis. This is because signal-to-noise ratio can reflect both the average and the variation of the quality characteristics. S/N ratio can be defined as Eq. (4)

$$\eta = -10\log(MSD) \tag{4}$$

Where MSD is the mean-square deviation for the output characteristic. The MSD for the higher-thebetter quality characteristic can be expressed as Eq. (5)

$$MSD = \frac{1}{n} \sum_{i=1}^{n} \frac{1}{T_i^2}$$
(5)

On the other hand, the lower-the-better quality characteristic for filling velocity and shrinkage porosity also is being taken for obtaining the optimal casting quality. The MSD for the lower-the-better quality characteristic can be expressed as Eq. (6):

$$M SD = \frac{1}{n} \sum_{i=1}^{n} S_i^2$$
 (6)

Where n is the total number of tests in a trial and Ti is the value of product yield and Si is the value of filling velocity and shrinkage porosity at the ith test.

The proposition for the optimisation of a gating system with multiple performance characteristics (three objective) using a weighting method is defined as

multi-response S/N ratio in the jth test. η_{ji} is the ith single response S/N ratio for the jth test. w_i is the weighting factor in the ith performance characteristics. The

objective function was formulated according to the

where
$$X = \begin{bmatrix} n_{1C} \\ n_{2C} \\ . \\ . \\ n_{9C} \end{bmatrix}$$
; $Y = \begin{bmatrix} n_{11} & n_{12} & n_{13} \\ n_{21} & n_{22} & n_{23} \\ . \\ . \\ n_{91} & n_{92} & n_{93} \end{bmatrix}$; $Z = \begin{bmatrix} w_1 \\ w_2 \\ w_3 \end{bmatrix}$ (8)

$$\& \sum_{i=1}^{3} W_i = 1 \tag{9}$$

Assumption is using L9 orthogonal array. w₁ is the factor of product yield; w₂ is the factor of shrinkage porosity; w₃ is the factor of filling velocity; η_{ic} is the

Maximize
$$f(X) = \eta_{Yield} w_1 + \eta_{Porosity} w_2 + \eta_{Velocity} w_3$$
 (10)

previous optimisation criteria:

Where w_1 , w_2 , w_3 are the weighting factors of S/N ratio for yield, porosity and velocity, respectively.

V. ANALYSIS OF VARIANCE (ANOVA)

The purpose of the ANOVA is to investigate which of the process parameters significantly affect the performance characteristics. This is accomplished by separating the total variability of the multi-response S/N ratios, which is measured by the sum of the squared deviations from the total mean of the multi-response S/N ratio, into contributions by each of the process parameters and the error. The five connective parameter symbols can be calculated as Eqs. (11) and (12)

$$SS_{p} = \sum_{i=1}^{m} \frac{(S\eta_{jc})^{2}}{t} - \frac{1}{m} \left[\sum_{i=1}^{m} \eta_{ic} \right]^{2}$$
(11)

$$SS_{T} = \sum_{i=1}^{m} \eta_{jc}^{2} - \frac{1}{m} \left[\sum_{i=1}^{m} \eta_{ic} \right]^{2}$$
(12)

$$V_{\rm P} = \frac{\rm SS_{\rm P}}{\rm D_{\rm P}} \times 100 \tag{13}$$

$$SS_{P}^{'} = SS_{p} - D_{p}V_{e}$$
(14)

$$P_{p} = \frac{SS_{P}}{SS_{T}} \times 100 \tag{15}$$

Where *m* is the number of the tests (*m*= 9). *p* represents one of the tested parameters, *j* is the level number of this parameter *p*, *t* is the repetition of each level of the parameter *p*, and $S \eta_{jc}$ is sum of the multi-response S/N ratio involving this parameter *p* and level *j*. The total degree of freedom is $D_{T} = m$ -1, for the tested parameter, $D_{p} = t$ -1, V_{p} is the variance, SS'_p is the corrected sum of squares and P is the contribution of reach individual factor.

VI. Computational Experiment

Simulation of the mould filling and solidification process required geometrical information for the casting, the gating system and the sand mould. Solid CAD models were created using the Pro-E wildfire 4.0 software of PTC (Parametric Technology Corporation) 2012

(7)

and converted into PARASOLID (.x t) file. Then the PARASOLID (.x t) file directly imported to ProCAST 2009.1 for simulation. Once the meshed geometry is established, the casting process design parameters, then the initial boundary conditions are defined according to the actual experimental condition for doing simulation. The boundary condition should be defined for all simulation experiments. With the ViewCast module the fluid flow in the cavity and solidification during the casting process were analyzed and potential defects were predicted. The ViewCast can only view the fluid flow and temperature field patterns in the cavity during the casting process and predict the potential defects graphically. in order to generate the corresponding simulation result data file according to the specific 3D coordinate in the casting model based on FEM model node number VisualCast module (ProCAST 2009.1) was employed to study to predict the filling velocity and shrinkage porosity numerically.

VII. Result and Discussion

Based on simulation result the value of shrinkage porosity & filling velocity are for different 9 sets of gating system. Casting yield is calculated with eq. (2). Now S/N ratio is calculated for all values of the three performance characteristics with at the help of Eq. (4)-(6). The three combination of weighting factor were selected in this study of multi-response S/N ratio calculated with the help of Eq. (7)-(9). Now to calculate the response of each factor to its individual level was calculated by averaging the S/N ratios of all experiments at each for each factor.

For case 1, the order of the performance characteristics is the product yield ($w_1 = 0.5$), the shrinkage porosity ($w_2 = 0.2$), and the filling velocity ($w_3 = 0.3$). For case 2, the order of the performance characteristics is the product yield ($w_1 = 0.3$), the shrinkage porosity ($w_2 = 0.5$), and the filling velocity ($w_3 = 0.2$).Finally, for case 3, the order of the performance characteristics is the product yield ($w_1 = 0.3$), the shrinkage porosity ($w_2 = 0.5$), and the filling velocity ($w_3 = 0.2$).Finally, for case 3, the order of the performance characteristics is the product yield ($w_1 = 0.1$), the shrinkage porosity ($w_2 = 0.2$), and the filling velocity ($w_3 = 0.7$). Figs. 6.1–6.3 show the multiresponse S/N ratio for case 1–3, respectively. The multiresponse S/N ratio for each level of the gating system parameter is calculated based on Eqs. (7) – (9).

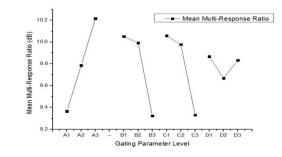


Fig. 2: Multi-response S/N ratio graph for case 1 $(w_1 = 0.5, w_2 = 0.2, w_3 = 0.3)$

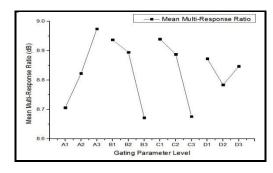


Fig. 3 : Multi-response S/N ratio graph four case 2 $(w_1 = 0.3, w_2 = 0.5, w_3 = 0.2)$

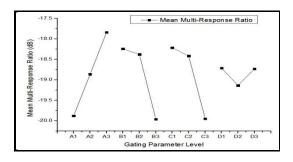


Fig. 4 : Multi-response S/N ratio graph for case 3 $(w_1 = 0.1, w_2 = 0.2, w_3 = 0.7)$

As shown in previous equations, regardless of the lower-the-better or the higher-the-better performance characteristics, the larger the multi-response S/N ratio the smaller is the variance of performance around the objective value. For case 1, case 2 and case 3 the A3B1C1D1 is the maximum multi-response S/N ratio. The larger ingate height will help to lower the ingate filling velocity characteristic which has largest weighting factor for performance characteristics of all three cases. However, the relative important factor among the gating parameters for the multiple performance characteristics still need to be investigated by using the analysis of variance (ANOVA) method which can conduct the factor contribution more accurately.

VIII. THE FACTOR CONTRIBUTION WITH DIFFERENT COMBINATION OF WEIGHTING FACTORS

The purpose of the ANOVA is to investigate which of the process parameters significantly affect the performance characteristics. This is accomplished by separating the total variability of the multi-response S/N ratios, which is measured by the sum of the squared deviations from the total mean of the multi-response S/N ratio, into contributions by each of the process parameters and the error. First, the total sum of the squared deviations SST from the total mean of the multi-response S/N ratio η_{ic} can be calculated by Eq. (11) – (15). Table (6.7) - (6.9) shows the results of ANOVA for case 1 to case 3. It can be found that the contribution of Ingate height and Ingate width is more than other

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Runner factors. The sequence of the four factors affecting the casting quality is the Ingate height, the Ingate width, the Runner height, and the Runner width. For case 1, Case 2 and case 3, the contribution of two Ingate parameters is more than 66%. This shows that ingate parameter make a significant effect on the three case quality objective.

IX. VALIDATION EXPERIMENT

The Validation experiment is the final step in verifying the conclusions from the previous round of experimentation. The estimated S/N ratio η_{opt} using the optimal level of gating parameters can be calculated as Eq.16

$$\eta_{opt} = \eta_{tm} + \sum_{j=1}^{n} \eta_{om} - \eta_{tm}$$
 (16)

Where η_{tm} is total mean of the multi-response S/N ratio, η_{om} is mean of the multi-response S/N ratio at the optimal level, and *n* is the number of the main design parameters that affect the quality characteristics. In confirmation experiment, it is found that the increase in multi-response S/N ratio from the initial gating parameters to the optimal gating parameter is 0.52864 dB. As product Yield has decrease 0.55%, the shrinkage porosity is decreased by 1.19% and filling velocity is decreased by 19.14%.For the case 3, the increase of the multi-response S/N ratio from the initial gating parameters to the optimal gating parameters is 0.96734 dB

X. CONCLUSION

The Taguchi method with multiple performance characteristics has been demonstrated for obtaining a set of optimal gating system parameters based on the defined objectives. The conclusions may be stated; the multiple performance characteristics such as product yield, shrinkage porosity, and filling velocity can be simultaneously considered and improved through this optimisation technique. For case 1 and case 2 and case 3, the A3B1C1D1 is the optimum level with the maximum multi-response S/N ratio. Regardless of the case 1 to case 3, the sequence of the four factors affecting the casting quality is the, the ingate height, the ingate width runner height and the runner width. The ingate height is the most significant factor which influences the casting quality. The optimal parameters for the gating system may be same with different weighting factors from case inside

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Advantage of SWET Technique on Joining Inconel 792 Material

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Abstract - Inconels 792 are nickel-base superalloy material that has high strength and creep resistance at temperature near their melting point. This material is commonly used in aircraft gas turbine (jet) engines, where parts or components are subjected to high temperature and high stress. Not-withstanding the high-temperature capabilities of the alloys, during service the parts are often damaged by hot gas erosion and other types of mechanism. Welding is one of the repair method available nowadays. The application is typically accomplished by Gas Tungsten Arc Welding (GTAW). Unfortunately, however, these superalloys also have limited ductilities at elevated temperature ranges, a phenomenon termed "strain-age" cracking. The solution proposed is Superalloy Welding at Elevated Temperature (SWET). Elevating temperature on the parts or components that are to be welded probably could reduce the thermal gradient occurred, thus creating a crack-free weldments. Also elevated temperature could reduce the amperage needed to achieve the welding temperature, hence lower electricity and cost are resulted.

Keywords : Inconel, Superalloy, GTAW, SWET.

GJRE-A Classification : FOR Code: 091207



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Advantage of SWET Technique on Joining Inconel 792 Material

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Abstract - Inconels 792 are nickel-base superalloy material that has high strength and creep resistance at temperature near their melting point. This material is commonly used in aircraft gas turbine (jet) engines, where parts or components are subjected to high temperature and high stress. Notwithstanding the high-temperature capabilities of the alloys, during service the parts are often damaged by hot gas erosion and other types of mechanism. Welding is one of the repair method available nowadays. The application is typically accomplished by Gas Tungsten Arc Welding (GTAW). Unfortunately, however, these superalloys also have limited ductilities at elevated temperatures, and are consequently subject to cracking due to differential thermal strains in some temperature ranges, a phenomenon termed "strain-age" cracking. The solution proposed is Superalloy Welding at Elevated Temperature (SWET). Elevating temperature on the parts or components that are to be welded probably could reduce the thermal gradient occurred, thus creating a crackfree weldments. Also elevated temperature could reduce the amperage needed to achieve the welding temperature, hence lower electricity and cost are resulted.

Keywords : Inconel, Superalloy, GTAW, SWET.

I. INTRODUCTION

N ickel-base superalloys are extensively used in aircraft gas turbine (jet) engines. These superalloys which have the highest volume of precipitates, typically 40 volume percent or more, exhibit the highest strengths and creep resistances at temperature near their melting points (Flowers, G.E, at al.1998).

These high-volume-fraction gamma prime superalloys are used in articles such as turbine blades and vanes, which operate at high temperature for prolonged periods. Hence, these parts are often damaged by hot gas erosion and other types of mechanisms. However, these superalloy materials are difficult and expensive to manufacture. Therefore, when such parts or components are damaged during engine operation, it is far more desirable to repair rather than replace it. As a result, a variety of repair method have been developed and reported.

Repair of damaged region is commonly accomplished by a welding process. After the damaged area is cleaned, a filler metal is melted and applied to the damaged area. The application is typically accomplished by tungsten inert gas welding, wherein an electric arc is struck between the article and a tungsten electrode, forming a molten pool in the damaged region. But there is a problem with the precipitation hardenable alloys, such as Inconel 792. These materials have the inability to weld with a like material for purposes of repair. Welding initiates high temperatures that have a tendency to cause cracking at the area of the weld site, thereby resulting in destruction of the welded parts. The biggest issue is the creation of differential thermal stresses that lead to strain-age cracking and liguation cracking in the weldment and in adjacent regions of the welded substrate. This cracking is harmful to the performance of the welded parts, and a number of methods have been proposed to overcome the cracking.

In one such approach, the application of Superalloy Welding at Elevated Temperature (SWET) is conducted on the parts. Pre-heating prior to welding is done to a temperature greater than its aging temperature and to maintain that temperature during the welding operation. Generally, the purpose of SWET is to minimize the thermal gradient, thus reducing the residual stress created on the weldment. This article will describe the SWET technique and the advantages of its application. An experiment has been carried out to see the performance of the application and will also be explained.

II. WHAT IS SWET

Superalloy, like it has been mentioned before, is a very difficult-to-weld material. SWET is advancement in repairing or welding cast superalloy. The application process is heating the article to elevated temperature and maintaining that temperature prior to welding. In the application of SWET, preheating should be in a temperature greater of its aging temperature. This is to avoid the precipitation phase to commence resulting strengthening of the material. The combination of strengthening and stress produced by the welding can cause cracking (Everett, M.A., 1987)

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Preheating will also reduce thermal gradients due to welding operation. Under rapid heating, the grain boundary phases are unable to dissolve fully into the surrounding matrix and partial dissolution leads to the formation of a low melting point eutectic and melting of the grain boundary region. Local dissolution of grain boundary phase will cause liquation cracking or fissuring. Preheating will also reduce cooling rate, thus producing more ductile metallurgical structure with greater resistance to cracking. For superalloy material, preheating typically carried out ranging from 500°C – 1010°C [Mokadem, S., 2009).

III. WELDING DEFECT

The major difficulty of welding a superalloy is the occurrence chance of defects on the weldments (Fig.1). Most common defect is the hot cracking. Hot cracking predominantly occurs in the Heat Affected Zone (HAZ). Hot cracking occurs due to the effects of the thermal cycle of welding. Rapid heating and cooling occur in the area adjacent to the weld. Incipient melting can be caused by the welding process. Incipient melting at grain boundaries can lead to reduced ductility and subsequent cracking (Donachie, M.J. & Donachie, S.J., 2002).

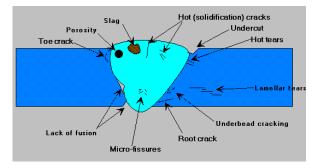


Fig. 1 : Types of defects on weldments (Fontana, F.G., 1987)

Liquation cracking in the HAZ is also another defect that can form due to welding. The liquation or melting occurs because of a reaction between dissolving precipitate and the matrix. When melting is accompanied by sufficient thermal stress, fissuring can form along the HAZ grain boundaries and extend into the fusion zone.

IV. EXPERIMENT PROCEDURES

a) Inconel 792

Inconel 792 is classified in as-cast nickel-based superalloy which is used for components operating in high temperature, corrosive environment with high working load. This material is typically used for turbine wheel APU that has working temperature ranging from 566 °C – 650 °C and rotating speed at 41.700 RPM (Unknown, 2003). Inconel material exhibit high strength

and creep resistance at temperature below their melting points. However, these superalloys also have limited ductility at elevated temperature.

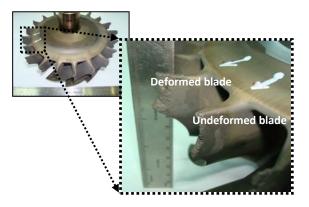


Fig. 2 : Failed and worn out turbine wheel blade tip due to cracking, two samples of deformed and undeformed blade were researched

For the experiment, composition analysis on the specimen is conducted by Energy-Dispersive X-ray analysis (EDX) method.

Chemical Element	IN-792 (%) Std	Measured on Base
С	0.2	1.7
Ni	60	67.56
Cr	13	10.91
Со	9	11.69
Мо	2	-
Fe	-	-
Al	3.2	2.45
В	0.02	-
Ti	4.2	3.99
Та	-	-
W	4	-
Zr	0.1	-
Other	2 Nb	1.13 Si
		0.57 S

Tabel 1 : Measured on the spot by EDX system analysis compared to the standard of Inconel 792

b) Preheating

For this experimental purpose, preheating is applied on temperature 200 °C, 400 °C and 600 °C for 1-2 hours. Preheating the article is performed using a heater and a larger mass holder, as shown in Fig.3.



Fig. 3 : Photograph of larger mass holder covered with heater, part marked as red circle

c) Repair Welding

Most common arc welding technique used in many industries is the Gas Tungsten Arc Welding (GTAW). GTAW is a welding process that uses an arc between a tungsten electrode (non-consumable) and the weld pool. The process is used with shielding gas and without the application of pressure. The process may be used with or without the addition of filler metal.

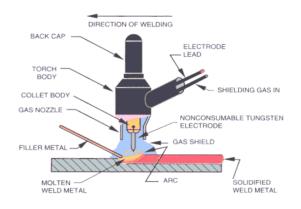


Fig. 4: Schematic of GTAW Technique (http://www.spectroweldinstitute.com)

GTAW has become indispensable as a tool because of the high-quality welds produced and low equipment costs. GTAW can be used to weld more materials than any other welding process, even exotic and heavier-alloyed metals. Among those materials you can successfully use GTAW for stainless steel, aluminum, nickel, and titanium. This has become the main reasons for selecting GTAW on the repair application (Fig.4).

d) Advantages of GTAW Technique

- Produces superior quality of welds, generally free of defects.
- Free of the spatter which occurs with other arc welding processes.

- Can be used with or without filler metal as required for the specific application.
- Allows excellent control of root pass weld penetration.
- Produce inexpensive autogenously welds at high speeds.
- Can use relatively inexpensive power supplies.
- Allows precise control of the welding variables.
- Can be used to weld almost all metals, including dissimilar metal joints.
- Allows the heat source and filler metal additions to be controlled independently.
- Allows for welding in all positions.

e) Process

After the article has been mounted on to the larger mass holder and preheated, the welding process can be performed. The GTAW process uses a non-consumable tungsten (or tungsten alloy) electrode held in a torch. Shielding gas is fed through the torch to protect the electrode, molten weld pool, and solidifying weld metal from contamination by the atmosphere (Unknown, 2008).

The electric arc is produced by the passage of current through the conductive, ionized shielding gas. The arc is established between the tip of the electrode and the work. The electricity used for this process is fed from a 65 KVA 3 Phase 63 Ampere 50 Hz Power Electric (Fig.5). Heat generated by the arc melts the base metal. Once the arc and weld pool are established, the torch is moved along area being repaired and the arc progressively melts the faying surfaces. Filler wire, if used, is usually added to the leading edge of the weld pool to fill the repaired area. Cooling of this process is then conducted by still air.



Fig. 5 : GTAW process being performed

V. Repair Results And Discuss

As shown in Fig.6, the welding process has been initiated without any trouble. Visual inspection has been conducted to see any defects on the welded surface and also the HAZ. Observation reveals there is no defect detected yet. Further examination on microstructures should be initiated to see any defects occur in the subsurface. 2012



Fig. 6 : Photographs of welded articles, weldments are marked with red circle

Noticed during the repair accomplishment, the increasing preheating temperature on the parts reduces the amperage needed to achieve the arc of welding. Lower amperage will reduce electricity usage, hence lower cost is needed for welding application. Electricity usage was noted and shown in Table 2.

Table 2 : Electricity usage during welding operation

	Temperature (°C)	Voltage(V)	Amperage (A)
1.200	200	10	17
I.400	400	10	13
l.600	600	10	11

a) Metallographic Examination



Fig. 7 : Photographs of prepared specimen for metallographic examination

Fig.7 shows metallographic practice by cutting, sectioning, mounting, grinding, polishing, and etching was done per ASTM E 3 & E 407. The etching reagent used in this practice was Kalling reagent's No. 2.

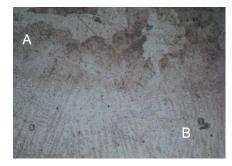


Fig. 8 : Stereo-microscope Photograph of SWET application on 400 °C, A) Base metal and B) Weld metal, etched by Kalling Reagent's no. 2, 100x

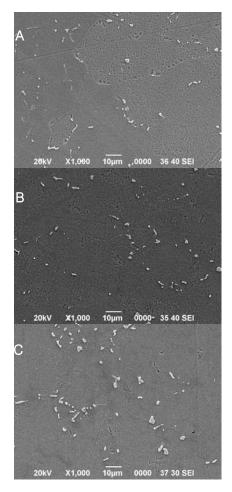


Fig. 9: Photograph of SEM result welded specimen heated at A) 200 °C, B) 400°C and C) 600°C, Etched by Kalling Reagent's no. 2, 1000x

It is shown on Fig.8, distinct material difference between base metal, Inconel 792, and weld metal, Inconel 625, separated by diffusion line.

Fig.9 shows SEM results after been etched. On the entire specimens, it can be seen carbides forming on the grain boundaries. Gamma-prime precipitates are also available within the gamma matrix. Different color on photographs as an effect of different contrast applied during SEM.

Fig.10 shows photographs of the base metal and weld metal microstructure. Photographs are taken using SEM with 1000x magnification. Fig.10A, 10C and 10E shows base metal with different preheating temperature applied, in orderly 200°C, 400°C, and 600°C. Increased preheating temperature results increasing maximum cooling rate. Hence, softer and smaller grain sizes are formed on the metal. Reducing grain size reduced susceptibility to hot cracking (Donachie, M.J. & Donachie, S.J., 2002). However, there is no distinct difference between the base metal.

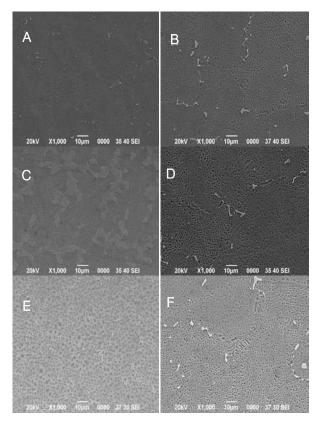


Fig. 10 : Photograph of weld metal and base metal under SEM metallography, 1000X

Fig.10B, 10D and 10F shows no microstructure changes. Because the base metal is far from the welding area and preheating temperature are kept below phase transition temperature, no changes occurred (Unknown, 1992).

As seen on Fig.11, microcracks have been detected on the article that was welded at temperatur 200 °C. Based on the location of the cracks which is on the HAZ area, it is predicted as a liquation cracking (Donachie, M.J. & Donachie, S.J., 2002). Rapid heating on the article creating a huge thermal gradient resulting thermal stress around HAZ area. Another stress applied on the area came from the welding procedure. Welding direction creates transversal tension on the specimen, adding up more stress. The present of a second-phase precipitate can cause increased hardness of the specimen. Increasing hardness and the inability to relieve stress due to welding are a perfect combination to cracking. Increased preheating temperature prior to welding is proposed to reduce thermal gradient and increase maximum cooling rate which enable the article to relieve thermal stress (Haafkens, M.H., & Matthey, J.H.G., 1982)

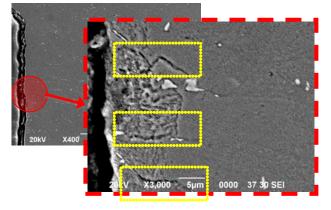


Fig. 11 : Microcracks detected with SEM on the HAZ area on SWET applied article at 200°C, 3000x

b) Microhardness Examination

Inconel 792 is nickel base precipitationhardening cast superalloy that may be welded in the solution-treated condition because greater ductility of the base metal in the solid solution phase permits stress relaxation during welding. Inconel 792 has 1100-11500C gamma prime solvus temperature in where the solution heat treating at 11200C and the aging heat treating at 845oC is conducted (Donachie, M.J. & Donachie, S.J., 2002). The SWET technique may eliminate strain age cracking at base metal, weld metal, and heat-affected zone upon subsequent heat treatment to develop alloy mechanical properties.

Concerning the result of microhardness distribution shown in Fig. 12, it seems that the preheat temperature 200, 400, 600°C have no significant influence to hardness distribution on HAZ and base metal, except hardness distribution on weld metal

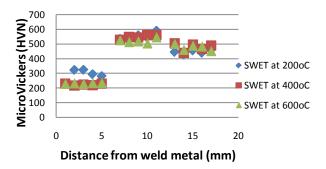


Fig. 12 : Hardness distribution on weld pool, HAZ, and base metal. Name of Machine: Zwick/ Roell Indentec

200°C pre heating somewhat affect the increasing in hardness distribution in weld metal that may be caused by higher cooling rate resulting in smaller grain size in the weld pool. Fig.12 informed that an increase in the pre-weld heat treatment temperature increased the grain size but the hardness decreased, although the hardness of 718 Plus alloys was still greater than that of Inconel 718 (Vishwakarma, K.R., et al., 2005). However, the disadvantage of 200°C preheating is inducing the availability of micro cracks.

c) Advantage of SWET

- Drive away moisture and contaminant from the weld area.
- The slower cooling rate provides an opportunity for hydrogen that may be present to diffuse out harmlessly, reducing the potential for cracking.
- Reducing temperature gradient during welding operation, minimize excessive residual stress, thus reducing chance of cracking.
- More controlled heating and cooling on the material, resulting better microstructure.
- Slow down the cooling rate in the weld metal and base metal, producing a more ductile metallurgical structure with greater resistance to cracking.
- Amperage needed to achieve welding temperature are reduced, welding cost can be minimized.

VI. Conclusions

- This analysis study is based on the evidence of experimental investigation. The following is concluding remarks from this study.
- Inconel 792 is an as-cast nickel-base superalloy and has a difficult-to-weld characteristic
- Welding difficulty is due to its precipitation hardening profile. Welding cause thermal gradient which will induce precipitate formation. Hardening will trap excess stress which leads to cracking.
- Cracking commonly occurs on the HAZ where temperature could increase or decrease rapidly and non-uniform.
- SWET is an application which can solve these difficulties, increasing Inconel-792 part capability to be repaired. Heating article prior to welding will reduce differential of temperature adjacent to the welding area.
- Heating the article prior to and during welding should be done in temperature ranging from 500 °C and 1010 °C.
- Heating will reduce cooling rate, resulting increased ductility and better microstructure.
- Welding technique suitable for SWET application on Inconel 792 is the Gas Tungsten Arc Welding. Because its capability to weld wide range of alloys, low cost equipment, and great quality weldment.
- SWET application not only creating a crack-free weldment, but also reducing welding cost by lowering amperage needed to reach arc of welding.

VII. Acknowledgments

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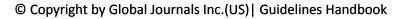
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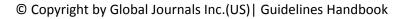
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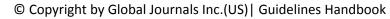
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