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AUTOMOTIVE ENGINEERING

DISCOVERING THOUGHTS AND INVENTING FUTURE

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CONTENTS OF THE VOLUME

- i. Copyright Notice
- ii. Editorial Board Members
- iii. Chief Author and Dean
- iv. Table of Contents
- v. From the Chief Editor's Desk
- vi. Research and Review Papers
- 1. Certain Results of Examination of Technical Stochastic Stability of A Car After Accident Repair. *1-8*
- 2. Operating Experience and Analysis of Engine Operated on Ethanol Diesel Emulsion. *9-12*
- 3. Online Tool Wear Prediction Models in Minimum Quantity Lubrication. 13-18
- 4. Laboratory-Scale Bioremediation Experiments on Diesel and Polycyclic Aromatic Hydrocarbons Contaminated Soils. *19-21*
- 5. Global Social and Economic Impact on The use of Biofuels and Recomendations for Sustainability. 23-30
- vii. Auxiliary Memberships
- viii. Process of Submission of Research Paper
- ix. Preferred Author Guidelines
- x. Index



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Certain Results of Examination of Technical Stochastic Stability of A Car After Accident Repair

By Jerzy Kisilowski, Jarosław Zalewski

Warsaw University of Technology.

Abstract - This paper presents the chosen results of simulation of sports car mathematical model in different conditions of motion. The car model was loaded with the extra mass representing both driver and passenger. The location of the center of mass was disturbed, as if the car had previously been damaged due to side impact accident, and then repaired without the control of basis points in its body. It is shown how the car body can be damaged as a result of side crash at different velocity.

A simulation of double lane change was conducted as a maneuver of omitting a long obstacle. Different road conditions were taken into consideration, i.e. icy, uneven road. In further steps, some parts of road lane was divided into defined number of disjoined classes, which enabled us to find the frequency of the car remaining in each class. This, in turn will allow the examination of technical stochastic stability of car model and comparison with the definition according to ISO 8855:1991.

Keywords : safety, stability, side impact, road accident.

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CERTAIN RESULTS OF EXAMINATION OF TECHNICAL STOCHASTIC STABILITY OF A CAR AFTER ACCIDENT REPAIR

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Certain Results of Examination of Technical Stochastic Stability of A Car After Accident Repair

Jerzy Kisilowski^α, Jarosław Zalewski^Ω

Abstract - This paper presents the chosen results of simulation of sports car mathematical model in different conditions of motion. The car model was loaded with the extra mass representing both driver and passenger. The location of the center of mass was disturbed, as if the car had previously been damaged due to side impact accident, and then repaired without the control of basis points in its body. It is shown how the car body can be damaged as a result of side crash at different velocity.

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I. INTRODUCTION

ne of the most important issues concerning road traffic in recent times is the car, human and road active and passive safety. The scope of much research is the examination of different aspects of safety within the driver - car - surrounding system. The aim of this paper is to show the chosen results of examination of stochastic technical stability of a sports car mathematical model, with the consideration of the changes caused by the side impact crash and an after accident repair, as well as road conditions and disturbances coming from the road surface. Definition of stochastic technical stability is presented in [2], [3], [4] and [5]. In [1] the stability of discrete and continuous structures is presented, whereas in [9] - general mechanical criteria of retaining the stability by the car. These criteria are used in theory of road car dynamics. In [10] the mathematical description of the process of crash of vehicles is presented.

The necessity of conducting such research results, among others, from the statistical data. The authors concentrated on side impact accidents and their share in general number of accidents in Poland. Collisions were not analyzed.

ii. Chosen analysis of Road Accidents

In figure 2.1 percentage share of side impact crashes in general number of accidents is shown. This type of crashes establishes over 30 per cent of all accidents in Poland between 1995 and 2008. Taking into consideration the severity of injuries as well as deformations of car body, it is important to pay attention to both the reasons and the consequences of side impact crashes, which can occur in further exploitation of cars repaired after accident. There is often lack of control of geometric parameters of car body after repairing or changing the damaged parts.Statistics concerning road accidents with comments are also in [6], [8] and [11].

Taking into consideration what is mentioned above, the authors decided to focus on the analysis of side impact crash in the process of simulations (oblique location of the cars involved in accident in the moment of crash) and the examination of motion of the car, that was involved in this crash. The model of a sports car was chosen. Then the assumption was made, that neither the body of the chosen car was controlled on a special frame, nor its mass – inertia parameters were checked

Fig. 2.1 : Percentage share of different types of Crashes in general number of accidents in 1995 - 2008.



Source : own research.

Author^α: Warsaw University of Technology, Faculty of Transport. Author^Ω: Warsaw University of Technology Faculty of Administration and Social Science.

Another factor taken into account during the preparation of the simulation were the extreme conditions of road traffic. Among the accidents, for example in 2005, around 36 per cent (fig. 2.2) occurred in bad road conditions (wet road, snow, dirt, oil, leaves on the road), 32 per cent during bad weather (fig. 2.3). It made the authors to implement similar conditions to the simulation. Randomly occurring unevenness of the road was also added.

The additional simulation of side impact crash accident was done with the use of PC-Crash 8.0. Its purpose was to show deformations of a sports car body. The simulation of car motion after accident and repair was done with the use of MSC Adams 2005r2

Fig. 2.2: Percentage share of accidents connected to road conditions in poland in 2005.



Source : own research.



Fig. 2.3: Weather conditions during road accidents in Poland in 2005.

Source : own research

III. SIMULATION OF SIDE IMPACT CRASH IN PC CRASH SOFTWARE

To examine the depth of deformation in car body as a result of side crash, a simulation in PC-Crash software was done with the relevant parameters. The situation reflects oblique side crash. The car being hit is Ferrari 355 GTS and the car hitting is Mercedes S500. Results of this simulation are shown for two sets of velocities of colliding cars. The authors would like to pay attention to potential deformations of a sports car body, which can occur as a result of side crash. It is also necessary to mention the consequences in the further exploitation of such car.

Basic assumptions concerning the simulation of the oblique side impact crash:

- the motion is set on a dry road surface ($\mu = 0.8$);

- the cars move with two sets of velocities:

a) Ferrari – 50km/h, Mercedes – 60km/h;

b) Ferrari – 80km/h, Mercedes – 100km/h;

- the whole mass of Ferrari was increased from 1350kg to 1500kg, adding the mass of the driver and the passenger;

- the whole mass of Ferrari was increased from 2100kg to 2395kg, adding the mass of the driver and three passengers;

- the height of the center of mass for Mercedes was set on 0,6m, for Ferrari - on 0,45m.

In fig 3.1 the location before the crash is presented, while in fig. 3.2 a, b – the motion of both cars during the crash as a sequential location of both cars for each set of velocities respectfully. Damages to the sports car body are shown in fig. 3.3a, b.

Fig. 3.1: Location of cars before crash.

Source : own research

Fig. 3.2a: Simulation of oblique side impact crash for velocities 50km/h (Ferrari) and 60km/h (Mercedes).



Source : own research.

201

The simulation was realised for several times, during which the repetitiveness of the depth of deformations in car bodies was observed. Other parameters, for example velocities after the crash, differ in every simulation. However, the tolerance of such difference ranges from 2 to 5%, depending on if the car was hitting, or was being hit.

Fig. 3.2 a: Simulation of oblique side impact crash for velocities 80km/h (Ferrari) and 100km/h (Mercedes).



Source : own research.



Fig. 3.3 a: Deformation of the sports car body for the

Source : own research.

Fig. 3.3b: Deformation of the sports car body for the velocities 80 and 100km/h.



Source : own research.

In table 3.1a i 3.1b exemplary protocols of both accidents for both velocity configurations are shown.

The depth of the deformations is worth noticing. At v = 60km/h, the hitting car (Mercedes) has its front deformed by 0,33m, and at v = 50km/h for Ferrari it is 0,25m in the left side part of its body. It is also important to consider the mutual penetration of both cars.

The results of the simulation for the second set of velocities present almost 0,6m deformation for Mercedes and 0,43m deformation of side part in Ferrari.

The authors are especially interested in the deformation of the sports car, because on such basis the scale of disturbances of the center of mass after repair of a damaged car can be assumed. It is due to the lack of control of geometric and inertia parameters of car body in the process of the elimination of damages.

Tab. 3.1a ; Protocol of the side crash for velocities 50 and 60km/h.

car	Mercedes-Benz S 500	Ferrari - 355 Berlinetta		
INITIAL VALUES	OF PARAMETERS			
Before crash velocity [km/h]:	60.00	50.00		
Angle of the car [deg] :	-57.43	0.00		
Angular velocity around z axis [1/s] :	0.00	0.00		
Location of cm in x axis [m] :	-2.36	-3.14		
Location of cm in y axis [m] :	5.26	-3.91		
Location of cm in z axis [m] :	0.60	0.45		
Velocity along z axis [km/h] :	0.00	0.00		
Lateral tilt [deg] :	0.00	0.00		
Roll angle (around y axis)[deg] :	0.00	0.00		
Angular velocity around x axis [1/s] :	0.00	0.00		
Angular velocity around y axis [1/s] :	0.00	0.00		
FINAL VALUES O	F PARAMETERS	5		
After crash velocity [km/h]:	48.05	55.86		
Velocity change dv [km/h] :	14.56	23.25		
Angle of the car [st.] :	-41.31	168.94		
Angular velocity around z axis [1/s] :	0.01	0.65		
Location of cm in x axis [m] :	11.10	15.03		
Location of cm in y axis [m] :	-10.84	-8.79		
Location of cm in z axis [m] :	0.60	0.44		
Velocity along z axis [km/h] :	0.03	0.17		
Lateral tilt [deg]:	1.61	-1.52		
Roll angle (around y axis) [deg] :	0.00	5.02		
Angular velocity around x axis [1/s] :	-0.13	-0.70		
Angular velocity around y axis [1/s] :	0.00	0.09		
Depth of the deformations [m] :	0.33	0.25		
Restitution coefficient k	0.1	0		

Source : own research.

Pojazd	Mercedes-Benz S-500	Ferrari 355-Berlinetta
INITIAL VALUES OF PARAMETER	S	
Before crash velocity [km/h]:	100.00	80.00
Angle of the car [deg] :	-57.43	0.00
Angular velocity around z axis [1/s] :	0.00	0.00
Location of cm in x axis [m] :	-2.36	-3.14
Location of cm in y axis [m] :	5.26	-3.91
Location of cm in z axis [m] :	0.60	0.45
Velocity along z axis [km/h] :	0.00	0.00
Lateral tilt [deg] :	0.00	0.00
Roll angle (around y axis) [deg] :	0.00	0.00
Angular velocity around x axis [1/s] :	0.00	0.00
Angular velocity around y axis [1/s] :	0.00	0.00
FINAL VALUES OF PARAMETERS		
After crash velocity [km/h]:	78.79	90.87
Velocity change dv [km/h] :	26.54	42.38
Angle of the car [st.] :	92.37	- 179.59
Angular velocity around z axis [1/s] :	1.60	0.00
Location of cm in x axis [m] :	22.80	33.01
Location of cm in y axis [m] :	-19.54	-15.66
Location of cm in z axis [m] :	0.60	0.46
Velocity along z axis [km/h] :	0.08	-1.36
Lateral tilt [deg] :	8.18	-6.84
Roll angle (around y axis) [deg] :	-0.02	-1.75
Angular velocity around x axis [1/s] :	-0.03	0.30
Angular velocity around y axis [1/s] :	0.24	-0.21
Depth of the deformations [m] :	0.58	0.43
Restitution coefficient k	0	.10

Tab. 3.1b : Protocol of the side crash for velocities 80 and 100km/h.

Source : own research.

IV. DESCRIPTION OF THE SIMULATION OF CAR MATHEMATICAL MODEL WITH THE DISTURBED CENTER OF MASS

The object of the simulation was the model of a sports car. For this model the mass and location of the driver and the passenger was included in the mass-inertial parameters. The model is shown in fig. 4.1.

The simulation, realizing the maneuver of double lane change was done with the use of MSC Adams/Car 2005r2 software. It was prepared for the conditions given below:

- additional mass representing the driver (85kg) and the passenger(70kg) was included;

with the use of static moments new coordinates(x, y, z) of the center of mass of car body were calculated. Initial location of the center of mass was (1450.0mm, 0.0mm, 450.0mm) in relation to the point called "origo", which is the point of the beginning of the axis system that is situated on the road surface and moves with the car. The initial mass of the car body was 955kg. The location of the center of mass after adition of the driver and the passenger changed to (1533.78mm, -4.52mm, 463.96mm). The mass of the car body increased to 1150kg. The location of the center of mas is calculated in relation to the point called "origo", which lies at the beginning of the axis system connected to the road surface but moving along with the car. The location of coordinates (x,y) can also be calculated as in [4];

disturbance was added to the coordinates calculated for the driver and the passenger. This disturbance is assumed to be a result of the previous crash and a possibility of the change of mass and moments of inertia. Two cases were taken into consideration. Basing on the results from p. 3 it was assumed, that in the process of repair the coordinates of the center of mass will not be restored to their initial location. No literature, describing the typical disturbances of the center of mass in car body after accident and repair. was found. New coordinates of the center of mass were defined as follows: x and y were transformed by 150mm, while the coordinate z - by 40mm (1383.78mm, 145.48mm, 503.96mm). As a result of those transformations new values of inertia and deviation moments were obtained;

the car rides for 700m realizing the maneuver of double lane change. Omitting long obstacle was simulated here. The car moved at 100km/h, on the icy road surface ($\mu = -0,30$);

time of the maneuver t = 25s;

- two trajectories were obtained a solid line for the car
- with additionally disturbed center of mass as a result of an accident, and a dash line for the car without after accident disturbances. In fig. 5.2 lateral displacement in function of time is shown for both the car with disturbed center of mass of its body by 150mm, and that with the undisturbed one.

Fig. 4.1 : Sports car model used in the simulation of motion.



Source : MSC Adams | Car.

v. Examination of Stochastic Technical Stability of Car Mathematical Model

The Ω set (the set containing the part of the trajectory in the range $[t_1;\ t_1+T])$ of the area of states E was divided into 10 classes every 50 mm: [K1; K10] (fig. 5.1a). In the plot road parameters and geometric parameters of the car were not taken into consideration.

The Ω' set (the set containing the part of the trajectory in the range $[t_1';\,t_1'+T'])$ of the area of states E was divided into 10 classes every 50 mm: [K1'; K10'] (fig. 5.1b). On the axis of lateral displacement (x) the classes of both sets are marked.

The frequencies of occurrences were counted for two areas:

- the area of omitting the obstacle [t₁; t₁+T] time frame [6s;16s] for every 10m of the road;
- final area, when the car finishes the maneuver $[t_1'; t_1'+T']$ time frame [22s; 25s] for every 10m of the road.

These time frames were divided into sub-frames with the step of $\Delta t = 0,375s$ (fig. 5.2).

In fig. 5.3a, b the parts of trajectories from fig. 5.2 are shown, on which the frequencies of occurrences are examined, for the maneuver realized in the conditions of disturbing the horizontal coordinates of the center of mass in car body (respectively for $[t_1; t_1+T]$ and $[t_1'; t_1'+T']$).

Fig. 5.1 a : Ω series in the area of states E containing the part of the trajectory for $[t_1; t_1 + T]$).









Source : own research.





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Source : own research.







VI. RESULTS

Analysis was made for the time frame $[t_1; t_1+T]$. The frequencies of occurrences were counted as follows. In every step of the time frame the frequencies of existence of the solution in each class were examined. Basing on [3]

 $W(K_{j}) = \frac{T_{Kj}}{T} = \frac{N_{Kj} \cdot \Delta t}{N \cdot \overline{\Delta} t} - \frac{N_{Kj}}{N}$

where:

 T_{Ki} - time of remaining in the given class;

- N_{Kj} - the number of sub-frames, for which the solution remains in the given class.

The values of the frequencies of occurrences are presented in tab. 6.1 – 6.2. Kolmogorov – Smirnov test (λ test) was performed in order to verify the H₀ hypothesis about the incompatibility of the step curve and the continuous probability on the significance level α =0,05. D_n, D_x, D_n' and D_x' here mean the Kolmogorov – Smirnov statistics. Normal and Rayleigh means were analyzed.

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Tab 6.1. Verification of the hypothesis on the basis of λ test for the step curve and the continuous probability for	1
The state of the hyperhouse of the sade of the stop out of and the continuous probability for	\subset
[t1; t1+T], without disturbances, normal and Rayleigh means.	(

(5.1)

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			step curve	continuous probability (normal means)						step curve	continuous probability (Rayleigh means)			
class	N_{Kj}	W(Kj)	F(Kj)	F(u)	D _n	critical value	$\lambda \text{ test}$ ($\alpha = 0.05$)	N_{Kj}	W(Kj)	F(Kj)	F(x)	D _x	critical value	λ test ($\alpha = 0.05$)
1	12	0,445	0,445	0,98745	0,54245	0,37543	hypothesis accepted	12	0,445	0,445	0,98515	0,54015	0,37543	hypothesis accepted
2	8	0,296	0,741	0,99998	0,25898	0,45427	hypothesis rejected	8	0,296	0,741	0,99999	0,25899	0,45427	hypothesis rejected
3	4	0,148	0,889	1	0,111	0,62394	hypothesis rejected	4	0,148	0,889	1	0,111	0,62394	hypothesis rejected
4	0	0	0,889	1	0,111	-	-	0	0	0,889	1	0,111	-	-
5	1	0,037	0,926	1	0,074	0,97500	hypothesis rejected	1	0,037	0,926	1	0,074	0,97500	hypothesis rejected
6	1	0,037	0,963	1	0,037	0,97500	hypothesis rejected	1	0,037	0,963	1	0,037	0,97500	hypothesis rejected
7	1	0,037	1	1	0	0,97500	hypothesis rejected	1	0,037	1	1	5,84E-10	0,97500	hypothesis rejected
8	0	0	1	1	0	-	-	0	0	1	1	5,84E-10	-	-
9	0	0	1	1	0	-	-	0	0	1	1	5,84E-10	-	-
10	0	0	1	1	0	-	-	0	0	1	1	5,84E-10	-	-

Source : own research.

Tab. 6.2: Verification of the hypothesis on the basis of λ test for the step curve and the continuous probability for [t1; t1+T], with disturbances of the center of mass by 150mm, normal and Rayleigh means.

			step curve	continuous probability (normal means)						step curve	continuous probability (Rayleigh means)			
class	Ν _{κj}	W(Kj)	F(Kj)	F(u)	D _n	critical value	λ test ($\alpha = 0.05$)	N_{Kj}	W(Kj)	F(Kj)	F(x)	D _x	critical value	λ test ($\alpha = 0,05$)
1	0	0	0	0,25462	0,25462	-	-	0	0	0	0	0	-	-
2	0	0	0	0,25462	0,25462	-	-	0	0	0	0	0	-	-
3	5	0,185	0,185	0,71226	0,52726	0,56328	hypothesis rejected	5	0,185	0,185	0,52608	0,34108	0,56328	hypothesis rejected
4	13	0,482	0,667	0,99990	0,33290	0,36143	hypothesis rejected	13	0,482	0,667	0,99993	0,33293	0,36143	hypothesis rejected
5	5	0,185	0,852	0,99999	0,14799	0,56328	hypothesis rejected	5	0,185	0,852	1	0,148	0,56328	hypothesis rejected
6	1	0,037	0,889	1	0,111	0,97500	hypothesis rejected	1	0,037	0,889	1	0,111	0,97500	hypothesis rejected
7	1	0,037	0,926	1	0,074	0,97500	hypothesis rejected	1	0,037	0,926	1	0,074	0,97500	hypothesis rejected
8	0	0	0,926	1	0,074	-	-	0	0	0,926	1	0,074	-	-
9	1	0,037	0,963	1	0,037	0,97500	hypothesis rejected	1	0,037	0,963	1	0,037	0,97500	hypothesis rejected
10	1	0,037	1	1	2,22E-16	0,97500	hypothesis rejected	1	0,037	1	1	3,35E-10	0,97500	hypothesis rejected

Source : own research.

VII. CONCLUSIONS

The examination of stochastic technical stability was made within two aspects. Trajectories of car motion and the frequencies of the occurrence of deviation from the initial location were compared. The analysis was made for the trajectories of motion after the double lane change maneuver and returning to initial lane.

If, according to fig. 5.1a and 5.1b, the area in which the trajectory can occur is divided into 10 equal sections, then for time $[t_1; t_1+T]$ it can be specified, whether the trajectories will leave this area. For such criteria the trajectories, after omitting the obstacle, remain in Ω area.

Maximal values of amplitudes of the trajectories for the car with the center of mass disturbed are near the border of stability, according to the accepted criteria. We believe that if the disturbances are increased, the trajectory will leave the Ω area.

Another scope of the conclusions concerns the frequencies of occurrence of the trajectories in the specified sections. As seen in tab. 6.1 and 6.2, the frequencies of occurrences in classes 4 and 5 are much higher for the trajectory of the car with the disturbed center of mass. For example, in class 4, for the car with the undisturbed center of mass the frequency of occurrences is zero, whereas for the car with the disturbed center of mass it is 0,482. In class 5 it is 0,037 and 0,185 respectively.

Maximal amplitude values of the trajectory for the car with the undisturbed center of mass for in classes 9 and 10 are zero, and for the car with the disturbed center of mass 0,037 in both classes.

As it is seen, the disturbances of the center of mass meaningly influences both the maximal values of amplitudes of the trajectories and the frequencies of occurrences in class for high amplitudes of trajectories.

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Operating Experience and Analysis of Engine Operated on Ethanol - Diesel Emulsion

By S.Peniel Pauldoss, Syed Ummer M. Thangal Research scholar, Karunya University, India.

Abstract - Ethanol is a bio-based renewable and oxygenated fuel, thereby providing potential to reduce the PM emission in diesel engines and to provide reduction in life cycle CO₂. Although ethanol has been used as fuels oxygenate to reduce tail-pipe emissions in gasoline, its use in diesel has been limited due to technical limitations (i.e., blending). Commercially viable e-diesel is now possible due to the development of a new additive system. Tetra Methyl Ammonium Bromide, a new additive allows the splash blending of ethanol in diesel. The objective of this investigation is to first create a stable ethanol-diesel emulsified fuel with 2% Tetra Methyl Ammonium Bromide additive, and then to generate transient performance, combustion and emissions data for evaluation of different ethanol content on a diesel engine. A singlecylinder, air-cooled, direct injection diesel engine developing a power output of 5.2 kW at 1500 rev/min was used. Base data was generated with standard diesel fuel. Subsequently three fuel blends, namely 80D: 20E, 75D: 25E, 70D: 30E and 65D: 35E by volume were prepared and tested. Engine performance and emission data were used to optimize the blends for reducing emission and improving performance. Results show almost equal performance for 90D: 10E blends with reduced emissions compared to neat fuel.

Keywords : Oxygenated fuel, additive, alternate fuels, performance and emission.



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S.Peniel Pauldoss^α, Syed Ummer M. Thangal^Ω

Abstract - Ethanol is a bio-based renewable and oxygenated fuel, thereby providing potential to reduce the PM emission in diesel engines and to provide reduction in life cycle CO₂. Although ethanol has been used as fuels oxygenate to reduce tail-pipe emissions in gasoline, its use in diesel has been limited due to technical limitations (i.e., blending). Commercially viable e-diesel is now possible due to the development of a new additive system. Tetra Methyl Ammonium Bromide, a new additive allows the splash blending of ethanol in diesel. The objective of this investigation is to first create a stable ethanol-diesel emulsified fuel with 2% Tetra Methyl Ammonium Bromide additive, and then to generate transient performance, combustion and emissions data for evaluation of different ethanol content on a diesel engine. A single-cylinder, air-cooled, direct injection diesel engine developing a power output of 5.2 kW at 1500 rev/min was used. Base data was generated with standard diesel fuel. Subsequently three fuel blends, namely 80D: 20E, 75D: 25E, 70D: 30E and 65D: 35E by volume were prepared and tested. Engine performance and emission data were used to optimize the blends for reducing emission and improving performance. Results show almost equal performance for 90D: 10E blends with reduced emissions compared to neat fuel.

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I

Introduction

educing the emissions and fuel consumption are no longer future goals instead they are the demands of the day. Indiscriminate extraction and increased consumption of fossil fuels have led to the reduction in carbon based resources. Alternative fuels promise to harmonize sustainable development, energy conservation, efficiency management and environmental preservation. Diesel engines have the advantages of high thermal efficiency lower emission of CO and HC. However, they have the disadvantage of producing smoke, particulate matter & oxides of nitrogen and it is difficult to reduce both NOx, and smoke density simultaneously in diesel engine due to trade off between NOx and smoke. It follows therefore. that substantial amount of effort has been directed at providing solutions to these problems. Among various developments to reduce emissions, the application of oxygenated fuels to diesel engines is an effective way to reduce smoke emissions. The potentiality of oxygenated fuels to suppress soot precursor formation is dominated by molecular structure as well as fuel oxygen contents

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[1]. When oxygen content in the fuel reaches approximately 30% by mass, smokeless combustion in diesel engines could be realized [2]. Since ethanol is a widely available oxygenate with a long history of use in gasoline blends it has also been considered as a potential oxygenate for diesel fuel blending. Researchers have investigated the use of ethanol in diesel engines over the past several decades. The limited miscibility at lower temperature, less heating value, poor lubricating properties and the required minor variations in fuel delivery systems restrict the use of ethanol in diesel fuel [3]. Also the addition of ethanol to diesel fuel decreases the blend's viscosity and causes cetane number of the blends linear reduction at ambient temperature [4]. Usually, when ethanol content in the blends reaches 20-40%, high concentration of additives are needed to ensure the mixture homogeneity in the presence of high water contents, and to attain the required cetane number for suitable ignition [5],[6]. Literary survey revealed that several oxygenated organic compounds (ether, amino alcohols, surfactants etc....) may be used as additives and when the ethanol increases concentration beyond 20%, high concentrations of additives needed to stabilize the mixture. Choosing unsuitable organic additive meets with several difficulties viz; immiscible fuel-alcohol blends, difficulty to handle, high cost etc., [7] [8] [9].

C. Sundar Raj et al investigated the effect of 1, 4 dioxane on ethanol diesel blends and reported even though 10% dioxane is capable to stabilize 30% ethanol with 60% diesel with significant reductions in emissions, 70% diesel- 20% ethanol with 10% dioxane is the optimum mixture [10].

Diesel-ethanol emulsion stabilized by 2% Tetra Methyl Ammonium Bromide is investigated in this study. Each of the different ethanol proportions were mixed with diesel in different percentages by volume (20%, 25%, 30% & 35%). The mixture was then kept for 5 days during which constant stirring were carried out. This was done so as to allow maximum amount of the oil to become dissolved. After this the mixture was thoroughly filtered to remove any undissolved particles. It was absorbed that there is a colour change in the fuel. The above fuel solution was then tested in a CI engine to determine its performance an emission characteristics.

II. FUEL PROPERTIES OF DIESEL, ETHANOL

General fuel properties of diesel and ethanol are presented in Table 1.

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TABLE 1 CHEMICAL PROPERTY OF DIESEL, AND ETHANOL	Molecular Formula	Molecular weight	Density at 20 °C (×10³kg/m²)	Boiling point (°C)	Flash point (°C)	Viscosity (mPa s)	Cetane Number	% of oxygen by weight
Diesel ^a	C _x H _y	190–220	0.829	180–360	65–88	3.35	45–50	0
Ethanol ^b	C ₂ H ₆ O	46.07	0.789	78.4	13	1.20	8	35

a. Table on Gasoline and Gasohol from Alcohols and Ethers, API Publication 4261, Second Edition (July 1988) b. http://en.wikipedia.org/wiki/Ethanol

III. PARAMETER TESTED AND Experimental Procedure

Experiments were conducted on Kirloskar TV1, Four stroke, single cylinder, and air cooled diesel engine. The rated power of the engine was 5.2kw at 1500 rpm. The engine was operated at a constant speed of 1500 rpm and standard injection pressure of 200 bars. The fuel flow rate was measured on volume basis using a burette and a stop watch. K-type thermocouple and a digital display were employed to note the exhaust gas temperature. AVL smoke meter was used for measurement of smoke density. NOx emission was measured by AVL digas analyzer. In cylinder pressure was measured with help of AVL combustion analyzer. The schematic experimental setup is shown in Fig. 1.



IV. RESULTS AND DISCUSSIONS

a) Performance Parameters

The lower heat value of the ethanol makes heat value of the mixture to decrease and hence the BSFC to increase for higher blends. Fig. 2 shows the brake specific fuel consumption for different ethanol additions at peak load. Among the blends 10% ethanol shows minimum brake specific fuel consumption to other blends. Increase in BSFC at higher blends indicates that there is no cavitation due to ethanol additions.





ethanol Concentration

Fig. 3 shows the brake thermal efficiency for different ethanol additions. From the figure it is observed that the brake thermal efficiency of 10% ethanol blends recorded a maximum of 30.5% efficiency. Improvement in combustion, especially diffusion combustion due to the increase in oxygen concentration from ethanol in the fuel is the reason for this increase in brake thermal efficiency. However, decrease in heat value of the blend makes the efficiency to decrease for higher blends.

b) Emission Parameters

The variation of smoke density with respective engine brake power is shown in Fig. 4. The addition of ethanol, decrease the smoke density especially between part loads to peak load. Addition of ethanol reduces smoke density uniformly at peak load because of the decreased quenching distance and the increased lean flammability limit due to the high combustion temperature. The presence of oxygen in the fuel assists in permitting the oxidation reactions to proceed close to completion. The results reveal that the tendency to generate soot from the fuel-rich regions inside diesel diffusion flame is decreased by ethanol in the blends. 16% reduction of smoke was observed for 90D: 10E blend ratio compared with the neat fuel.



Fig. 4: Veriation of smoke density for different ethanol concentration

The presence of oxygen increases the heat release rate for the oxygenated fuel and hence the NOx emission will be high. The anticipated increase in NOx emissions as a function of increasing ethanol concentration is apparent in Fig. 5. Nitrogen oxides emissions are predominately temperature phenomena. It can be seen that NOx emissions of all blends increase more rapidly than those of neat fuel as ethanol proportion and load increase at medium and high loads. The maximum increase in NOx emissions occur at 80~100% full load conditions because of long ignition delay and rich oxygen circumstance from ethanol in the mixture.



Fig. 5 : Veriation of NOx emmissions for different ethanol concentration

b) Combustion Parameters

Oxygen molecules presented in ethanol increase the spray optimization and evaporation and hence the combustion process of the engine. Fig. 6 illustrates cylinder pressure traces for different ethanol blended diesel fuels for various conditions of the engine. A peak pressure of 74 bars for 10% ethanol blend was recorded while it was 68 bars for neat fuel. The oxygenated fuel engine has longer delay period compared to neat fuel.



Fig. 6: Cylinder pressure for different crank angle.

Fig. 7 illustrates heat release rate of the oxygenated fuel blends and neat fuel at different crank angle. The heat release rate is high for oxygenated fuels due to the longer duration of the combustion. It can be seen that heat release rate curves of the oxygenated fuel blends and neat fuel show similar pattern. The reason is the rate of diffusion combustion of the oxygenated fuel increases the heat release rate and consequently oxygenated fuel has controlled rate of pre-mixed combustion.





V. CONCLUSSIONS

The results of the present study may be summarized as follows,

- Addition of 2% Tetra Methyl Ammonium Bromide as surfactant can stabilize up to 30% ethanol with diesel.
- The specific fuel consumption decreases with increase in ethanol blend in diesel fuel but 90D: 10E shows lower specific fuel consumption.
- Brake thermal efficiency decreases with increase in ethanol ratio. However, 90D: 10E shows equal performance compared with neat fuel.
- · Considerable amount of smoke reduction with a

little penalty in NOx was resulted

• Maximum cylinder pressure and heat release rate for blends were found to be increased.

On the whole it is concluded that 2% addition of Tetra Methyl Ammonium Bromide by virtue of its properties is capable to stabilize 30% ethanol with 70% diesel by volume, and 10% ethanol diesel emulsion can be used in a compression ignition engine with significant reduction in exhaust emissions as compared to neat diesel without any engine modifications.

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Online Tool Wear Prediction Models in Minimum Quantity Lubrication

By S.Narayana Rao, Dr. B.Satyanarayana, Dr. K.Venkatasubbaiah

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Abstract - With the problems in usage of cutting fluids, the use of Minimum Quantity Lubrication (MQL) has gained prominence. Though several mathematical models have been postulated in literature on dry cutting, models that deal with cutting fluids are very rare and the models on MQL are seldom found. The present work tries to discuss regression and artificial neural network models postulated on influence of MQL on tool wear, while machining AISI 1040 steel using HSS tool. The proposed models were validated with the experimental results.

Keywords : tool wear; MQL; cutting fluids; regression model; artificial neural networks. GJRE-B Classification: FOR Code: 860603



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S.Narayana Rao^a, Dr.B.Satyanarayana^o, Dr.K.Venkatasubbaiah^β

Abstract - With the problems in usage of cutting fluids, the use of Minimum Quantity Lubrication (MQL) has gained prominence. Though several mathematical models have been postulated in literature on dry cutting, models that deal with cutting fluids are very rare and the models on MQL are seldom found. The present work tries to discuss regression and artificial neural network models postulated on influence of MQL on tool wear, while machining AISI 1040 steel using HSS tool. The proposed models were validated with the experimental results.

Keywords : tool wear; MQL; cutting fluids; regression model; artificial neural networks

I. INTRODUCTION

Given the current state of manufacturing industry, the ability to develop robust products with the help of cost-effective techniques are necessary to meet the challenges of a dynamic and ever-changing sector. This is particularly true for production processes, where the idle and down times arising from various factors prove to be one of the major impediments in achieving the goal [1, 2].

In terms of the cost factors, machining is considered as one of the most important of the manufacturing processes. The associated machine downtimes are mainly attributed to the frequent replacement of worn tools. Hence, the prime focus for researchers to reduce the downtimes and achieve costeffectiveness resides in the estimation of tool life and the investigation of remedial measures for tool wear.

A key factor that affects the wear rate of tools is the temperature reached during the cutting operation along with the applied forces. Reduction in tool wear can be readily accomplished by using cutting fluids that can act both as lubricants and as coolants while machining. Water miscible oils prove to be the most promising and popular cutting fluids used, owing to the confluence of cooling properties of water and lubricating abilities of oil. Despite numerous advantages, their usage is restricted because of the microbial contamination that poses health hazards to the workers, and associated problems with their disposal. This has given rise to several alternatives including Minimum Quantity Lubrication (MQL).

To assess tool wear online, different methodologies are reported in literature. A majority of

the models consider different cutting parameters and predict tool wear either using mathematical models or artificial neural networks.

Mathematical models have been proposed to help evaluation of tool wear under different conditions [1, 3 and 4].

Rao [5] developed a mathematical formulation to estimate tool flank wear online through the estimation of cutting forces. Relation for predicting radial component of cutting forces from various measured machining parameters was developed.

Theoretical and experimental studies were carried out by Luo et al [6] to investigate the intrinsic relationship between tool flank wear and operational conditions in metal cutting processes using carbide cutting inserts. A flank wear rate model, which combines cutting mechanics simulation and an empirical model, was developed to predict tool flank wear land width. Machining was done under different operational conditions using hard metal coated carbide cutting inserts. The results of the experimental studies indicated that cutting speed had a more dramatic effect, than feed rate, on tool life. The wear constants in the proposed wear rate model were determined by regression analysis using the machining data and simulation results. A close agreement between the predicted and measured tool flank wear land width was reported.

Ozel and Karpat [7] studied the predictive modeling of surface roughness and tool wear in hard turning using regression and neural networks. The cutting tool used was cubic boron nitride. In this study, effects of cutting edge geometry, workpiece hardness, feed rate and cutting speed on surface roughness and tool wear were experimentally investigated. A four factortwo level fractional factorial design was used. Exponential model for surface roughness and tool flank wear for hard turning of AISI 52100 steel using CBN tools were proposed. The tool wear model was given as:

$$VB = K_2 C^{a1} V^{b2} L^{c3}$$

$$(1)$$

Exponential regression models for surface roughness and tool flank wear were given, respectively, for finish hard turning of AISI H13 steel using CBN tools (Eq.2.2 & 2.3).

$$R_{a} = K_{1} H^{a1} E^{b1} V^{c1} f^{d1} L_{c}^{e1}$$
(2)

$$VB = K_{2} H^{a1} E^{b1} V^{c1} f^{d1} L_{c}^{e1}$$
(3)

where 'K₁' and 'K₂' are proportionality constants, 'C' is CBN content of tool in percentage volume, 'V' is cutting speed, 'f' is feed, 'L_c' is cutting length in axial

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direction, 'H' is work material hardness and 'E' is edge radius of CBN tool.

Srikant [8] modeled tool wear in wet machining with cutting fluids of different emulsifier contents. The model was formulated as:

$$VB = 0.277 \times (\upsilon^{1.4} \ t_m^{0.109} \ F_C^{0.623} \ H^{0.669}) \ / \ (R_a^{1.6} k^{1.3} T_C^{1.3}) \ (4)$$

where VB is tool wear, υ is kinematic viscosity of the fluid, t_m is machining time, F_c is cutting force, H is hardness of the machined surface, R_a is the surface roughness, k is thermal conductivity and T_c is the cutting temperature. An average Regression coefficient of 0.85 was reported. However, the model was developed only for conventional lubrication and not MQL.

In recent years, the use of artificial neural networks (ANN) for the monitoring of tool wear has proved to be extremely successful. In the conventional system, the operator learns by his experience and tries to take decisions based on his past experiences. This learning is due to the processing of the external data or stimulus by the neurons in the brain to produce the reaction. Artificial neural networks imitate this learning behavior of the human brains. The network learns with the obtained data and takes decisions based on learning data. Many researchers tried Neural Networks to monitor the tool wear and obtained encouraging results.

S.Purushothaman and Srinivasa [9] trained a multi-layer perceptron with back propagation algorithm with 30 patterns of 6 inputs each consisting of speed, feed, depth of cut and the cutting forces in three directions. The outputs were the flank wear, centre line average of the workpiece and maximum depth of the profile as the outputs. The network was trained taking different neurons in the hidden layer as 10, 15 and 20. 15 neurons proved to be optimal. The weights obtained from the training were used for testing with 6 new patterns. Dimla [10] applied independent, descriptive inputs, viz. the three components of cutting force, three components of acceleration describing the vibration. Fusion of signals was emphasised. The results showed a success rate of 73-93% with a single layer perceptron, while the use of a multi layer perceptron scored an accuracy of 81-98%. The error obtained in the network was attributed to the noise in the data. The number of neurons in the hidden layer was fixed based on trial and error method to achieve the minimum error. Srikant [8] developed an ANN model using back propagation neural network for tool wear in wet machining. Better accuracy was reported compared to the built regression model (Eq.2). However, the model was built only for conventional lubrication method.

It is clear from the literature that the regression models and neural networks are employed for tool wear prediction as function of cutting conditions, tool geometry and work material. However, models applied to MQL are seldom found. Hence, there is a need for the development of prediction models as a function of lubricating conditions in MQL.

II. MATHEMATICAL REGRESSION MODEL

A mathematical regression model has been built to estimate tool wear on line. AISI 1040 steel was machined using cemented carbide and HSS tools under constant cutting conditions on al 10 HP lathe to estimate several influencing measurable parameters like cutting forces, temperatures, surface roughness of machined samples, hardness of measured samples, etc. The cutting conditions adopted were:

Averag	, le cutting s	- d	102 m/mi	'n	
Feed ra	ange	:	= 0.44 m	m/rev	
Depth	of cut		:	= 0.5 mn	n
Wator	miscihle	oil	with	carbon	nano

Water miscible oil with carbon nano tube inclusion levels as 0.5%, 1%, 2%, 3%, 4% and 5% were used as coolant. Flow rate of the coolant was maintained as 100 ml/ hr. Basic properties of the fluids like kinematic viscosity, thermal conductivity, etc. were also measured and used to postulate the model.

In order to reduce the number of variables involved in the model, dimensional analysis is carried out and the following five non-dimensional Π -terms are deduced.

$$\Pi_1 = \upsilon * t_m / R_a^2$$
(5)

$$\Pi_{2} = (T * \upsilon * F_{c}) / (R_{a}^{2} * k)$$

$$\Pi_3 = VB/R_3$$
(6)

$$\Pi_4 = (R_a^2 * H) / F_C$$

where, υ is kinematics viscosity of the fluids in m²/s, t_m is the machining time in min, R_a is surface roughness in m, VB is tool flank wear in m, T is cutting temperature in °C, H is hardness of tool is MPa. Since relation between different machining parameters is inherently non-linear, a relationship was assumed as:

$$\Pi_{3} = \mathsf{K}_{1} \, \Pi_{1}^{a} \, \Pi_{2}^{b} \, \Pi_{4}^{c} \tag{8}$$

The relation was converted into a linear relation by taking logarithms of Π terms as

$\log \Pi_3 = \log K_1 + a * \log \Pi_1 + b^* \log \Pi_2 + c * \log \Pi_4$ (9)

Multiple linear regression was carried out for the linearized terms using SPSS (a registered product of SPSS Inc., Chicago). Multiple linear regression postulates a functional dependence between the independent and dependent variables minimizing the modeling error. Experimental data obtained while using conventional cutting fluid, 0.5%, 1%, 2%, 3%, 4% and 5% CNT inclusion levels for HSS and cemented carbide tools was used to build the model, the remaining data was left for validation. A linear function was assumed between the logarithmic terms and the problem reduces to finding the coefficients a, b, c and K₁. In the present analysis, the above constants were found to be -0.284, 0.111. -0.903 and 139.31 (antilog of (2.144)) respectively. The formulated model may be expressed as:

 $VB = 139.31 \times (\upsilon^{-0.173} t_m^{-0.284} F_C^{1.014} H^{-0.903} T_C^{-0.111} R_a^{-0.46} k^{-0.111})(10)$

An average Regression coefficient of 0.91 was obtained.

Eq. 6 has been used to predict the value of tool wear from different parameters.

Analysis of Variance (ANOVA) is a powerful statistical technique often employed confirms the effect of several simultaneously applied factors on the response variable. A null hypothesis, postulating no dependence of the applied factors and response variables is considered and is checked for its validity. Degrees of Freedom (DF) and sum of the squares (SS) are computed for the considered data. F-statistic (variance ratio) is computed as the ratio of sums of squares denoting influence of factors and their interdependence. The computed value of variance ratio (F) is compared with the standard ANOVA table and the hypothesis is accepted or rejected at a particular (1% or 5%) confidence level. If the hypothesis is rejected at 1% confidence level, it also stands rejected at 5% confidence level [9].

In the present work, the degrees of freedom were found to be 3 and 122, F-statistic was obtained as 248.961 from SPSS. The tabulated critical value of F distribution for the obtained degrees of freedom at 1% significance level was 3.78. Hence the proposed null hypothesis advocating no dependence of tool wear on the taken parameters was rejected at 1% significance level. Hence the choice of parameters is justified.

III. ARTIFICIAL NEURAL NETWORKS

Tool wear monitoring in automated industries calls for monitoring systems that can replace human expertise and knowledge. Pioneering researchers realized that if computers are to replace humans then their design should resemble the brain. Artificial neural networks is a science that tries to imitate the mechanism of human brain in solving problems. Several types of artificial neural networks, based on particular computing abilities of the human brain are proposed. Choice of a particular neural network depends on the application [10].

Of the available artificial neural networks, back propagation network has gained importance due to the shortcomings of other available networks [11]. The network is a multi layer network that contains at least one hidden layer in addition to input and output layers.

The number of hidden layer neurons was kept as three and size of the network is fixed as 7-3-1, after testing for the error by trial and error. After fixing the network parameters, the network was trained using experimental data obtained while using 0, 0.5, 2, 4 and 5% CNT inclusions for HSS and cemented carbide tools to obtain stable weight structures. Using these weight structures, the network was tested for remaining data as input patterns.

IV. VALIDATION OF PROPOSED MODELS

The proposed models were validated by comparing the predicted results with the experimental results. Results from regression model and neural network model for HSS tool are compared with the experimental results (Figs. 1 & 2).



Fig. 1 : Comparison of predicted and experimental values while using HSS tool and cutting fluid with 1% CNT inclusion

201



Fig. 2: Comparison of predicted and experimental values while using HSS tool and cutting fluid with 3% CNT inclusion

Absolute values of percent errors obtained using regression and neural network models are presented in Table 1. It is observed that maximum error is 9.29% for regression model and 4.82% for neural network model.

Table 1 :	Absolute	error for	prediction	(HSS to	ool)
rubic r.	Absolute		prediction		JUIJ

Machining	Error for 1 inclus	% CNT	Error for 3 % CNT inclusion		
time (min)	Regression	ANN	Regression	ANN	
5	6.18	2.93	6.72	2.97	
15	5.7	3.6	6.72	4.29	
25	9.29	4.82	9.02	3.85	
35	7.8	2.02	2.27	2.27	
40	8.5	1.85	1.06	2.98	

Results from regression model and neural network model for cemented carbide tool are compared with the experimental results (Figs. 3 & 4).



Fig. 3: Comparison of predicted and experimental values while using cemented carbide tool and cutting fluid with 1% CNT inclusion



Fig. 4: Comparison of predicted and experimental values while using cemented carbide tool and cutting fluid with 3% CNT inclusion

Absolute values of percent errors obtained using regression and neural network models are presented in Table 2. It is observed that maximum error is 9.29% for regression model and 4.82% for neural network model.

Machining	Error for 1 % inclusion	CNT	Error for 3 % CNT inclusion			
	Regression ANN		Regression	ANN		
5	0.28	3.86	9.05	3.79		
15	8.37	2.67	4.80	1.81		
25	5.6	3.64	6.26	1.64		
35	1.79	1.41	6.48	2.54		
40	9.81	4.5	7.8	3.95		

Table 2 : Absolute error for prediction (Cemented carbide tool)

Comparison of predicted tool wear with experimental results in all the tested cases indicate that the error is less than 10% in the prediction of tool wear using regression model and 5% for neural network model, validating both the models (Tables 1 & 2). Higher error in regression model predictions is obtained since some of the factors that contribute to tool wear like condition of the machine tool, inconsistencies in workpiece-tool compositions, etc. were not taken into account and this affects the regression model.

However, since neural network was trained with the experimental data and the influence of all the factors is inherently present in the data, the model is devoid of above limitations. No generalization of the data is done in neural networks, as in case of regression model for finding best-fit curve. Neural network maps the inputs to the outputs in multi-dimensions and takes care of nonlinearity present in the case of study leading to more accurate predictions.

V. CONCLUSIONS

Tool wear prediction models were developed using mathematical regression and neural network. Experimental data of measured tool flank wear was used to develop the models. The models were used to predict tool wear for HSS and cemented carbide tools while using cutting fluids of different CNT content. Predicted tool wear values were compared with the experimental results to validate the developed models. Proposed regression and neural network models to predict tool wear based on several measurable parameters give the values of tool wear within acceptable limits. ANOVA justifies the parameters considered in the model. Neural network predicts tool wear with higher accuracy.

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Laboratory-Scale Bioremediation Experiments on Diesel and Polycyclic Aromatic Hydrocarbons Contaminated Soils

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Abstract - Laboratory investigations were performed to estimate the potential of bioslurry for bioremediation of PAHs and TPH-contaminated soil of Azimabad region in the south of Tehran refinery plant. The soil slurry-Sequencing Batch Reactor (SS-SBR) consisted of covered 8L Plexiglas vessel with a working volume of 6L. The reactor was equipped with a 400 rpm speed mixer. Oxygen was supplied through a fine-bubble diffuser at the bottom. A granular activated carbon trap as used to collect volatile organics in effluent air, fill period was relatively instantaneous, and Draw period lasted approximately 1 minute so the recent period comprised essentially the entire cycle time. In draw period a fraction of slurry (10%) was removed from period a fraction of slurry (10%) was removed from the SS-SBR weekly and it replaced with untreated slurry. This volumetric replacement volume of slurry (the recycle fraction) remained in the reactor to provide acclimated microorganism for the next batch of untreated slurry.

The soil used in slurry studies was poorly graded sand with clay (SP-SC) which contaminated with approximately 67500 mg/kg TPH and 500mg/kg PAHS and passed through a sieve with an opening diameter of 0.5mm tap water was added to produce solids concentration of 10% (0.1kg dry soil/l slurry). Ammonias nitrate and phosphate were added to provide a C: N: P ratio of approximately 60:2:1 process performance .The TPH concentrations were determined by Gas chromatography with Flame Ionization Detector (GC-FID) after ultrasonic extraction the PAHS concentrations were determined with both of High performance liquid chromatography (HPLC) an GC-FID after silica-gel clean up. The results have shown high overall removal efficiency for TPH close to 96%. whereas PAHs were not detected at the end of each cycles.

Keywords : Bioremadiation, PAHs, TPH, SS-SBR. GJRE-C Classification : FOR Code: 030301, 090401



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Laboratory-Scale Bioremediation Experiments on Diesel and Polycyclic Aromatic Hydrocarbons Contaminated Soils

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Abstract - Laboratory investigations were performed to estimate the potential of bioslurry for bioremediation of PAHs and TPH-contaminated soil of Azimabad region in the south of Tehran refinery plant.

The soil slurry-Sequencing Batch Reactor (SS-SBR) consisted of covered 8L Plexiglas vessel with a working volume of 6L. The reactor was equipped with a 400 rpm speed mixer. Oxygen was supplied through a fine-bubble diffuser at the bottom. A granular activated carbon trap as used to collect volatile organics in effluent air, fill period was relatively instantaneous, and Draw period lasted approximately 1 minute so the recent period comprised essentially the entire cycle time. In draw period a fraction of slurry (10%) was removed from period a fraction of slurry (10%) was removed from the SS-SBR weekly and it replaced with untreated slurry. This volumetric replacement volume of slurry (the recycle fraction) remained in the reactor to provide acclimated microorganism for the next batch of untreated slurry.

The soil used in slurry studies was poorly graded (SP-SC) which contaminated with sand with clay approximately 67500 mg/kg TPH and 500mg/kg PAHS and passed through a sieve with an opening diameter of 0.5mm tap water was added to produce solids concentration of 10% (0.1kg dry soil/l slurry). Ammonias nitrate and phosphate were added to provide a C: N: P ratio of approximately 60:2:1 process performance. The TPH concentrations were determined by Gas chromatography with Flame Ionization Detector (GC-FID) after ultrasonic extraction the PAHS concentrations were determined with both of Hiah performance liquid chromatography (HPLC) an GC-FID after silica-gel clean up. The results have shown high overall removal efficiency for TPH close to 96%, whereas PAHs were not detected at the end of each cycles.

Keywords : Bioremadiation, PAHs, TPH, SS-SBR

I. INTRODUCTION

Bioremediation of contaminated soils offers a number of advantages over conventional treatments on the basis of its environmental friendliness and low costs. The interest inthis technology has increased over the last few years (,USEPA 2001).

Slurry-phase bioremediation technology is applicable for treating soils and sludge contaminated with hazardous wastes and it is a cost-effective

alternative to cumbersome and often less effective treatment methods such as solid phase remediation(VenkataMohan et al., 2004, in press; Boopathy, 2000; Rahman et al., 2003; Bento et al., 2005; Sarma et al., 2006; Ramakrishna et al., 2006). The bioslurry treatment method has several advantages in that an optimal environment for degradation of the organic contaminants can be maintained with a high degree of reliability. Biological reactions can proceed at accelerated rates in a slurrysystem because of contact between contaminants and microorganisms, effective mixing and maintenance of high bacterial population, which enhance the degradation rate. (USEPA, 1993). Bioslurry reactors can be operated under aerobic or anaerobic or anoxic condi-tions(Zappi et al., 1996). Reduction in bioslurry reactors is initially postulated to be a consequence of the (potentially) limiting mass transfer rate i.e., from the soil to the aqueous phase, as it is assumed that microflora could only utilize substrates dissolved in aqueous phase.

Petroleum products such as diesel fuel, heavy oil, gasoline, fuel residues, and mineral oil are common soil contaminants. remediation of oil-contaminated soils to eliminate oily odors and oil .lm on runo. water and in groundwater is required.

The biodegradation of oils in a slurry-phase bioreactor(SPB) has a higher degradation rate than other biological treatment methods (US EPA, 1990; Puskas et al., 1995). Various modes of SPB operation have been tested in laboratories and pilot-scale plants, and one of the most common and best performing modes involves a soil slurry-sequencing batch reactor (SS-SBR).

The fate of polycyclic aromatic hydrocarbons (PAHs) in nature is of great environmental concern due to their toxic, mutagenic and carcinogenic properties (Haeseler et al., 1999). Their environmental mportance led the USEnvironmental Protection Agency (US-EPA) to identify 16 unsubstituted PAHs as priority pollutants, 8 of which are possible human carcinogens (Menzi et al., 1992). The potential use of microorganisms to clean up contaminated soil, sediments and water can provide efficient, inexpensive and environmentally safe cleanup of the waste material (Bishop, 1998).

In this study, we adopted a different method for enhancing the biodegradation of oil: we transferred the oils from the fine soil and increased contact between the

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microorganisms and the oil.. The microorganisms must be separated from the soil so that both can be reused.

The use of a support medium bearing the microorganisms also permitted the separation of the microorganisms from the soil after purification.

This paper describes the treatment of a soil with TPH and PAH contamination in laboratory bio-slurry reactor and describe the ability of that to remove oil and polycyclic aromatic hydrocarbons.

II. SOIL SAMPLES

The soil used in slurry studies was poorly graded sand with clay (SP-SC) which contaminated with approximately 67500 mg/kg TPH and 500mg/kg PAHS and passed through a sieve with an opening diameter of 0.5mm (Table 1)

III. BIOREACTOR

The study was carried out in the thermostated chamber (at21±0.3 °C) using a 8 I pyrex-made reactor with a 17.1 cm diameter and 47.0 cm height (Fig. 1), upper closed with a stainless steel flange to ensure the seal. The reactor operating level was set at 41.0 cm (leaving 6 cm of freeboard); thus the reactor working volume was 6 I. The reactor was equipped with a DO probe (cell OX325, WTW), a pH probe (Mettler Toledo) and a magnetic stirrer with a variable speed impeller, working at 400 rpm and placed in the flange central position. Oxygen was supplied by an air flow of 50 N I h–1 and distributed through a fine bubble diffuser at the bottom of the reactor. The air flow was forced to pass through a humidifier

Before entering the reactor, in order to minimize evaporation.Off gases firstly were piped to an air-cooled condenser andthen collected to an amberlite resin trap (XAD2 Supelco) to catch volatile organic compounds. Peristaltic pumps (Cellai 503U) were used for fill and draw operations.

IV. THE FEED SLURRY

Before using, the soil was passed through a 0.5mm sieve. The sieved fraction was partially air-dried and was stored at 4°C to maintain biological activity. Prior to using in bioslurry experiments, the samples were spiked with a known concentration of PAHs including Naphthalene, Phenanthrene and Pyrene (750 mg/kg) dissolved in dichloromethane. Tap water was added to produce a solids concentration of 10% (0.1 kg dry soil/L slurry). The Mineral Salt Medium (MSM) provide a C:N:P ratio of approximately 60:2:1 by adding ammonia, nitrate and phosphate as NH4Cl, KNO3, K2HPO4. Sodium sulphate (Na2SO4) and Magnesium sulphate heptahydrate (MgSO4.7H2O) were added with 2000 mg/L and 200 mg/L concentrations respectively. Since the samples were collected from an aged contaminated site, the endogenous microorganisms were supposed to degrade contaminants and therefore no adapted microorganism addition (bioaugmentation) was performed.

v. Experimental Design

6 L of prepared slurry was fed to reactor through the feed reservoir by gravity. The reactor was operated in sequencing batch mode. Fill period was relatively instantaneous, and Draw period lasted approximately 1 minute so the React period comprised essentially the entire cycle time. In draw period a fraction of slurry (10%) was removed from the SS-SBR weekly and it replaced with untreated slurry. This volumetric replacement strategy provided a 14 days solid retention time (SRT) and 70 days hydraulic retention time (HRT). A certain volume of slurry (the recycle fraction) remained in the reactor to provide acclimated microorganism for the next batch of untreated slurry.

VI. ANALYSES OF CONTAMINANTS

a) TPH analysis

At every sampling event, the soil slurry samples were collected from all the reactors for the total petroleum hydrocarbon (TPH) analysis. Diesel fuel components were extracted with dichloromethane and analyzed by gas chromatography as follows. Fifty ml of dichloromethane was mixed with 25 ml ofsoil slurry sample in an airtight vial. The slurry-solvent mixture was mixed for 10 min with a wrist-action shaker to partition the diesel fuel components to the solvent phase. A 10 ml portion of the solvent was then transferred into a clean glass-barrel syringe. The solvent was filtered through a 0.5 mm TeNon membrane filter (Millipore Millex-SR 0:5 m /lter unit; Bedford, MA) to remove particulates and through a sodium sulfate cartridge to remove water. Finally, a 2-ml sample of the filtrate was collected for analysis.

A gas chromatograph (GC) (Hewlett-Packard model 5890 T gas chromatograph with autosampler model 7673; Palo Alto, CA) with a capillary column (Supelco PTE-5TM, 30 m, 0:32 mm diameter, 0.25-_m /Im thickness; Bellefont, PA) and a Name ionization detector was used to detect and quantify the TPH. The GC was standardized using standards of refined No. 2 diesel fuel. The GC was operated with the helium carrier gas Now rate at 19.0 cm/s, column inlet pressure at 5.7 psi, inlet temperature at 300°C, and an oven temperature program of40 °C (held 13 min) to 260°C (held 10 min) at 8°C/min. The total area counts from TPH analyses were used to calculate the percent degradation of TPH under each condition compared to corresponding time zero samples under each condition.

b) Pah Analysis And Clean-Up Of The Extracts

The extracts in all cases, were concentrated to 2–3 ml using a rotary evaporator and then to 1ml under a stream of nitrogen.

The extracts were passed through a mixed silica column to remove co-extractive substances. The column

2011

was packed at the bottom with cotton wool and then filled with 15 g of activated silica. 1 cm ofsodium rinsed with sulfate was added at the top of the column, the column was 30 ml of DCM and 30 ml of n-hexane.

VII. RESULTS AND DISCUSSION

Slurry-phase biodegradation experiments were performed to investigate the remediation of PAHand TPH contaminated soil.

The SS-SBR was operated with a 14days cycle. Hydraulic retention time of 60 days was achieved by replacing 900 mL of the slurry volume every two weeks. TPH concentration at the end of each cycle is shown in Figure 1. TPH concentrations were reduced from 67.5 g/kg in the feed slurry to 2.7g/kg after treatment in the SS-SBR. This represents a removal efficiency of 95% (Fig1). Rates of TPH removal in SS-SBR showed a considerable decrease at first two weeks of operation

Also Fig. 2 shows the decrease in time removal efficienty of TPH in slurry-phase bioreactor treatments with 60 days HRT of the SBR.

But the concentration of pahs in the external sample could not be detected because it was very low.

VIII. CONCLUSION

The analyzes show that SS-SBR have a good ability for removing the petroleum and PAHs contaminated Soil.

In this process at the end of 60 days HRT the concentration of TPH is decreased from 67500 mg/kgdrysoil to 3003 mg/kgdrysoil that have removal efficiency of 96%

Also the analyze of low concentration of	PAHs
with Clean-up of the extracts can not practicable.	

Soil constituent	Measure d value					
Solids concentration (%w/v)	10					
Slurry diesel fuel (mg/kg)	67500					
Naphthalene concentration (mg/kg)	250					
Pyrene concentration (mg/kg)	250					
рН	7.6					
CFU (107/g soil)	9					

Table 1 : Soil content

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Figure 2: TPH removal efficiency during 90 days HRT

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Global Social and Economic Impact on The use of Biofuels and Recomendations for Sustainability

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Abstract - Biofuels currently represent a potential source of renewable energy. As well as that could lead to major new markets for farmers. However, only some of the current biofuel programs are feasible, and most involve high social costs and environmental ironically. The economic, environmental and social impacts of biofuels are widely debated and needs to be carefully assessed before extending public support to programs of biofuels on a large scale. The country strategy on biofuels should be based on a thorough assessment of these opportunities and costs in the medium and long term. One factor to consider is that oil reserves will run out, experts say, in fifty years. This article presents the social and economic impact of biofuel production in industrialized countries and developing countries that are or could become, efficient producers in export markets and profitable new.

Keywords : Biofuels, biomass, renewable energy, fossil fuels. GJRE-B Classification : FOR Code: 090201

GLOBAL SOCIAL AND ECONOMIC IMPACT ON THE USE OF BIOFUELS AND RECOMENDATIONS FOR SUSTAINABILITY

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Global Social and Economic Impact on The use of Biofuels and Recomendations for Sustainability

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Abstract - Biofuels currently represent a potential source of renewable energy. As well as that could lead to major new markets for farmers. However, only some of the current biofuel programs are feasible, and most involve high social costs and environmental ironically. The economic, environmental and social impacts of biofuels are widely debated and needs to be carefully assessed before extending public support to programs of biofuels on a large scale. The country strategy on biofuels should be based on a thorough assessment of these opportunities and costs in the medium and long term. One factor to consider is that oil reserves will run out, experts say, in fifty years. This article presents the social and economic impact of biofuel production in industrialized countries and developing countries that are or could become, efficient producers in export markets and profitable new.

Keywords : Biofuels, biomass, renewable energy, fossil fuels.

I. INTRODUCTION

Biofuel is the term which is called to any type of fuel derived from biomass, refers to any organic matter of recent origin that has been derived from animals and plants as a result of photosynthetic conversion process, the biomass energy derived from plant and animal material such as wood from forests, residues from agricultural and forestry processes, industrial waste, human or animal (Hernández and Hernández, 2008).

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Biofuels currently represent a potential source of renewable energy that could also generate major new markets for agricultural producers (Hernández and Hernández, 2008, p.15). However, only some of the current biofuel programs are feasible, and most involve high social costs and environmental ironically. The economic, environmental and social impacts of biofuels are widely debated and needs to be carefully assessed before extending public support to programs of biofuels on a large scale.

The fuels of biological origin can replace part of the traditional fossil fuel consumption, such as oil or coal. Applying agricultural techniques and strategies appropriate processing, biofuels can provide emissions savings of at least 50% compared to fossil fuels such as diesel or gasoline (Hernández and Hernández, 2008, p.17). In addition, biofuels are produced from agricultural crops, which are renewable sources of energy.

A disadvantage in the production of these fuels has been rising for example, food prices, increased competition for land and water, and deforestation. When using agricultural land for direct cultivation of biofuels, rather than use only the remains of other crops, has begun to produce an effect of competition between food production and biofuels, resulting in an increase in the price of the first (Hernández and Hernández, 2008).

A key step in maximizing opportunities and regional comparative advantages, is to follow the procedures for environmental impact assessment, which are key instruments for decision making. The main impacts are related to increases in demand for inputs, resources and energy, with the potential risks to water quality and habitat conservation (Stachett, Rodrígues, Aparecida, Buschinelli, and Ligo, 2007).

One advantage is related to environmental preservation, any effective path leading to a reduced consumption of nonrenewable energy collides with the same difficulty: the decrease of the gain or extraordinary profits, which would negate the essence of a free market. The free market "can" help innovate something to sell (eg biofuels) that will help "keep", however the actual act of environmental preservation kills profits (Recompensa, Días, Zabala, and Ramos, 2008).

The purpose of this paper is to show the advantages and disadvantages in the use of biofuels,

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based on research of different authors and the social and economic impact of biofuel production in industrialized countries and developing, which could reach to be efficient producers in new export markets and profitable. This article is distributed as follows: Section 2 considers the current situation in the social and economic impact of biofuel production in industrialized countries and developing countries; section 3 presents the methodology, Section 4 the results, with advantages and disadvantages of using biofuels in developed and developing, and finally in Section 5 the conclusion, which presents the potential benefits to using biofuels.

II. STATE OF THE ART

a) Current status of biofuels

The world is facing a massive global campaign, which aims to include in the fastest possible way different raw materials such as sugar cane, sovbeans. corn, rapeseed, sugar beet, etc., The production of biofuels as perfect substitutes petroleum derivatives. The main justifications found for this phenomenon are based on global warming and environmental pollution. The 1st generation biofuel specific crops used as raw materials, the most widely publicized are biodiesel and bioethanol. The latter represents more than 90% of all biofuels used today in the world. In Brazil, Sweden and the United States there are 6 million vehicles on the road that can accept mixed ethanol / gasoline up to 85%. The processing steps are different depending on the source of carbon and the technologies used in 1st generation processes are simpler than those of the 2nd processes and their production and investment costs are lower (Chauvet and González, 2008).

Figure 1 shows schematically the main stages to produce ethanol from sucrose (cane, beet, etc.), Starch (corn, wheat, tubers, etc.) And lignocellulosic residues (straw, agricultural residues and industrial, bagasse, etc.). The characteristics of lignocellulose offers major technical challenges, which increases the



Figure 1 : Main stages to produce bioethanol

cost of production and investment technologies for the production of biofuels 2nd generation are under development in the world, and is expected to dip sensitive in both items in the medium and long term.

Table 1 shows the variation in the cost of bioethanol production 1st generation according to the carbon source and feedstock used (Chauvet and González, 2008).

Source of carbon	Crops	Efficiency (l/ton of crops)	Efficiency (Vha)	Production cost (USD/l	Country
Sucrose	Beet (juice)	100	7000	0.48	European Union
	Cane (juice)	70 - 85	6000	0.21	Brazil
		10	590	0.32	India
	Cane (molasses)	10	730	0.23-0.37	Mexico
	Sorghum	56-90	2500-4000		Sweden
Starch	Corn	400	3000	0.29-0.37	United States
	Wheat	340	2700	0.62	European Union
	Corn/Wheat	285		0.59	United States
Cellulose	Bagasse (cane)	55	3850	0.8	Chile

Table 1 : Main raw materials for ethanol

The differences between the energy that wants to get today's agriculture and energy contained in fossil fuels (oil, natural gas and coal) which represents 80% of the energy consumed in the world, the first is obtained as a result of photosynthesis : sun, water and nutrients that are purchased each year to crops, but fossil energy has the same origin but with the difference that the result of saving of photosynthesis produced over millions of years. Intention now is to replace all fossil fuel consumption (oil, natural gas and coal) using biofuels, which has a set of specific such as: a) high fossil energy consumption, b) the need to use large farms and concentration land c) intensive use of technologies and machines, d) large-scale environmental damage, e) high concentration of capital (Recompensa, Días, Zabala and Ramos, 2008).

The key to the economics of biodiesel production is in the raw materials used. In Colombia there have been several investigations at laboratory and pilot plant in order to obtain biodiesel from different raw materials such as palm oil, castor oil, frying oils and byproducts of the poultry industry. Castor oil belongs to the raw materials considered strategic for the production of biodiesel in the country. With regard to diesel engines, biodiesel, given the technical advantages, strategic and environmental features, is the best alternative to replace partially or totally to petroleum diesel fuel (Benavides, Benjumea and Pashova, 2007).

Biodiesel has achieved great interest as an alternative source of energy, as it has many attractive features: non-toxic, biodegradable, nonflammable, technically viable and economically competitive. In Medellin, Colombia was modeled and simulated a membrane bioreactor using an enzyme catalyst Candida Antarctica lipase for the production of biodiesel from palm oil and ethanol. The result was that the membrane reactor with immobilized enzymes is the best option for the production of biodiesel. Not only because it achieves high conversions, but also because it minimizes the residence time, it also shows the simultaneous separation of reactants and reaction products (Solano, Moncada, Cardona and Simón, 2008).

United States of America imports oil from different countries, so that its influence is global, both in the real economy and financial markets. From the supply side, oil-producing countries are in conflict zones and unstable, so it records a negative impact on international financial markets. The difficulty of projecting the price of oil, uncertainty in the estimation of future prices is one of the main points of the Agenda (international energy) despite the perception of high price insensitivity to bringing the complaint. On the other hand, specifically the United States seeks an increase in research investment in clean energy technologies and alternative fuel production (De Paula and Cristian, 2009).

It should be stressed that within this strategy, biofuels are meant to be part of the diversification of energy demand, such as with wind and solar. Given these energy programs, both U.S.A and European Union have increased their production volumes of biofuels each year. At the regional level Brazil is inserted internationally as a producer of biofuels, with a clear objective: to capture markets that require a demand for this type of energy above its level of production. Brazil is the world's largest producer of ethanol, from the use of sugar cane as feedstock, sharing leadership with the United States, which is produced from corn. Brazil, in addition to producing ethanol, biodiesel produces (De Paula and Cristian, 2009).

In Brazil, the Federal Government established that from 2008, the biodiesel should be added to diesel at 2% and from 2013 the percentage increased to 5%. For its part the European Union states that by 2010 all diesel fuel dispensed in Europe will contain 10% biodiesel (Aimaretti, Intilángo, Clementz and Yori, 2008). In the case of Argentina, are developing some points of the agricultural sector, from which it extracts the raw material for biodiesel: soybeans. To make feasible the alternative fuel business, it was necessary for soybean crops are grown in abundance in the country. In addition to this increase in yield for soybeans, another feature of the Argentine agricultural sector is that it has a highly competitive oil industry worldwide. In Argentina there are sustainable and unsustainable practices in agriculture. But the truth is that the challenges exist, and it should be noted that what is at stake is the strategic natural resource: the "soil" (De Paula and Cristian, 2009).

The bounded oil reserves and the need to reduce environmental pollution intensified the development of renewable fuels like biodiesel. In Argentina, the use of glycerol obtained as a byproduct of biodiesel production, is the key advantage as it provides added value to a low-cost feedstock, reducing the final cost of biodiesel produced, achieving an economic benefit (Aimaretti, Intilángo, Clementz and Yori, 2008).

In the case of Mexico, in 2006 began the construction of two ethanol plants in the state of Sinaloa. The argument for this policy is to dispose of corn production in the region to the niche market covering the states of California and Arizona in the United States, the two projects involve an investment of 85 million dollars and treated some 335 thousand tons of corn and sorghum. The benefits provided by the Sub-Objective direct income support to the account for the states of Sinaloa, Sonora, Tamaulipas, Chihuahua and Baja California, in 2004, with 62% of the tonnes supported, and in 2005 with 72%. Sinaloa has been the most benefited by concentrating 40% of subsidized tons nationwide in 2004, and 35.5% in 2005. The product has received more support is corn (Chauvet and González, 2008).

The politics of ethanol can have a significant impact on corn prices, causing costs to soar and may also increase the inefficiency of agricultural subsidies and vice versa. Production costs of ethanol from corn in the U.S. are very high. The gap between the intersection of the supply curve of ethanol and oil prices create large costs that can harm all the external benefits (Gorter and Just, 2010).

III. METHODOLOGY

Choose the topic to develop this article was based on the current problem: **the preservation of the environment**. Several points are factors in our research, given that biofuels currently represent a potential source of renewable energy, considering the volatility of international oil prices (energy resource of excellence) and that oil producing countries are in conflict zones and unstable , representing a negative impact on international financial markets (De Paula and Cristian, 2009).

The methodology used to develop research on the advantages and disadvantages in the use of biofuel, the social and economic impact in industrialized countries and developing, was performed based on descriptive research (Medina, 2007) and (Hernandez, Fernandez and Baptista, 2010, p.80), making an initial search process (data collection), collection (sampling), analysis of information (variables) and results in order to present an overview of the topic research.

The methodology undertaken for this research can be summarized in the following points:

- 1. Data capture
- We performed an initial search procedure in scientific databases:
 Springer, Emerald, Wiley, Oxford Journals, World
- Scientific, Redalyc.b. The search criteria were based on key words: biofuels, biomass, renewable energy, fossil fuels, etanol and diesel.

2. Sampling

- a. In approximately 30 articles read were selected that had the most relevant and appropriate to the subject develops, and we choosing a total of 16 articles, which can be found in the references.
- 3. Information analysys

a. The information collected, carefully analyzed, following four main variables:

- Variable 1: Developing Countries.
- Variable 2: Industrialized countries.

- Variable 3: Benefits of the use of biofuels (point of view social and economic)
- Variable 4: Disadvantages of the use of biofuels (point of view social and economic)
- 4. Results
- a. Based on the descriptive research and the variables used to analyze the information (research articles), provides the results of research that are the basis for the conclusions.

In Figure 2, you can see the applied methodology.





IV. RESULTS

The results obtained in research on the advantages and disadvantages in the use of biofuel, the social and economic impact in industrialized countries and developing countries, are described in Table 2.

Variable 1: Developing countries	Variable 2: Industria lized countries	<i>Variable 3: Benefits of the use of biofuels (point of view social and economic)</i>	<i>Variable 4: Disadvantages of the use of biofuels (point of view social and economic).</i>
×	~	✓ The development of alternative energy, the progress in the investigation of second- generation biofuels and to promote greater use of biofuels, are just only a few points to follow in developed countries (De Paula and Cristian, 2009).	✓ Focus on production: the location of the sites are in countries that in recent years have demonstrated high legal uncertainty and unpredictability policy and regulatory (De Paula and Cristian, 2009).
Mexico		✓ In 2006, began the construction of two ethanol plants in the state of Sinaloa. The argument for this policy is to dispose of corn production in the region to the niche market that includes the states of California and Arizona, United States (Chauvet and González, 2008).	 The transportation costs of corn produced in Sinaloa to consumption centers in the south are high, no less incongruous than the volumes of corn destined for ethanol production when the country is importing, but more disturbing and scandalous is to subsidize the business of a few producers, such as the social group is supporting an activity which is not profitable and also is exported (Chauvet and González, 2008). Mexico as producer and exporter of oil, the renewable energy research is not their priorities (Chauvet and González, 2008).
Developed and part emerging e China ar	countries icularly conomies nd India	✓ Concentration and demand growth in developed countries and emerging economies (De Paula and Cristian, 2009).	✓ Financial speculation and uncertainty, The main reason for high prices is the growing perception in the markets, in the future the offer maybe will not be sufficient to satisfy demand. (De Paula and Cristian, 2009).
	United States of America	✓ Rationalize energy consumption in homes, buildings, businesses, cars and public transport so reduction contamination (De Paula and Cristian, 2009).	 Agricultural subsidies in the United States of America, the policy statement that ethanol reduces the tax costs, can still not be confirmed. But the inefficiency of production subsidies for corn and ethanol are still worrying, however ethanol production (and consumption) is constant, as determined by the government (Gorter and Just, 2010). The increase in ethanol prices increases also the corn price, because it competes for the land with other crops (Gorter y Just, 2010).
	Europea n Union	 Direct their efforts to establish an energy diversification of oil supply. Establish privileged partnerships with producer countries (Russia), transit (Algeria) and develop alternative energy (De Paula and Cristian, 2009). 	
✓	V	 Generation of second-generation biofuels obtained by biomass that can be obtained not necessaryly by inputs for food or compete with them (Chauvet and González, 2008). 	✓ The reason that has stopped its application are the technical difficulties that they present, the estimated levels of investment and high production costs for obtain biofuels (Chauvet and González, 2008).
Brazil		 Capture of markets that require a demand for this type of energy above its level of production (De Paula and Cristian, 2009). The integration of technological development and pro-activity of all team members is crucial for the development of flexible fuel (De Souza, Sin, Nigro and Lima 2009). Production of biofuels in the world is profitable because of subsidies and incentives for renewable energy. In Brazil, the prices to be sustainable levels of profitability of ethanol production from sugar cane is profitable when a barrel of oil 	✓ The high cost of castor oil and the relatively low level of technology, is still present in the production areas of Brazil and are the main obstacles to actually make feasible the production of biodiesel (Stachett, Rodrígues, Aparecida, Buschinelli, and Ligo, 2007).

		 ranges from 45 to 50 USD (Chauvet and González, 2008). ✓ The local arrangements for the production offer the best options for promoting sustainable development and avoiding environmental degradation risks (Stachett, Rodrígues, Aparecida, Buschinelli, and Ligo, 2007). ✓ The socio-environmental impact and the intensification of production is reflected favorably on the expectations of farmer training, income generation, improved land value, and improving opportunities, training, and job quality indicators (Chauvet and González, 2008).
✓ 	✓	 Participation of governments, some governments have provided incentives and financing to develop for new technologies with the aim of achieving a sustainable economy (Hazy, Torras and Ashley, 2008). <i>Tariff</i>, Biofuel production in industrialized countries has been developed under the protection of high tariffs, while subsidies granted to producers (Hernández and Hernández, 2008). Participation of governments, some governments, some financing to develop for new technologies with the aim of achieving a sustainable economy (Hazy, Torras and Ashley, 2008).
	Japan	 Being a buyer of Brazilian products but wants to ensure that the supply of the product will not be interrupted (Recompensa, Días, Zabala and Ramos, 2008). In countries where the rights over mineral resources are privately owned (such as in the United States of America and Canada), these resources can be controlled via property rights and that situation is a disadvantage for Japan, because for biofuels can be apply the same situation (Recompensa, Días, Zabala and Ramos, 2008). In the rest of the world, the minerals can be easily controlled through exclusive contracts with governments (Recompensa, Días, Zabala and Ramos, 2008).
Colombia		✓ The simulation of the production of biodiesel from palm oil using an immobilized lipase as biocatalyst (Candida Antarctica) in a membrane bioreactor, is the best option for biodiesel production (Solano, Moncada, Cardona and Simón, 2008).
Argentina		 The use of glycerol obtained as a byproduct of biodiesel production, is the key advantage as it provides added value to a low-cost in raw material, reducing so the final cost of biodiesel produced, achieving an economic benefit (Aimaretti, Intilángo, Clementz and Yori, 2008). Improving fuel quality through the use of additives, significantly reduces the environmental pollution produced, helping to meet stringent environmental regulations that apply today (Aimaretti, Intilángo, Clementz and Yori, 2008).

Table 2: Results of the advantages and disadvantages of using biofuels.

IV. CONCLUSIONS

In the production of biofuels, if we take the example of ethanol and other biofuels in Brazil, this attempted solution to our energy problems are being controlled through ownership or lease of land to produce raw materials and /or the Intellectual property (proprietary processes of distillation, proprietary microbes that turn sugar substances, etc.), the point is that governments create more problems, no matter that biofuels provide a low energy return on investment, the depletion of fertile soils , pollution and energy, what matters is that governments can do a lot of money (Recompensa, Días, Zabala and Ramos, 2008).

In relation to environmental preservation any effective path leading to a reduced consumption of nonrenewable energy collides with the same difficulty: the decrease of the gain or extraordinary profits, which would negate the essence of free market (Recompensa, Días, Zabala and Ramos, 2008).

First generation biofuels such as ethanol production is one of the more traditional industrial applications in all respects, the requirements of scale, costs and improving efficiency in fuel use almost inevitably point towards the use of transgenic crops, which further complicate the national debate. The second-generation biofuels are the benefits that can be obtained from biomass that is not appropriated for food supplies or compete with them, such as agricultural harvests, industrial and urban waste, so there is also rivals for the use of natural resources. Cost-effective production of ethanol obtained from lignocellulose via enzymatic hydrolysis would increase the variety and availability of basic material and, therefore, expand the production of biofuels without compromising food security and sovereignty (Chauvet and González, 2008).

The trend is towards second generation biofuels, since the use of crops for biofuel does not replace the energy needs of low-cost oil achieved today and its derivatives. Hence the importance for a country like Mexico, at this time, to allocate resources for Research & Development for 2nd generation biofuels. For the July 24, 2007, the administration reported that "the federal government will not support projects and ethanol plants carrying corn as raw material, since it has the priority of this cereal are not distracted from their destinations in human food or animal nutrition " (Chauvet and González, 2008).

The management of strategic natural resource "soil" presents a challenge because there is no quantification of damages in the case of unsustainable practices (De Paula and Cristian, 2009).

Is important to link the sustainability standards for biofuels policies, the most logical approach would be to punish or compensate the use of ethanol. Concerns about land use for biofuels can be contracted with the overall theme of global climate change in general. Agriculture has considerable potential for the mitigation of greenhouse gases, especially in developing countries. The impact of biofuel policies in the development and adoption of new technology should be examined. Biofuel policies may be needed to ensure the market in order to exploit the benefits of learning "doing and using" dynamic benefits and innovation of new technologies (Gorter and Just, 2010).

The production of biofuels is part of a competitive strategy in the global market, mainly for developed countries like the United States. The problem created by the rising international food prices exacerbated a structural agricultural situation in Mexico, where he has abandoned the priority to have an auto policy in food supply and insufficient support investment in the field (Merino and Castañeda, 2008). Bioenergy generation is not the panacea for poverty in the Mexican countryside, nor would solve the problems of the country's economy in general. You can create a problem socioeconómicoambiental, not planned in multidisciplinary production, use and exploitation (González, 2009).

a) Recommendations

For the use of biofuels actually be an advantage in the economic, social and environmental care, should take care of the following (Serna, F., Barrera, L.):

- 1. Biofuels policy : The success of biofuels depends on their use mandatory, tax facilities, subsidies provided by the State, pricing to consumers, the recognition of the rights of workers and the thousand and one ways develop from the rural communities and effective use of their land
- 2. Grants : The production of biofuels in the world is profitable because of subsidies and incentives for renewable energy, but must ensure that these subsidies are allocated to the most vulnerable
- **3. Soil use**: The problem of land use represents the medium and long term environmental liabilities is hardly balanced with assets derived from the production of biofuels.
- 4. Second generation biofuels : They should turn the attention to second generation biofuels, the advantages is that they can be obtained from biomass that is not appropriated for food supplies or compete with them and protect this soil use.
- 5. Research & Development: Both developed and developing nations must pay attention to the benefits associated with research and development, adopt new technologies, resulting in improved environmental heritage and obtaining economic benefits in the development of biofuels.
- 6. Profit vs. environmental benefits : The ambition for the profits do not should exceed the benefits of environmental preservation. In relation to environmental preservation any effective path leading to a reduced consumption of nonrenewable energy collides with the same difficulty: the decrease of the gain or extraordinary profits.

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30

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INDEX

Α

Ammonium \cdot 14, 15, 19, 20 assumptions \cdot 4

В

biodegradation · 33, 34, 37 biodiesel · 41, 42, 43, 44, 47, 49, 53, III biofuel · 39, 41, 44, 45, 51 Biofuels · 39, 41, 43, 45, 46, 49, 51, 52, 53 biomass · 39, 44, 46, 51, 52 brain · 24, 26 Bromide · 14, 15, 19, 20

С

carbon \cdot 14, 24, 33, 41 Chihuahua \cdot 44 Colombia \cdot 42, 49 Comparison \cdot 26, 28, 30 Concentration \cdot 16, 46 concentrations \cdot 14, 33, 35, 37 considered \cdot 14, 22, 26, 30, 42 consumption \cdot 14, 16, 19, 39, 40, 42, 46, 47, 51, 52

D

Detector \cdot 33 Development \cdot 51, 52, 53 dynamic \cdot 22, 51

Ε

emissions · 14, 15, 18, 20, 39 Engineerig · 39 ethanol · 14, 15, 16, 17, 18, 19, 20, 41, 42, 43, 44, 46, 47, 51 Ethanol · 14, 16, 18, 20 Experimental · 16, 25, 30, 32 Exponential · 23

F

flammability · 17 fuel · 14, 15, 16, 17, 18, 19, 20, 33, 36, 37, 39, 42, 43, 46, 49, 51

G

Gasoline · 16 geometric · 1, 5, 9

Η

horizontal · 9

I

industry \cdot 22, 42, 43 insufficient \cdot 52

J

justified · 26

Κ

kinematic \cdot 24

L

Laboratory \cdot 33, 35, 37 literature \cdot 7, 22, 24 location \cdot 1, 4, 7, 12, 46 logarithmic \cdot 25 lubrication \cdot 24

Μ

management \cdot 14, 20, 51, 53, III microorganisms \cdot 33, 34, 35 multidisciplinary \cdot 52

Ν

Neural · 24, 30, 31, 32 nonrenewable · 40, 51, 52

0

occurrences · 9, 11, 12

Ρ

passenger \cdot 1, 4, 7 penetration \cdot perceptron \cdot petroleum \cdot 36, 37, 41, 42 Petroleum \cdot photosynthesis \cdot precursor \cdot provide \cdot 14, 33, 34, 35, 36, 39, 51

R

Randomly \cdot 3 regression \cdot 22, 23, 24, 25, 26, 28, 30 relationship \cdot 22, 25 reserves \cdot 39, 43

S

simulation · 1, 3, 4, 5, 7, 9, 23, 49 Smokeless · 20 software · 3, 7 Solano · 43, 49, III sovereignty · 51 stabilize · 14, 15, 19, 20

T

technical · 1, 12, 14, 41, 42, 47 technology · 33, 47, 51 temperature · 14, 16, 17, 18, 22, 24, 25, 36 trajectories · 7, 9, 12

V

velocity · 1, 5, 7

Ζ

Zabala · 40, 42, 49, 51, 53



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