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¹ CFD Analysis of Intake Valve for Port Petrol Injection SI Engine

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6 Abstract

This paper presents the supersonic combustion of hydrogen using ramp based injector with 7 two-dimensional turbulent non-premixed combustion model. The present model is based on 8 the standard k-epsilon (two equations) with standard wall functions which is P1 radiation 9 model. In this process, a PDF (Probability Density Function) approach is created and this 10 method needs solution to a high dimensional PDF transport equation. As the combustion of 11 hydrogen fuel is injected from the ramp based injector, it is successfully used to model the 12 turbulent reacting flow field. It is observed from the present work that, the maximum 13 temperature occurred in the recirculation areas which is produced due to shock 14 wave-expansion and the fuel jet losses concentration and after passing successively through 15 such areas, temperature decreased slightly along the axis. From the maximum mass fraction of 16 OH, it is observed that there is very little amount of OH around 0.013 were found out after 17 combustion. By providing ramp, expansion wave is created which cause the proper mixing 18

¹⁹ between the fuels and air which results in complete combustion.

20

Index terms— Mach number, CFD, combustion, hydrogen fuel, non-premixed combustion, scramjet, standard k-epsilon turbulence model, standard wall functions, steady s

23 1 Introduction

he engine cycle of typical internal combustion engines consist of four consecutive processes as intake, compression, 24 25 expansion (including combustion) and exhaust. Of these four processes, the intake and compression stroke is one 26 of the most important processes which influences the pattern of air flow structure coming inside cylinder during intake stroke and generates the condition needed for the fuel injection during the compression stroke. As a result 27 of the high velocity inside the internal combustion engine (ICE) during operation, all in cylinder flows are typically 28 turbulent. The exception to this is the flows in the corners and small crevices of the combustion chamber where 29 the close distance of the walls diminished out turbulence. Heat transfer, evaporation, mixing and combustion 30 rates all increase as engine speed increases. This increases the time rate of fuel evaporation, the mixing of the fuel 31 vapor and air as well as combustion process. Fluid motion within the engine cylinder is one of the major factors 32 that control the fuelair mixing and combustion process in spark ignition engines. It also has a significant impact 33 on heat transfer. Both the bulk fluid motion and the turbulence characteristics of the flow are essential to produce 34 the homogeneity structure of air flow come into cylinder. Generally, the initial in-cylinder flow pattern is set up 35 36 by the intake process and then be substantially modified during compression process. The small-scale mixing 37 of turbulence with compressible flows is represented by the turbulence kinetic energy and turbulence kinematic 38 viscosity .Turbulence inside the cylinder is high during the intake and then decreases as the flow rate slows near bottom dead centre (BDC). It increases again during the compression stroke as swirl, squish and tumble increase 39 near top dead centre (TDC) [1]. Intake generated swirl usually persists through the compression, combustion, 40 and expansion stroke and it can greatly enhances the mixing of air and fuel to give a homogeneous mixture in the 41 very short time. It is also a main mechanism for very rapid spreading of the flame front during the combustion 42 process [2]. Many researchers worked in this area via experimental as well as computational to explorer the 43 phenomenon of the incylinder flow of Internal Combustion Engine. Some of them are cited here. B. Reveille 44

and A. Duparchy [3] worked on 3D CFD analysis of an abnormally rapid Combustion phenomenon in downsized 45 gasoline engines. This paper has focused on a particular abnormally rapid, yet non destructive and seemingly 46 stable combustion phenomena which have been identified on low speed mid to high load operating points when 47 performing aggressive downsizings on various engines. Franz X. Tanner & Seshasai Srinivasan [4] worked on 48 49 CFD-based optimization of fuel injection strategies in a diesel engine using an adaptive gradient method. A gradient-based optimization tool has been developed and, in conjunction with a CFD code, utilized in the search 50 of new optimal fuel injection strategies. The approach taken uses a steepest descent method with an adaptive 51 cost function, where the line search is performed with a backtracking algorithm. Vijaya Kumar Cheeda, R. Vinod 52 Kumar, G. Nagarajan [5] worked on design and CFD analysis of a regenerator for a turboshaft helicopter engine. 53 In this paper a continuous heat transfer regenerator for a turboshaft helicopter engine is designed suitably. The 54 regenerator effectiveness is assessed by the CFD tool CFX and evaluated the effectiveness and the pressure drop. 55 The predicted CFD results are in good agreement with experimental results. L. Li, X.F. Peng, and T. Liu [6] 56 worked on combustion and cooling performance in an aero-engine annular combustor. The investigation was 57 conducted to understand the characteristics of the flow, combustion, cooling performance and their interaction in 58 an aero-engine combustor. The conservation equations and Eddy-dissipation combustion model were employed 59 for solving the flow, heat transfer, and combustion in the entire combustor. The reliability of the simulation 60 61 was demonstrated by comparing calculated combustor exit temperature distributions with profiles of the rig-62 test measurements. Christian Hasse, Volker Sohm, and Bodo Durst [7] worked on Numerical investigation of cyclic variations in gasoline engines using a hybrid URANS/LES modeling approach. The study investigates the 63 feasibility of using the SST DES model to predict cycle to cycle variations in internal combustion engines and the 64 effect of cyclic variations in engines and their root causes including the major flow patterns. Wendy Hardyono 65 Kumiawan, Shahrir Abdullah and Azhari Shamsudeen [8] worked on CFD study of cold-flow analysis for mixture 66 preparation in a motored four-stroke direct injection engine. In this study, the CFD simulation to investigate 67 the effect of piston crown to the fluid flow field inside the combustion chamber of a four-stroke direct injection 68 automobile engine under the motoring condition is presented. The analysis is focused on study of the effect of the 69 piston shape to the fluid flow characteristics the result obtained from the analysis could be employed to examine 70 the homogeneity of airfuel mixture structure for better combustion process and engine performance. Andras 71 Kadocsa, Reinhard Tatschl and Gergely Kristof [9] worked on analysis of spray evolution in internal combustion 72 engines using numerical simulation. This paper summarizes results of research about a new approach of spray 73 74 formation calculations. Using a primary breakup model for separately describing the initial liquid disintegration 75 of injected liquid based on the flow properties stemming from a previous calculation of injector nozzle flow gives a better prediction capability and suits the new needs of advanced combustion systems such as HCCI engines or 76 various forms of split injection. Toyoshige Shibata Hideo Matsui, Masao Tsubouchi and Minoru Katsurada [10] 77 worked on Evaluation of CFD Tools Applied to Engine Coolant Flow Analysis. This paper presents the results of 78 test application of some automatic mesh generation tools to the CFD calculation of coolant flow, and compares 79 the functional characteristics and features of these tools. The paper also discusses coolant flow items that can 80 be evaluated by CFD analysis and the merits of applying CFD to these items. Semin, N.M.I.N. Ibrahim, Rosli 81 A. Bakar and Abdul R. Ismail [11] worked on In-Cylinder Flow through Piston-Port Engines Modeling using 82 Dynamic Mesh. This paper presents numerical study of three-dimensional analysis of two-stroke spark-ignition 83 cross loop-scavenged port. The objective of this study is to investigate the incylinder characteristics at motored 84 transient condition. The pressure on in-cylinder and intake port were collected and applied for validation with 85 numerical results for 1400 rpm. The three-dimensional modeling analysis was performed utilizing dynamic mesh 86 method. The prediction of distribution of in-cylinder pressure and mass fraction of gases function of crank angle 87 were discussed. The results shown that the relative error between experimental and numerical less that 2 %. 88 Helmut Doleisch [12] worked on simvis: interactive visual analysis of large and time-dependent 3d simulation 89 data. In this paper the major new technological concepts of the SimVis approach are presented and real-world 90 application examples are given. SimVis is a system for the graphical analysis of simulation data, built on a 91 new, cutting-edge technological approach for interactive visual analysis of large, multi-dimensional, and time-92 dependent data sets resulting from CFD simulation. S. M. Jameel Basha, P. Issac Prasad and K. Rajagopal [13] 93 worked on simulation of in-cylinder processes in a DI diesel engine with various injection timings. In this paper 94 an attempt has been made to study the combustion processes in a compression ignition engine and simulation was 95 done using computational fluid dynamic (CFD) code Fluent. An Axisymmetric turbulent combustion flow with 96 heat transfer is to be modeled for a flat piston 4-stroke diesel engine. The unsteady compressible conservation 97 equations for mass (Continuity), axial and radial momentum, energy, species concentration equations can express 98 the flow field and combustion in axisymmetric engine cylinder. Turbulent flow modeling and combustion modeling 99 was analyzed in formulating and developing a model for combustion process. R. Rezaei, S. Pischinger, P. Adomeit 100 and J. Ewald [14] worked on Evaluation of CI In-Cylinder Flow using optical and numerical techniques. In this 101 paper different port concepts for modern Compression-Ignition engines, usually quantities as the swirl level and 102 the flow coefficient are evaluated, which are measured on a stationary flow test bench. As additional criterion, 103 in this work, the homogeneity of the swirl flow is introduced and defined quantitatively. Different valve lift 104 strategies are evaluated using three-dimensional Particle Imaging Velocimetry in a stationary flow configuration 105 and transient In-Cylinder CFD simulation using both the Reynolds Averaged Navier Stokes equation and the 106 Large Eddy simulation approach. M.M.Noor1, K.Kadirgama1, R.Devarajan, M.R.M.Rejab, N.M.Zuki N.M. and 107

T.F.Yusaf [15] worked on Development of a High Pressure Compressed Natural Gas Mixer for A 1.5 Litre CNG-108 Diesel Dual Engine. In this paper Computational Fluid Dynamics (CFD) analysis software was used to study the 109 flow behavior of compressed natural gas (CNG) and air in a CNG-air mixer to be introduced through the air inlet 110 of a CNG-Diesel dual fuel stationary engine. Yasar Deger, Burkhard Simperl and Luis P. Jimenez [16] worked 111 on Coupled CFD-FE-Analysis for the Exhaust Manifold of a Diesel Engine. This paper aims to investigate the 112 thermo-mechanical behaviour of an exhaust manifold which has an active cooling system, the full water flow, 113 partial water flow (by 50% reduced cooling flow) and Vapour flow three cases of cooling analyzed. Fluid flow, 114 thermal heat transfer and stress analysis are coupled for each case using a oneway coupling approach. Selected 115 results given in form of temperature, stress and displacement distribution plots in this paper. The investigation 116 was focusing on potential structural optimization measures. Therefore some suggestions for design improvements 117 are presented also, which are presumably effective to reduce the temperature peaks and temperature gradients 118 and to ensure a longer service life for the exhaust manifold. Kihyung Lee, Choongsik Bae, and Kernyong Kang 119 [17] worked on the effects of tumble and swirl flows on flame propagation in a four-valve S.I. engine. The effects 120 of in-cylinder flow patterns, such as tumble and swirl flows, on combustion were experimentally investigated 121 in a four valve S.I. engine. Tumble flows were generated by intake ports with entry angles of 25 ? , 20 ? 122 and 15 ? . Inclined tumble (swirl) flows were induced by two different swirl control valves. The initial flame 123 124 propagation was visualized by an ICCD camera, the images of which were analyzed to compare the enflamed 125 area and the displacement of initial flames. The combustion duration was also calculated by the heat release analysis. B. Murali Krishna and J. M. Mallikarjuna [18] worked on Tumble flow analysis in an unfired engine 126 using particle image velocimetry. This paper deals with the experimental investigations of the in-cylinder tumble 127 flows in an unfired internal combustion engine with a flat piston at the engine speeds ranging from 400 to 1000 128 rev/min., and also with the dome and dome-cavity pistons at an engine speed of 1000 rev/min., using particle 129 image velocimetry and It is suggested in the paper to use the flat piston rather than dome, dome-cavity pistons 130 which are rather difficult to manufacture as far as tumble flows are concerned. B. Khalighi worked on Study 131 of the intake tumble motion by flow visualization and PTV [19]. The purpose of this work is to characterize the 132 in-cylinder tumbling flow generated by an engine head during the induction process using flow visualization and 133 PTV. The study was carried out for a 4-valve engine head with shrouded intake valves in special single cylinder 134 transient water analog. This shrouded intake valve configuration was used to obtain a prototypical "pure tumble" 135 flow suitable for fundamental combustion studies. K.M Pandey, S.N Pandey, and Bidesh Roy [20] worked on 136 numerical analysis to determine the effect of temperature on the intake generated swirl for port fuel injection 137 SI engine. Hence, for computational investigation for intake swirl within the engine, cold flow simulation will 138 provide faster computational result. In this study it was concluded that the temperature on various part of the 139 engine produces a very negligible effect on the intake swirl generation. Thus, we can see that very few works 140 have been done in field of determining the behavior of intake swirl red along the length of the engine cylinder. 141

142 **2** II.

¹⁴³ 3 Specification of the Si Engine

The engine considered for the computation analysis is a single-cylinder continuous type port fuel injection four stroke SI engine with cylindrical combustion chamber and single intake port and exhaust port. The computation analysis is performed at WOT maximum power condition. The specification of engine is listed in Table 1.

¹⁴⁷ 4 Poppet Intake Valve

A Poppet intake valve is used in the SI engine in which the computational analysis is performed. The dimensions of the Poppet intake valve are shown in the figure below:

¹⁵⁰ 5 Computational Domain and Boundary Conditions

The numerical formulation of the problem is incomplete without prescribing boundary conditions, which 151 correspond to the specific physical model. The specification of mathematically correct boundary conditions that 152 ensure the uniqueness of the solution, while being compatible with the physics at the boundaries, is not always 153 straightforward. Before arriving at the boundary conditions at various boundaries, we have to first identify the 154 solution/computational domain of the problem. The physical domain and computational domain usually differ. 155 However, the computational domain largely depends on the geometry of physical domain. The computational 156 157 domain boundary (truncated from the real boundary) along with appropriate boundary conditions should be 158 chosen in such a way that there is negligible change in the results with further increase in its size.

The computational domain shown in the figure 2 is a generalized one since, the analysis is performed at different crank angle during the suction stroke of the engine as result the distance of the piston from the engine head shown in the figure 2 by "B" also varies corresponding to the engine crank angle. The inlet boundary condition is assigned as mass flow inlet. Since the investigation is performed at 72 degree of the crank angle and at that instant the mass flow inlet of air is 0.01319 kg/sec for the computation.

II. Solid surface of the cylinder of the engine: -It is assigned wall boundary condition i.e. no slip condition on 164 the solid surface of the cylinder. The computation is performed with solid surface of the cylinder at a temperature 165 of 300 ? K for faster computational result [20]. 166

III. Outlet Boundary on the piston of the engine: -Outlet boundary is assigned the pressure outlet boundary 167 condition. For the investigation outlet pressure is taken as a static pressure of 0:935 bar. 168

IV. Discrete phase surface injection for injector: -In the computation domain the injector of the valve is assign 169 as discrete phase surface injection with fuel flow rate of 0.0011 kg/sec for the engine considered. 170 V.

171

Grid Independence Study 6 172

The resolution of the grid has a great quantitative impact over the results obtained. There exists a level of refining 173 of a computational domain beyond which there is no significant quantitative changes in the results achieved. The 174 computational domain at this level of refinement is said to enter the regime of grid independence. In the present 175 work maximum tangential velocity at a surface 9.18mm from engine cylinder head has been taken as the criteria 176 and the number of grid is refined until the required value is gained. For the simulation grid independence was 177

Result and Discussion 7 178

Computational result at 72 ? crank angle for the specified SI engine at various locations along the length of the 179 engine cylinder is shown below:- From the equation 1, it is clear that tangential velocity plays a vital role in 180 determining the intensity of swirl within the engine. 181

From the results of the computation analysis carried out at 72? crank angle with poppet intake valve, for the 182 specified SI engine it is seen that the surface at 9.18mm from engine cylinder head which is closer to the valve 183 shows higher tangential velocity at various location compared to the surface at 18.1mm and 28.8mm from engine 184 cylinder head which is at higher distance from the intake valve. 185

VII. 8 186

Conclusion 9 187

From this study the following it can be concluded that the surface which is closer to the poppet intake valve 188 shows higher tangential velocity at various locations compared to the surfaces which are at higher distance from 189

the intake valve i.e. the intensity of swirl decreases along the stroke length of the engine cylinder.

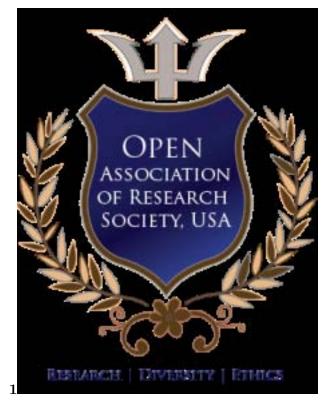


Figure 1: Figure 1 :

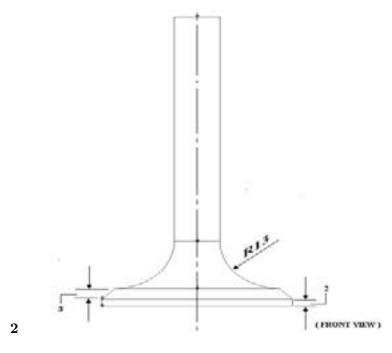


Figure 2: Figure 2 :

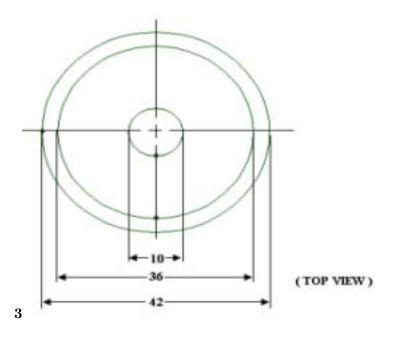
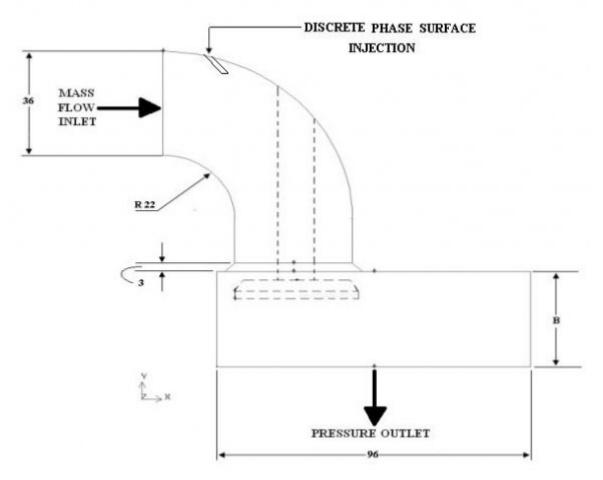
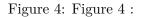


Figure 3: Figure 3 :



 $\mathbf{4}$



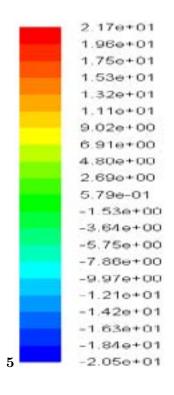


Figure 5: Figure 5 :

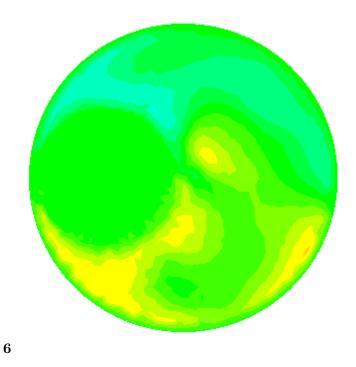


Figure 6: Figure 6 :

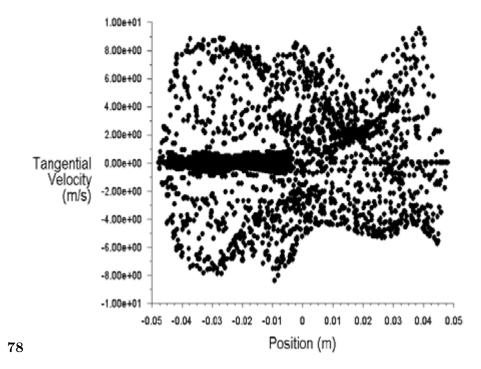


Figure 7: Figure 7 : Figure 8 :

1

 $\mathbf{2}$

calculation conditions	
Bore x stroke	95mm x 99 mm.
Compression ratio	9:1
Piston cavity	Flat.
Max power at WOT	$13.2~\mathrm{BHP}$ at 4950
	RPM.
Intake valve diameter 42mm	
Maximum intake	12mm.
valve lift	
Exhaust valve	64 ? BBDC.
opening	
Exhaust valve closure 5 ? ATDC.	
Intake valve opening	5 ? BTDC.
Intake valve closure	60 ? ABDC.
Fuel	C 8 h 18
III.	

Figure 8: Table 1 :

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(A)
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reached for 384876 cells and 82377 nodes as shown in table 2.
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Figure 9: Table 2 :

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