

# Vibrational Behaviour of a Quarter Car Travelling over Road Humps with Different Suspension Systems

Khalid Alnefaie

*Received: 13 December 2021 Accepted: 10 January 2022 Published: 23 January 2022*

---

## Abstract

Due to the unawareness of some vehicles' drivers to abide by the limited speeds, many authorities have had to set up road speed humps to calm down the vehicles flow, especially in densely populated areas. And as a result, bad vehicles ride comfort is produced from the suspension system. Therefore, researchers and car manufacturers were interested in improving the vibrational behaviour of the vehicle while traveling over humps. In this study, the vibrational behaviour of the vehicle was studied while traveling over different types of road humps using passive, semi-active and active suspension systems.

---

**Index terms**— vehicle ride comfort, quarter car model, road humps, vehicle stability, and vehicle vibrational behavior.

## 1 I. Introduction

uring the last century, the vehicle has become one of the basics of daily life. Wherever we are, the vehicle is considered as the companion of man in all parts of the earth. Wherever the human found the vehicle inherent to him. The vehicle is one of the ways to add more comfort and ease human life. Since the beginning of the production of vehicles, scientists and vehicle manufacturers have been interested in ride comfort as one of the most important factors in adding driving a pleasure. [1] Due to the unawareness of some vehicles' drivers to abide by the limited speeds, many authorities have had to set up road speed humps to calm down the vehicle's flow, especially in densely populated areas. And as a result, bad vehicle ride comfort is produced for the vehicle components. [2] Semi-active suspension is a type of vehicle suspension system in which the force generated by the damping is variable to achieve better ride comfort and reduce the amplitude of the shock amplitude of the generated vibrations. The damping force is varied depending on the input outgoing naturally changing road surfaces. The purpose of this system is to apply the adaptive active suspension using variable shock absorbers that produce variable damping force. The semi-active suspension system can be managed in a variety of control methodologies. One of these methods is a rather ideal technology referred to as the Skyhook control system . [3] As for the active suspension system, it is fundamentally different from other previous types, as it depends mainly on a control system that works to regulate the generation of additional power that is produced by an electrical or hydraulic actuator organized by a control algorithm based on the signals of the sensors indicating the road and driving conditions of the vehicle. In addition to the main suspension components; spring and damper; the active suspension includes the actuator to provide additional force to spring and damper forces that contribute to improving ride comfort. The active suspension is characterized by the generation of additional power from the actuator to reduce the impact of vertical forces generated by unexpected changes in road inputs. [4] There are two main types of humps, the short type which is known as bumps that are typically used to smooth lanes in low-speed areas such as school fronts and shopping mall parking lots. This type of bump is designed to force cars to travel at extremely low speeds less than 10 km/h. As for the other type of humps, it is to slow down traffic on a larger scale and is characterized by its large dimensions, relatively to the short type, and is used in the streets within the city to force cars over a range of 10-20 km/h. The humps usually lead to a sharp jolt in the car's suspension system, especially the short bumps, and it can reach severe damage to the suspension system if the driver tries to cross at speeds much greater than the established speed limits. It is necessary to design warning signs and lights before the hump to warn of the presence of a bump. There is a third type of bumps

46 called the cat-eye hump, which is often used as a warning sign of an emergency, and this variety of road humps  
47 significantly worsens the ride comfort . [5] To reach an optimal solution that guarantees the safety of driving on  
48 the roads inside the city, while obtaining an acceptable riding comfort, the car manufacturers tried to implement  
49 an intelligent system that is characterized by alignment in the suspension system to achieve the highest possible  
50 ride comfort. One of these systems is the active and semi-active suspension system. Therefore, the aim of this  
51 research is to study the vibrational behaviour of vehicle suspension system when the vehicle over humps using  
52 mathematical equations modelled in MATLAB Simulink. The research objectives are to create mathematical  
53 models for the vehicle and hence to build these models in MATLAB Simulink and then study to optimize the  
54 most used vehicle suspension system that gives the best ride comfort.

55 The road hump is an extension designed over the road to calm down the traffic flow. Many hump profiles are  
56 globally used. The circular hump is the most widespread one that is used on city roads. The circular hump is  
57 the most famous hump used in vehicle roads because of its design simplicity and its reasonable effectiveness. The  
58 circular hump is characterized by hump width and height. The recommended hump width is not less than 3-4 m  
59 while the maximum height is 10-15 cm. Recommended circular humps height is about 10 cm. Heights less than  
60 the assumed 10 cm will result in that the hump is not effective. Heights above 10 cm may cause severe damage  
61 to vehicles [1].

62 To force vehicle drivers to calm down the speed, there are several types of common road humps, such as  
63 speed bumps, speed humps, speed cushions, speed tables, and chicane. [2] Abdulmawjoud et al. [5] have studied  
64 the drivers' behaviour when the vehicle is travelling over three main types of standard humps, which are single  
65 circular hump, double circular humps, and trapezoidal hump. The traffic calm installed along the main roads of  
66 one of the cities was studied, and they found that the rate of decrease in the vehicle speed reached more than  
67 70% when the vehicles are travelling over the humps. It was noted that the trapezoidal hump causes a greater  
68 decrease in speed than the other species studied, with a decrease of approximately 80%. In terms of ride comfort,  
69 the worst ride comfort was recorded in the case of a single circular hump.

70 Pozuelo et al. [6] have presented theoretical and experimental study to investigate the vehicle vibrational  
71 behaviour when the vehicle is travelling over a circular hump. The main goal of the model and software that  
72 to introduce a prediction of the vertical dynamics of a vehicle when traveling over a hump using a half-car  
73 model. They also developed mathematical expressions to formulate the displacement behaviour resulting from  
74 the movement of the vehicle over the circular hump. The model signals are validated by comparing with the  
75 recorded experimental results of maximum vertical acceleration, maximum longitudinal pitch angle, maximum  
76 dynamic tire load of the front suspension, maximum dynamic tire of the rear suspension. The results showed  
77 that driving the vehicle over the hump leads to a severe deterioration in the ride comfort, as well as the stability  
78 parameters of the vehicle, especially at high speeds.

79 In another way, Mahmoud [7] presented the function of the circular hump in a simplified way, while he  
80 represented the rectangular hump as a function of the height and length of the hump and the speed of the  
81 vehicle. He presented the riding comfort factors as the suspension working space, the vertical body acceleration,  
82 and dynamic tire load as factors comparing the ride comfort and stability of the car on the road.

83 The suspension system of the vehicles is an important part of obtaining satisfactory ride comfort, as well as one  
84 of the components of the vehicle's safety requirement. A suspension system typically contains shock absorbers  
85 and springs. The shock absorbers compress and rebound with the help of springs when a force is applied to them.  
86 The suspension system provides a safe driving experience for the driver, passengers, and occupants of the vehicle  
87 by reducing or eliminating body roll in turns, bumps in the road, and vibrations [8].

88 A passive suspension system is a system in which the basic components are used to isolate the vibrations  
89 resulting from the movement of the vehicle on the road, such as springs and dampers. The design and selection  
90 of the spring and damper are chosen according to the vehicle's operating conditions and according to the design  
91 objectives and intended application [9].

92 A semi-active suspension system is an application of mechatronics to a suspension system. A semi-active  
93 suspension system is characterized by a switchable damper, and the damping coefficient can be adapted according  
94 to the driving conditions. The vehicle's ride comfort with a semi-active suspension system is improved in  
95 comparison with a passive suspension system. Vehicle stability is also performed with a semi-active suspension  
96 system when compared with a passive system [10][11][12].

97 To study the vibrational behaviour of the vehicle while travelling over roads, there are many methods to  
98 represent the road signals. Phalke et al. [13] have used the eccentric method of an external tire to generate the  
99 road excitation to the tire of a vehicle used as part of a quarter car model. This method has been applied in  
100 many previous studies such as ??lorin et al. [14] and Mehdi et al. [15]. Magnetorheological (MR) is one of the  
101 most recent and widely used applications in semi-active suspension systems. It consists of an intelligent device  
102 whose function is to dampen the vibrations to reach a relatively acceptable vibration amplitude that meets the  
103 requirements for vehicle ride comfort. Usually, the magnetorheological is based on the generation of a magnetic  
104 field using a direct current from the controller affecting the coil in the magnetorheological MR, and this causes  
105 the MR fluids to change from a viscous liquid state to a semi-solid state in the resistance gap [16][17][18].

106 The active suspension system is characterized by the presence of a linear actuator beside the spring and  
107 damper. The linear actuator can be either a hydraulic actuator or an electric motor. The role of the linear

---

108 actuator is to generate the force required for the suspension system to be more comfortable and the vehicle more  
109 stable during varied driving conditions [19][20][21].

110 Modelling of vehicle suspension systems can be simulated as a quarter car, which deals with two degrees of  
111 freedom [22]. Two masses are used in the quarter-car model: a sprung mass and an unsprung mass. The sprung  
112 mass includes the chassis, body, engine, and cabin. The sprung mass is carried over the spring and damper  
113 system [23]. Un-sprung masses are the axle and tire masses and are installed down the spring and damper system  
114 [24]. The quarter model of vehicle suspension system performance can be introduced with sprung mass vertical  
115 acceleration, tire dynamic load, and suspension working space ] 25 .[ To evaluate the vibrational behaviour of the  
116 vehicle while traveling over the bumps, Fakhraei et al. [28] assumed that the hump function is part of a sinusoidal  
117 wave for the circular humps, while for the rectangular humps, it was expressed as a function of the amplitude  
118 (height), the length of the bump and the frequency (vehicle speed). They studied the effect of traveling over  
119 humps on non-linear dynamic behaviours as well as ride comfort for the vehicle and driver. A mathematical  
120 model was presented, by solving the differential equations and then evaluating the ride comfort by calculating  
121 the RMS value of the vertical displacement of the vehicle body and the driver.

122 Other works have presented theoretical research aiming to reduce the cost of that which uses magnetorhe-  
123 ological MR damper such as Ghoniem et al. [32] who have used a new, low-cost damper for the application  
124 of the vehicle's semi-active suspension systems. The strategy of this system is based on changing the damping  
125 coefficient is adapted using an artificial neural network controller by controlling the throttle opening area. A  
126 controller was trained based on the data obtained from the PID controller. The results showed that the proposed  
127 new suspension system provides a cheaper alternative to commercially available semi-active suspension systems  
128 based uses magnetorheological MR damper. The proposed new semi-active suspension could cost up to 20% of  
129 the cost of the magnetorheological MR damper.

130 In this work, to study the vehicle's vibrational behaviour, a mathematical model for a quarter of a vehicle was  
131 designed using the MATLAB Simulink program. Three models of passive, semi active and active suspensions  
132 were presented for use in this study. Comparison of the vibrational behaviour of the three types will be introduced  
133 when the vehicle is travelling over different types of road humps such as circular, trapezoidal, and cat eye hump  
134 to achieve the most ride comfortable system.

## 135 2 II. Methodology

136 To study the vehicle's vibrational behaviour, a mathematical model for a quarter of a vehicle was designed using  
137 the MATLAB Simulink program. Three models of passive, semi active and active suspensions were presented  
138 for use in this study. Comparison of the vibrational behaviour of the three types will be introduced when the  
139 vehicle is travelling over different types of road humps such as circular, trapezoidal, and cat eye hump to achieve  
140 the most ride comfortable system. MATLAB Simulink will be used in this study; a quarter car model will be  
141 investigated to achieve vibrational behaviours of the vehicle and these effects on vehicle ride comfort.

142 Moreover, a comparison between the three models will be introduced.

143 From the simulation results, we assume to find the following data for each case :

144 ? Body Vertical Acceleration (m/s<sup>2</sup>).

145 ? Tire Dynamic Loads (N).

146 ? Suspensions Working Space (m).

147 ? Body Displacement (m) .

148 Where these four outputs are directly affecting the ride comfort and stability of the vehicle. Moreover, the  
149 vibrational behaviours of the three types of suspension systems will be investigated.

150 A semi active suspension system is normally characterized by the presence of a control system. Mostly PID  
151 controller is used to adapt the body vertical acceleration within minimum level. The damping coefficient is used  
152 as the controller action. The proportional parameter K P is firstly tuned. Then, the integrator factor K I is  
153 adapted until the system noise reached until minimum levels and the error becomes too low. The differential  
154 parameter K D is then adjusted to damp the noise of the signal. Saad et al [22] and Hanafi

## 155 3 Global Journal of Researches in Engineering

156 (A ) Volume Xx XII Issue I V ersion I et al [23] have used PID controller in their work to control semi-active  
157 suspension system. The active suspension system is characterized by the presence of a linear actuator beside  
158 the spring and damper. The linear actuator can be either a hydraulic actuator or an electric motor. The role  
159 of the linear actuator is to generate the force required for the suspension system to be more comfortable and  
160 the vehicle more stable during varied driving conditions [19][20][21] Tremendous development has occurred in  
161 vehicle technology in most of the vehicle's components, especially the suspension system. Firstly, the suspension  
162 system has been presented in the economic vehicles as a major part of the vehicle's parts. The main role of the  
163 suspension system is to isolate or reduce the vibrations resulting from the movement of the vehicle is travelling  
164 over different roads according to the quality of the asphalt. Conventional suspension system is consisting of  
165 sprung mass and un-sprung mass connected by a spring and damper. The un-sprung mass is attached to the  
166 bottom by means of a tire stiffness. The conventional system is called the passive suspension system. To enhance  
167 the performance of the suspension system, a semi-active suspension system has been applied, in which the value

168 of the damping coefficient is adapted based on changing operating conditions such as vehicle speed and road  
 169 quality. Many references have proven the effectiveness of the semi-active suspension system.

170 On the other hand, the quality of roads in residential areas and highways is increasing day by day, which  
 171 encourages some vehicle drivers to drive at high speeds more than the recommended limits set by the authorities.  
 172 Therefore, decision makers have been forced to extend road humps, especially where accidents are frequent.  
 173 Several shapes of humps and bumps have been presented such as circular, trapezoidal and circular bumps. Of  
 174 course, these humps greatly affect the vehicle ride comfort, especially when traveling over them at high speeds.

175 Therefore, the aim of this work is to present a theoretical study (a mathematical model) using the MATLAB  
 176 Simulink program to investigate the vibrational behaviour of a quarter a car with passive suspension and a  
 177 semi-active suspension system with a comparison between each system when driving over the types of bumps by  
 178 calculating -:

- 179 ? Body Vertical Acceleration (m/s<sup>2</sup>).
- 180 ? Tire Dynamic Loads (N).
- 181 ? Suspensions Working Space (m).
- 182 ? Body Displacement (m).

### 183 4 III. Modeling & Analysis

184 Table ?? : Below shows a medium sedan passenger car specification that will be used in this study. [6] Table ??:  
 185 Sedan vehicle specifications Many types of road humps are globally used in urban areas. In this study, three well  
 186 known types of road humps are used: circular hump, trapezoidal hump, and cat-eye hump.

#### 187 5 a) Circular Hump

188 The circular humps are one of the common humps that are used in urban areas and cities. The circular hump is  
 189 characterized by the arc radius "R", the hump length, and hump height.

190 It is required to calculate the time required that the vehicle is travelling over the hump. The time is the input  
 191 of the model.  $t = \frac{H}{R} \sqrt{2R - h} + \frac{h}{2R}$

192 Figure ?? : Circular hump profile Fig. ?? shows the circular road hump profile where the radius R in meter  
 193 and the length and the height of the hump.  $2 = \frac{h}{2R} + \left(\frac{h}{2R}\right)^2$   $2 = \frac{h}{2R} + \frac{h^2}{4R^2}$   $2 = \frac{h}{2R} + \frac{h^2}{4R^2}$   
 194  $\left(\frac{h}{2R}\right)^2$  b) Trapezoidal Hump

195 Fig. 2 shows the configuration of the trapezoidal hump. The trapezoidal hump is characterized by total length  
 196 "L", inclined length "L1", flat top length "L2", and hump height "H". The hump height can be expressed as  
 197 follow:  $H = \frac{L_1 \sin \theta}{2}$   $0 < \theta < \frac{\pi}{2}$   $1 < \frac{L_1}{L} < 2$  c)  
 198  $1 < \frac{L_1}{L} < \left(\frac{L_1}{L} + \frac{L_2}{L}\right)$   $\frac{L_1}{L} + \frac{L_2}{L} < 2$   $\frac{L_1}{L} + \frac{L_2}{L} < 2$   $\frac{L_1}{L} + \frac{L_2}{L} < 2$

199 Cat-Eye Hump  
 200 The cat-eye hump is arranged in a matrix configuration and distributed transversally to the roads. It is  
 201 principally designed as a cushion or attention system. Fig. 3 shows the cat-eye hump configuration. The same  
 202 equations of circular hump can be applied with a cat-eye hump. It can be assumed that 6 columns of the cat-eyes  
 203 are distributed with 25 cm intervals. Thus, the total distance is about 1.5 m. Table ?? below shows all types of  
 204 humps with their specifications. [33] Table ??: Circular, trapezoidal, and cat-eye humps specifications

## 205 6 Global Journal of Researches in Engineering

### 206 7 d) Passive Suspension System

207 Fig. ?? shows the configuration of the passive suspension system when the vehicle is travelling over a hump. The  
 208 equations of motion can be expressed as follow:

### 209 8 e) Semi-active Suspension System

210 Fig. 6 shows the configuration of the semi-active suspension system when the vehicle is travelling over a hump.  
 211 The semi-active suspension system is characterized by the presence of a controller that received the signals from  
 212 the sprung mass vertical acceleration and treats them by adapting the damping coefficient of the suspension  
 213 system. The equations of motion can be expressed as follow: 9 shows the configuration of the active suspension  
 214 system of a quarter car when the vehicle is travelling over a hump. The active suspension system is normally  
 215 characterized by the presence of a linear actuator beside the suspension and the damper. The linear actuator  
 216 force signals are received by the controller according to the body vertical acceleration. The equations of motion  
 217 can be expressed as follow:  $m\ddot{x} + c\dot{x} + kx = F(t)$  :

## 218 9 Global Journal of Researches in

219  $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   
 220  $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   
 221  $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   
 222  $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$   $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \ddot{y}$



referred to the passive one. However, the maximum value of the body vertical acceleration is about  $9 \text{ m/s}^2$  as a passive suspension system is used while, this value is reduced to about  $7 \text{ m/s}^2$  as active suspension system is applied. The suspension working space is considerably reduced as the semi-active suspension system is applied in comparison with active suspension system. The dynamic tire load is slightly improved with the active and semi active suspension systems referred to the passive one. The body displacement of the vehicle is considerably improved with the active and the semi-active suspension systems referred to the passive one. Fig. (13) shows the dynamic vibrational behaviour of a quarter car travelling over cat-eyehump at  $30 \text{ km/h}$  with passive, semi-active and active suspension systems. The vehicle ride comfort is worthily affected as the vehicle travelling over the cat eye hump at  $30 \text{ km/h}$ . No considerable changes in the body vertical acceleration were achieved with the using of the active and the semi-active suspension systems related to the passive one. However, the maximum value of the body vertical acceleration is about  $7 \text{ m/s}^2$  as a passive suspension system is used while, this value is reduced to about  $6 \text{ m/s}^2$  as active suspension system is applied. In the same context, the suspension working space is slightly reduced as the active suspension system is applied in comparison with passive suspension system. Differently, no change was prompted in dynamic tire load in both cases. The body displacement of the vehicle is considerably reduced as the using active or semi-active suspension systems compared with the passive suspension system. Fig. (14) shows the dynamic vibrational behaviour of a quarter car travelling over cat-eyehump at  $40 \text{ km/h}$  with the passive, the semi-active and the active suspension systems. As the vehicle speed is increased from  $30 \text{ km/h}$  to  $40 \text{ km/h}$ , the body vertical acceleration is reduced to about  $5 \text{ m/s}^2$  referred to  $30 \text{ km/h}$  vehicle speed there is no change prompted in. However, the maximum value of the body vertical acceleration is about  $7 \text{ m/s}^2$  as a passive suspension system is used while, this value is reduced to about  $5 \text{ m/s}^2$  as active suspension system is applied. In the same context, the suspension working space is considerably reduced as the active suspension system is applied in comparison with passive suspension system. Differently, no change was prompted in dynamic tire load in both cases. Looking at the body displacement of the vehicle, there is a slight improvement when using active suspension system compared with passive suspension system.

Figure 15: Vibrational behaviour of vehicle over cat-eyehump at  $50 \text{ km/h}$  Fig. (15) shows the dynamic vibrational behaviour of a quarter car travelling over cat-eyehump at  $50 \text{ km/h}$  with passive, semi-active and active suspension systems. The body vertical acceleration are improved as the vehicle speed increased. There are no tangible changes prompted in the body vertical acceleration when the semi-active or the active suspension system are used. However, the maximum value of the body vertical acceleration is about  $4 \text{ m/s}^2$  as a passive suspension system is used while, this value is reduced to about  $3.8 \text{ m/s}^2$  as active suspension system is applied. In the same context, the suspension working space is slightly reduced as the active suspension system is applied in comparison with passive suspension system. Differently, no change was prompted in dynamic tire load in both cases. Looking at the body displacement of the vehicle, there is a slight improvement when using active suspension system compared with passive suspension system.

## 11 V. Conclusions

The following conclusions can be achieved:

1. Mathematical models were introduced to study the vibrational behaviour of the vehicle when traveling over various types of road humps such as the circular, the trapezoidal and the cat-eye humps, using a passive, a semi-active and an active suspension systems.

2. The parameters that were investigated in this study to evaluate the ride comfort are the body vertical acceleration, the suspension working space, the dynamic tire load and the displacement of the body. The ride comfort is greatly affected by driving over humps, especially at high speeds. Traveling over humps, whether circular or trapezoidal, has a great impact on the comfort of riding, as well as the stability of the car. There is a clear and tangible improvement when a semi-active suspension system is used compared to a passive suspension system. The semi-active suspension system is characterized by the presence of PID controller. The PID goal is to minimize the value of the body vertical acceleration values considering the body vertical acceleration as the controller input and changing the damping coefficient as the controller output. These improvements were obtained in the body vertical acceleration, the suspension working space, the displacement of the body, and the dynamic tire load levels. With the high speeds, the ride comfort is achieved for all the humps used in this study except for cateye hump, whereas the worth ride comfort is achieved at low speeds. Therefore, through these results, it can be recommended to use the active or semi-active suspension systems instead of the passive

1 2

<sup>1</sup>© 2022 Global Journals Vibrational Behaviour of a Quarter Car Travelling over Road Humps with Different Suspension Systems

<sup>2</sup>© 2022 Global Journals

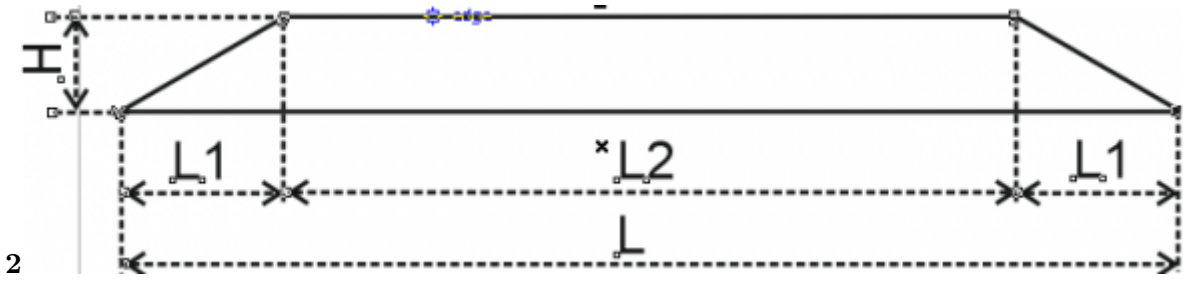


Figure 1: Figure 2 :

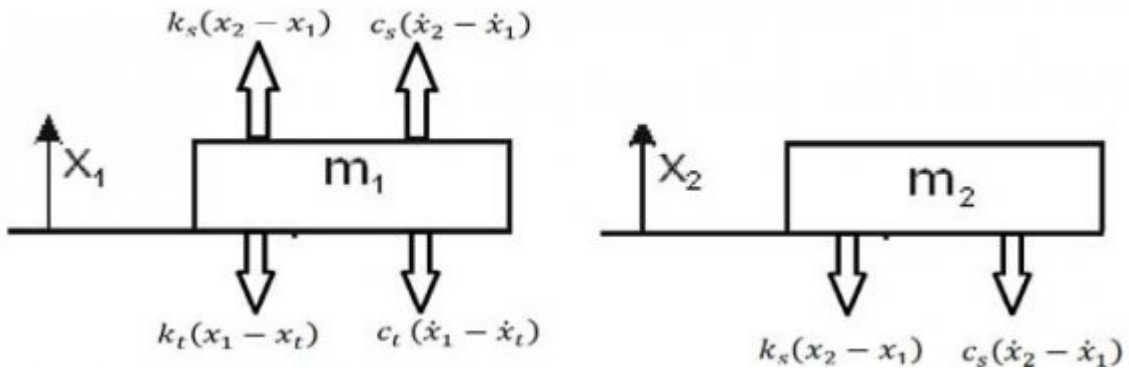


Figure 2: (

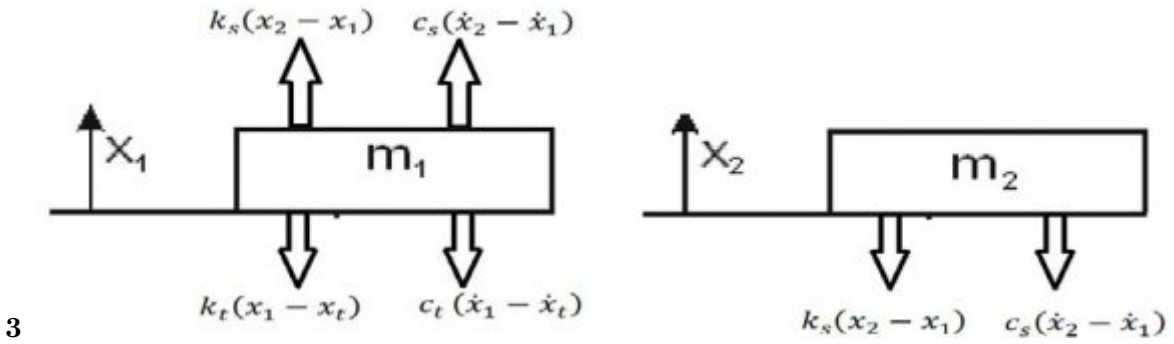


Figure 3: Figure 3 :

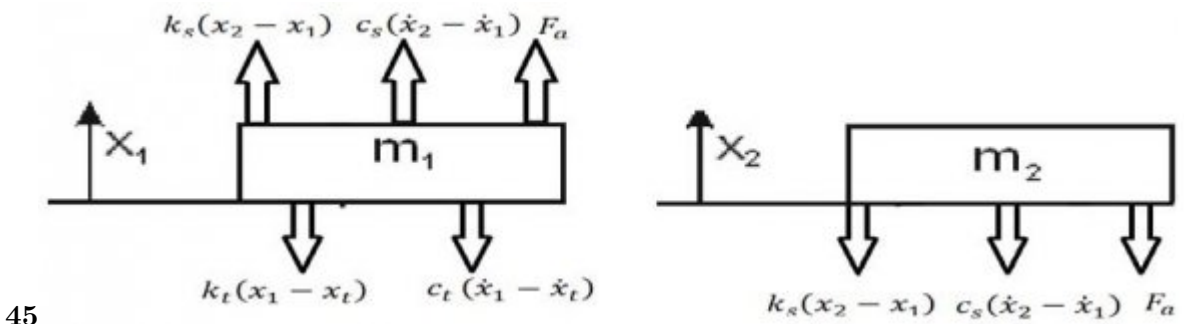


Figure 4: Figure 4 :Figure 5 :

6

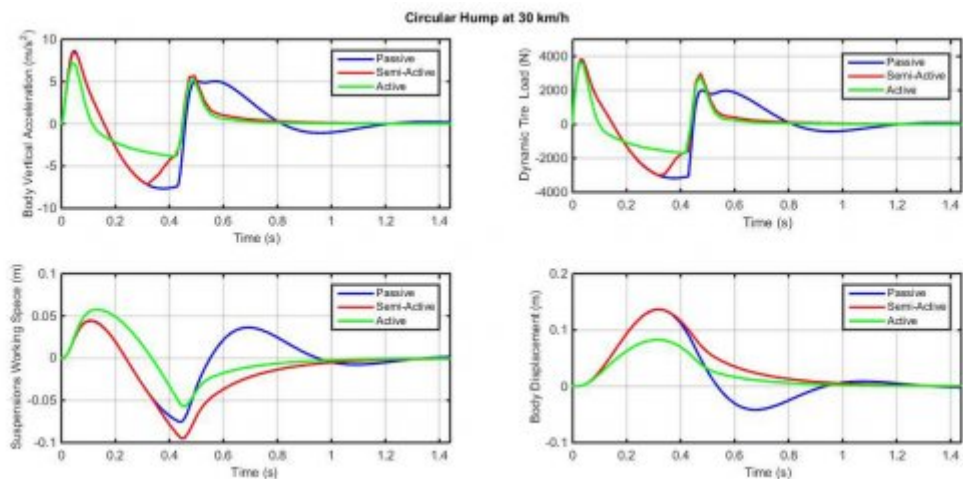


Figure 5: Figure 6 :

7

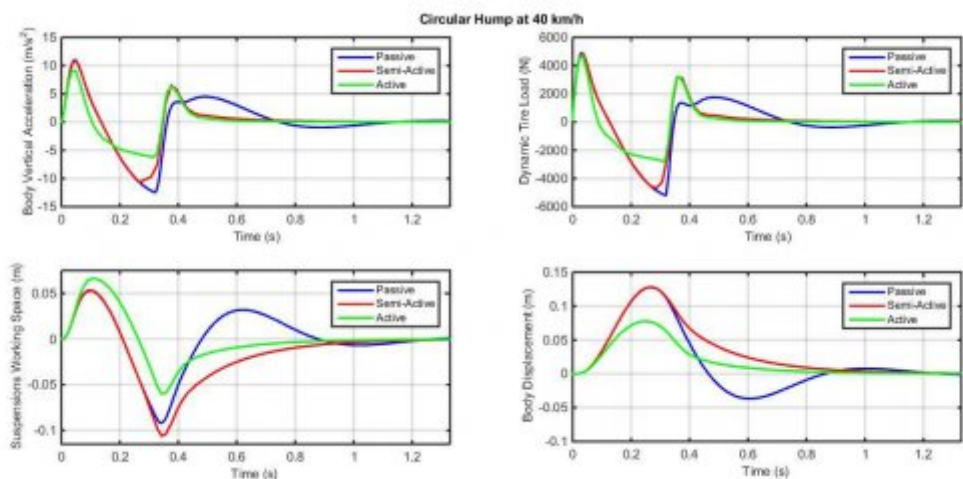


Figure 6: Figure 7 :

8

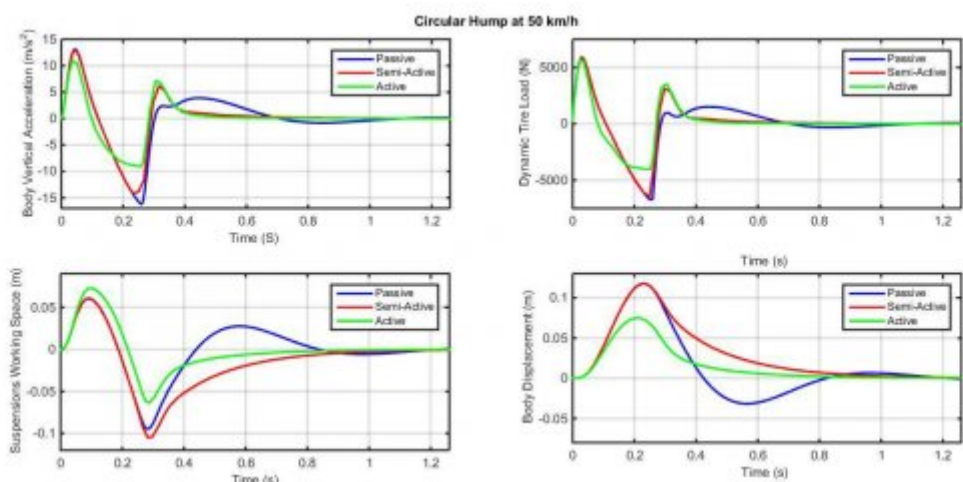
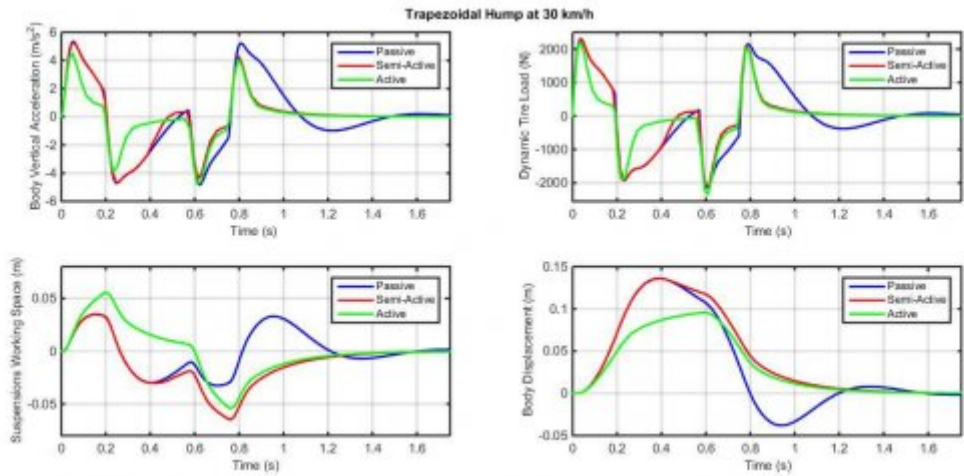


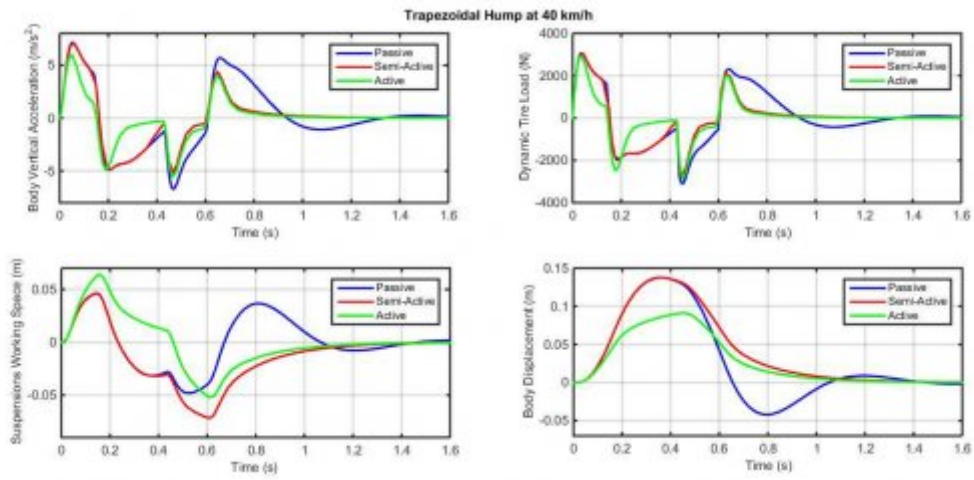
Figure 7: Figure 8 :





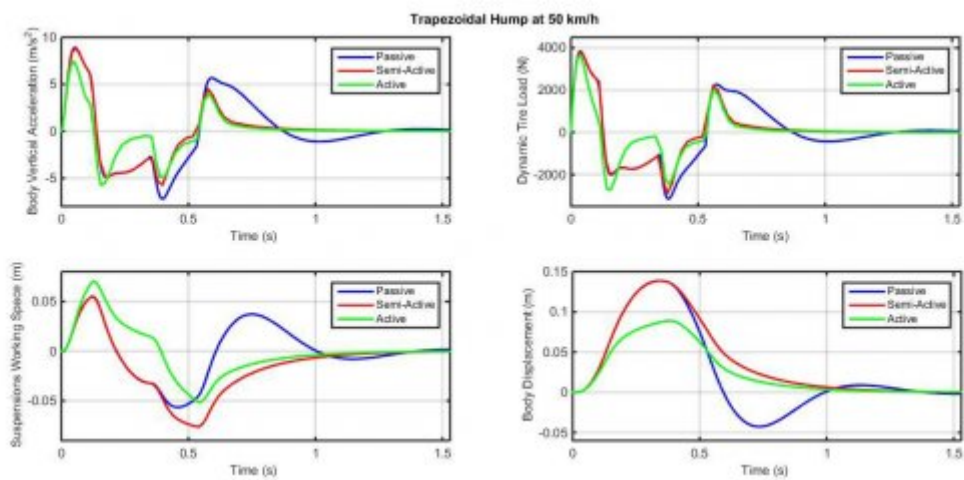
9

Figure 8: Figure 9 :



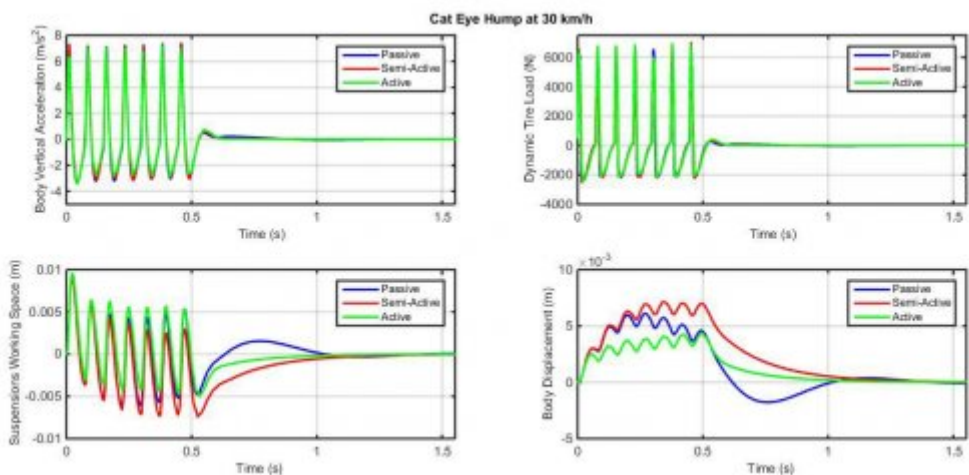
7

Figure 9: Figure 7 :



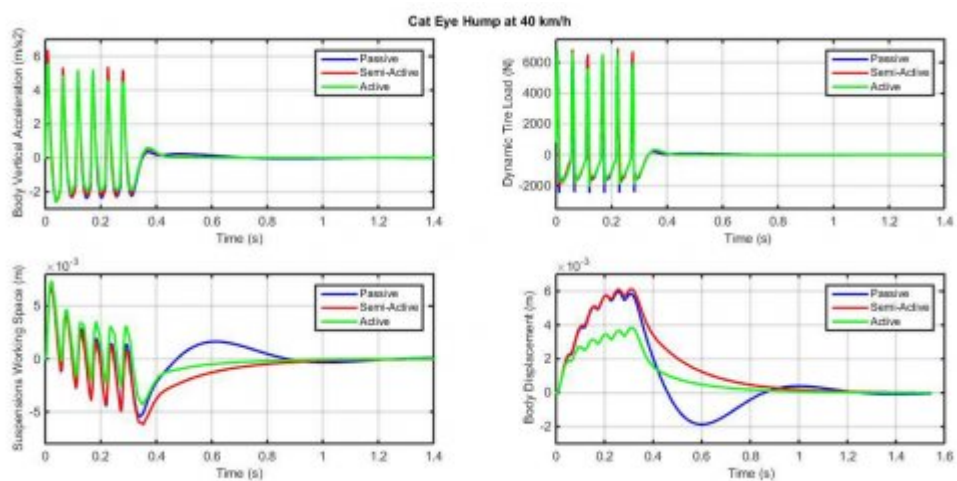
8

Figure 10: Figure 8 :



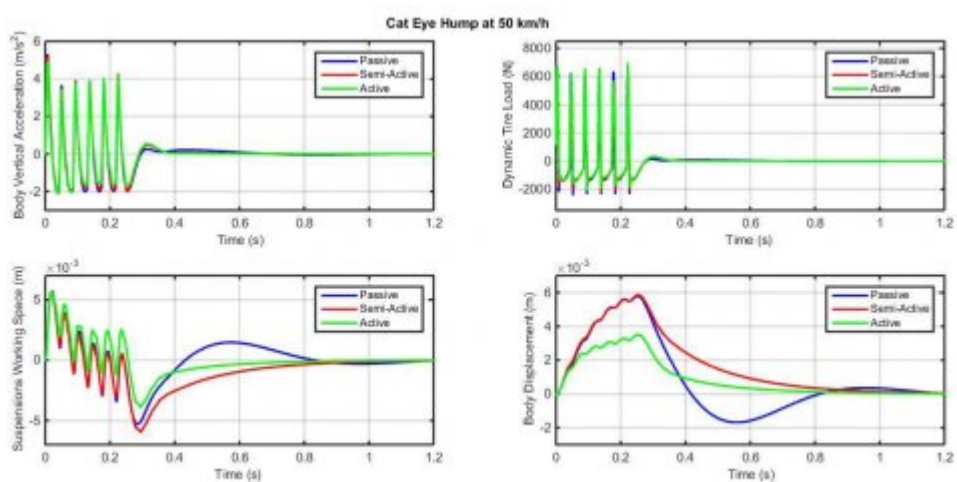
9

Figure 11: Figure 9 :



10

Figure 12: Figure 10 :



11

Figure 13: Figure 11 :

Year 2022

48

(A ) Volume Xx XII

Issue I V ersion I

Global Journal of Re-  
searches in Engineer-  
ing

Parameters Suspension Stiffness (k s )	Value 30000 (N/m)
Damping Coefficient (c s ) Sprung Mass	3500 (N?s/m) 381
(?? 2 ) Un-Sprung Mass (?? 1 ) Tire	(kg) 50 (kg)
Stiffness (k t ) Tire Damping Coefficient	220000 (N/m)
(c t ) Moment of Inertia (??) Wheelbase	140 (N.s/m) 1000
(??)	(kg.m 2 ) 2.69 (m)

© 2022 Global Jour-  
nals

Figure 14:

			Year 2022
			53
			(A ) Volume Xx XII
			Issue I V ersion I
No. Parameters / Quarter Car Model	Affect Ride Com-	Global Journal of Re-	
1 Body Vertical Acceleration (m/s 2 )	fort Stability Sta-	searches in Engineering	
2 Dynamic Tire Load (N) Suspensions	bility Ride Com-		
3 Working Space (m) Body Displace-	fort		
4 ment (m)			
	© 2022 Global		
	Journals		

Figure 15: :



- 337 [KSME Internantional Journal ()] , *KSME Internantional Journal* 1999. 13 (10) p. .
- 338 [Qazi et al. ()] ‘A parametric study on performance of semi-active suspension system with variable damping  
339 coefficient limit’. A J Qazi , A Khan , M T Khan , S J A P Noor . *AASARI Procedia* 2013. 4 p. .
- 340 [Ahmadian and Pare ()] ‘A quartercar experimental analysis of alternative semiactive control methods’. M  
341 Ahmadian , C Pare , Structures . *Journal of Intelligent Material Systems* 2000. 11 (8) p. .
- 342 [Cho et al.] *A roadadaptive control law for semi-active suspensions*, Y Cho , B S Song , K J K I J Yi .
- 343 [Yang ()] *A semi-active suspension using a magnetorheological damper with the nonlinear negative-stiffness  
344 component*, J Yang . 2021. 147 p. 107071.
- 345 [Bachok et al. ()] ‘A theoretical overview of road hump effects on traffic noise in improving residential well-being’.  
346 K S R Bachok , A A K Hamsa , M Z Mohamed , M J T R P Ibrahim . *World Conference on Transport  
347 Research* 2017. 25 p. .
- 348 [Hyniova et al. ()] *Active suspension system-energy control*, K Hyniova , A Stribrsky , J Honcu , A J I P V  
349 Kruczek . 2009. 42 p. .
- 350 [Phalke and Mitra ()] ‘Analysis of ride comfort and road holding of a quarter car model by Simulink’. T P Phalke  
351 , A C J M T P Mitra . *Materials Today: Proceedings* 2017. 4 (2) p. .
- 352 [Garcia-Pozuelo et al. ()] ‘Bump modeling and vehicle vertical dynamics prediction’. D Garcia-Pozuelo , A  
353 Gauchia , E Olmeda , V J A I M E Diaz . *Advances in Mechanical Engineering* 2014. 6 p. 736576.
- 354 [Yoshimura et al. ()] ‘Construction of an active suspension system of a quarter car model using the concept of  
355 sliding mode control’. T Yoshimura , A Kume , M Kurimoto , J J J O S Hino , Vibration . *Journal of Sound  
356 and Vibrations* 2001. 239 (2) p. .
- 357 [Ghoniem et al. ()] ‘Control of a new low-cost semi-active vehicle suspension system using artificial neural  
358 networks’. M Ghoniem , T Awad , O J A E J Mokhiamar . *Alexandria Engineering Journal* 2020. 59 (5)  
359 p. .
- 360 [Turnip et al. ()] *Control of a semi-active MR-damper suspension system: a new polynomial model*, A Turnip ,  
361 K.-S Hong , S J I P V Park . 2008. 41 p. .
- 362 [Wei and Zhiqiang ()] ‘Damping Multimode Switching Control of Semiactive Suspension for Vibration Reduction  
363 in a Wheel Loader’. T Wei , L J S Zhiqiang , Vibration . *Shock and Vibrations* 2019. 2019.
- 364 [Vashist and Kumar ()] ‘Design and analysis of suspension system for an All-Terrain vehicle’. A Vashist , R J M  
365 T P Kumar . *International Journal of Scientific & Engineering Research* 2021. 47 p. .
- 366 [Xie et al. ()] ‘Design of a denoising hybrid fuzzy-PID controller for active suspension systems of heavy vehicles  
367 based on model adaptive wheelbase preview strategy’. Z Xie , P K Wong , J Zhao , T J J O V Xu . *Journal  
368 of Vibroengineering* 2015. 17 (2) p. .
- 369 [Mitra et al. ()] ‘Development and validation of a simulation model of automotive suspension system using MSC-  
370 ADAMS’. A C Mitra , E Fernandes , K Nawpute , S Sheth , V Kadam , S J J M T P Chikhale . *Materialstoday*  
371 2018. 5 (2) p. .
- 372 [Mohite and Mitra ()] ‘Development of linear and non-linear vehicle suspension model’. A G Mohite , A C J M  
373 T P Mitra . *Materialstoday* 2018. 5 (2) p. .
- 374 [Abdel-Wahed et al. ()] ‘Effect of speed hump characteristics on pavement condition’. T A Abdel-Wahed , I H J  
375 J Hashim , T Engineering . *Journal of Traffic and Transportation Engineering* 2017. 4 (1) p. .
- 376 [Mashrosa et al.] ‘Evaluating the Effectiveness of Road Humps in Reducing Vehicle Speed: Case Study of a  
377 University Campus’. N Mashrosa , M F M Nora , A Y Kurniab , S A Hassana , N A Hassana , N Z M Yunusa  
378 . *International Journal on Advanced Science Engineering and Information*
- 379 [Zeinali and Darus ()] ‘Fuzzy PID controller simulation for a quarter-car semi-active suspension system using  
380 Magnetorheological damper’. M Zeinali , I Z M Darus . *2012 IEEE Conference on Control, Systems &  
381 Industrial Informatics*, 2012. IEEE. p. .
- 382 [DJ J ()] ‘Influence of unsprung weight on vehicle ride quality’. DJ J . *Journal of Sound and Vibrations* 1988.  
383 124 (3) p. . (Hrovat and Vibration)
- 384 [Sharma et al. ()] ‘Numerical studies using full car model for combined primary and cabin suspension’. S Sharma  
385 , V Pare , M Chouksey , B J P T . *Procedia Technology* 2016. 23 p. .
- 386 [Barry et al. ()] ‘On the dynamic analysis of a beam carrying Year 2022 multiple mass-spring-mass-damper  
387 system’. O Barry , D Oguamanam , J J S Zu , Vibration . *Shock and Vibrations* 2014. 2014.
- 388 [Türkay and Akçay ()] ‘On the performance limitations of quarter-car active suspension models’. S Türkay , H  
389 J I P V Akçay . *IFAC Proceedings Volumes*, 2007. 40 p. .
- 390 [Sert ()] ‘Optimization of suspension system and sensitivity analysis for improvement of stability in a midsize  
391 heavy vehicle’. E Sert , P J E . *Engineering Science and Technology, an International Journal* 2017. 20 (3) p.  
392 . (Boyraz, and a. i. j. technology)

- 393 [Yildiz ()] ‘Optimum suspension design for nonlinear half vehicle model using particle swarm optimization (PSO)  
394 algorithm’. A Yildiz . *Vibroengineering PROCEDIA* 2019. 27 p. .
- 395 [Omar et al. ()] ‘Parametric numerical study of electrohydraulic active suspension performance against passive  
396 suspension’. M Omar , M El-Kassaby , W J A E J Abdelghaffar . *Alexandria Engineering Journal* 2018. 57  
397 (4) p. .
- 398 [Florin et al. ()] ‘Passive suspension modeling using MATLAB, quarter-car model, input signal step type,’ products  
399 in machine manufacturing technologies, A Florin , M -R. Ioan-Cozmin , P Liliana . 2013. p. .
- 400 [Soliman et al. ()] ‘Semi-active suspension systems from research to mass-market-A review’. A Soliman , M J J  
401 O L F N Kaldas , A Vibration , Control . *Journal of Low Frequency Noise, Vibration and Active Control*  
402 2021. 40 (2) p. .
- 403 [Fakhraei et al. ()] ‘The influence of road bumps characteristics on the chaotic vibration of a nonlinear full-  
404 vehicle model with the driver’. J Fakhraei , H Khanlo , M Ghayour , K Faramarzi . *International Journal of*  
405 *Bifurcation and Chaos* 2016. 26 (09) p. 1650151.
- 406 [Abdulmawjoud et al. ()] ‘Traffic flow parameters development modelling at traffic calming measures located on  
407 arterial roads’. A A Abdulmawjoud , M G Jamel , A A J A S E J Al-Taei . *Ain Shams Engineering Journal*  
408 2021. 12 (1) p. .
- 409 [Parkhill et al. ()] ‘Updated guidelines for the design and application of speed humps’. M Parkhill , R Sooklall ,  
410 G Bahar . *ITE 2007 Annual Meeting and Exhibit. Pittsburgh: Institute of Transportation Engineers, 2007.*
- 411 [Mahmoud ()] ‘Vehicle dynamic behaviours crossing cat-eye reflectors’. K R Mahmoud . *International Journal of*  
412 *Vehicle Noise and Vibrations* 2014. 10 (3) p. .
- 413 [Mahmoud ()] ‘Vehicle dynamic behaviours crossing cat-eye reflectors’. K R J I J O V N Mahmoud . *International*  
414 *Journal of Vehicle Noise and Vibrations* 2014. 10 (3) p. .
- 415 [Hu et al. ()] ‘Vibration control of semi-active suspension system with magnetorheological damper based on the  
416 hyperbolic tangent model’. G Hu , Q Liu , R Ding , G J A I M E Li . *Advances in Mechanical Engineering*  
417 2017. 9 (5) p. 1687814017694581.