

Design and Economic Analysis of a Small Scale Formaldehyde Plant from Flared Gas

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Abstract

The Simulation of a 10,000 ton/yr capacity Formaldehyde plant from flared gases was performed using Aspen Hysys version 8.8, and the Hysys model of the plant was developed using data from literature. A material and energy balance for the various components of the plant was performed manually and with Hysys for comparison. The design/equipment sizing, Mechanical design, costing and economic evaluation, process control of the functional parameters of the various equipments and finally the full Hysys process flow diagram of the model was performed. The Formaldehyde reactors was simulated to study the effect of process functional parameters such as reactor dimensions, temperature, pressure, The effect of reactor size and number on Formaldehyde output was studied by simulating the plant with a compressor, mixer, conversion reactor, cooler, CSTR, heat exchanger, and storage tank.

Index terms— design, height, diameter, volume, composition, formaldehyde.

1 Introduction

ormaldehyde is produced in industrial scale from methanol. It uses atmospheric pressure to perform the production. There are steps in formaldehyde production. The first step involves the liquid methanol which vapourized into an air stream while steam was added to the resulting gaseous mixture. Also, the other step involves the gaseous mixture lead over a catalyst bed. The methanol was finally converted to formaldehyde through partial dehydrogenation and partial oxidation. (Alfaree & Adnan, 2016).

Besides, the report by Welch shows that 10 million of formaldehyde was produced annually and met the demand of the industries as at then, but as population increases, the demand of formaldehyde was increased and the production rate was not able to met industrial scale based on its wide application. (Alzein & Nath, 2018), the process industry would need more of formaldehyde production rate to met world production annually. This increase in population that occurs result to more production of formaldehyde at a later year. In the 2012, the production of formaldehyde amount to 32.5 million tons per year. According to ??Sukunya et al., 2014), this increase in demand was due to the applications of formaldehyde in chemical synthesis such as resin products. These resins are used for polywood production. Also, formaldehyde solution can destroy bacteria and fungi.

However, the 32.5 million tons per year was a report as at 2012, but we are now in 2019. This has resulted to increase in population of the world as well as the demand for formaldehyde base on its usage in process industries. (Cameroon et al., 2019).

Today, many researchers are looking for new areas in which formaldehyde can be applied, technology has increase and new methods are been discovered. (Chauvel & Lefebvre, 2015),The production based on report cannot met the demand today and so more researchers are to go into designing of units operations for the production of formaldehyde to met world demand which as a results of the current population density. Also, more processes for the production of formaldehyde can be added to the existing two processes and hence these calls for more future research to be carried out with a view of which production process gives the most yield with the least cost of production. ??Chouldhary et al., 2017).

The study of formaldehyde plant calls for new design of reactor that would produce formaldehyde in excess in other to take care of the world's population that requires the uses and applications of formaldehyde. The

2 B) METHODS

45 production of formaldehyde using the silver contact process amounts to 80% of total formaldehyde process. The
46 type of reactor determines the desired productions which depend on feed quality (Antonio et al., 2010; and the
47 reactor temperature . The work focus on the type of reactor design would produce formaldehyde in excess as
48 to met the current demand of society today. This is base on the wide application of formaldehyde. The study
49 require the development of design parameters or sizes of continuous stirred tank, plug flow and batch reactor for
50 the two routes used in producing formaldehyde. The reactor types would be tested in its design to compute and
51 simulate to ascertain which reactor type would be suitable to produce formaldehyde in the required quantity to
52 supply to the needs of the process industry for various applications.

53 Besides, the various reactor models would be tested with the reaction mechanisms and kinetics for simulations
54 of variables which would be used to ascertain the reactor that best give the highest production. The products
55 from the reactors are fed into absorber to form formaldehyde 37% by mass called formalin or more ??Andre et
56 al., 2002).

57 However, the formalin formed at room temperature was not stable and formed paraformaldehyde. The
58 paraformaldehyde formed was high concentration of formaldehyde. But formalin has methanol of 1.14% by
59 mass for more stability in solution and its temperature was more than 313k , the study focuses on the design of
60 reactor types for the production of formaldehyde. This formaldehyde has the formula HCHO and the first series
61 of aliphatic aldehyde which was discovered in 1859. The production of formaldehyde which started during the
62 twentieth century had continued even till date. The study becomes more imperative for industries, engineers and
63 producers who wants to exploits the opportunity to design reactor types for the production of formaldehyde.

64 Also, the study calls for new design of reactor that would produce formaldehyde in excess in other to take
65 care of the world's population that requires the uses and applications of formaldehyde. (Ghanta et al., 2017),
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67 The type of reactor determines the desired product which depend on feed quality (Antonio et al., 2010;, Their
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69 of society today. This is base on the wide application of formaldehyde. The study require the development of
70 design parameters or sizes of continuous stirred tank, plug flow and batch reactor for the two routes used in
71 producing formaldehyde. (Ghaza & Mayourian, 2014),The reactor types would be tested in its design to compute
72 and simulate to ascertain which reactor type would be suitable to produce formaldehyde in the required quantity
73 to supply to the needs of the process industry for various applications. (Gujarathi et al., 2020), the various
74 reactor models would be tested with the reaction mechanisms and kinetics for simulations of variables which
75 would be used to ascertain the reactor that best give the highest production. The products from the reactors are
76 fed into absorber to form formaldehyde 37% by mass called formalin or more ??Andre et al., 2002). However,
77 the formalin formed at room temperature was not stable and formed paraformaldehyde. The paraformaldehyde
78 formed was high concentration of formaldehyde.

79 But formalin has methanol of 1-14% by mass for more stability in solution and its temperature was more
80 than 313 k ??Geoffrey et al., 2009). The study focuses on the design of reactor types for the production of
81 formaldehyde. This formaldehyde has the formular HCHO and the first series of aliphatic aldehyde which was
82 discovered in 1859. The production of formaldehyde which started during the twentieth century had continued
83 even till date. The study becomes more imperative for industries, engineers and producers who wants to exploits
84 the opportunity to design reactor types for the production of formaldehyde.

85 The production and optimization of formaldehyde can include the streams for air, methanol and water in a
86 suitable composition in a plug flow reactor under certain conditions of temperatures and pressure ??Andreasen
87 et al., 2003). The purpose of using a plug flow reactor is to get desired product which can be optimized to get
88 best yield of formaldehyde (Antonio et al., 2010;. (Lauks et al., 2015), on the other hand, when the production of
89 formaldehyde involves the use of silver catalyst, the operation is carried out adiabatically by lagging the system
90 which helps to obtain a selectivity of 90%. (Marton et al., 2017), the life of the catalyst is short depending on
91 the impurities in the methanol and the gases at exist that contain considerable amount of hydrogen and water.
92 However, the silver being a metal would have low catalytic activity for the decomposition of methanol even at
93 a very high temperature. (Mazanec et al., 2019), the chemisorption of the monoatomic oxygen in the metal
94 brings its activation. (Meisong, 2015), thermal decomposition of formaldehyde depends on the gas stream, the
95 gas stream is cooled when it passes through the catalyst. The formaldehyde produced is then absorbed in an
96 absorber by water to get pure formaldehyde. Since the gaseous form of formaldehyde is unstable, it is better
97 absorbed in water. (Mohamad, 2016), the products of reaction contains the formaldehyde diluted in water other
98 gases which mainly contains nitrogen. Finally, the commercial and final product is obtain from the absorber of
99 about 55% weight of formaldehyde in water or formalin. (Mohsenzadeh, 2019), the design and optimization of
100 the reactor for the production of formaldehyde which uses two different routes and each would be considered
101 during the design of the reactor because we want to know which of the route would be best in the production
102 of formaldehyde. Also, the reactors would be batch, continuous stirred tank and plug flow reactor. Each reactor
103 would follow both routes

104 2 b) Methods

105 The methods that will be adopted in this Research includes: Material balance are the basics of process design.
106 A material balance taken over the complete process will determine the quantities of raw materials required and

107 products produced. Balances over individual process unit set the process stream flows and compositions. A good
108 understanding of material balance calculations is essential in process design.

109 Material balances are also useful tools for the study of plant operation and trouble shooting. They can be
110 used to check performance against design; to extend the often limited data from the plant instrumentation; to
111 check instrument calibrations and to locate source of material loss.

112 The loss of mass associated with the production of energy is significant only in nuclear reactions. Energy
113 and matter are always considered to be separately conserved in chemical reactions. $[m_{in}] = [m_{out}] + [m_{loss}]$
114 $[m_{in}] = [m_{out}] + [m_{loss}]$? $[m_{in}] = [m_{out}] + [m_{loss}]$? $[m_{in}] = [m_{out}] + [m_{loss}]$?

115 For steady state process the accumulation term will be zero except in nuclear process, mass is neither generated
116 nor consumed; but if a chemical reaction take place a particular chemical species may be formed or consumed in
117 the process. If there is no chemical reaction the steady state balance reduces to: $[Materials\ in] = [Materials\ Out]$

118 3 (b) Energy Balance

119 A general energy balance equation can be written as: $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out} + \Delta H_{rxn}$
120 $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out} + \Delta H_{rxn}$? + ? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out} + \Delta H_{rxn}$
121 ? ? ? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out} + \Delta H_{rxn}$? ? ? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out} + \Delta H_{rxn}$
122 $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out} + \Delta H_{rxn}$? If no chemical reaction occurs ? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out}$
123 ? = ? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out}$? = 0 Equation (3) becomes ? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out}$
124 $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out}$? = ? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out}$? ? ? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out}$
125 $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out}$?

126 If the system is a steady state process? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out} + \Delta H_{rxn}$? = 0
127 Equation (5) becomes ? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out} + \Delta H_{rxn}$? = ? $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out} + \Delta H_{rxn}$
128 $Q_{in} + \sum (m_i h_i)_{in} = Q_{out} + \sum (m_i h_i)_{out} + \Delta H_{rxn}$?

129 Energy flow for each stream shall be computed in terms of Heat Flow using the formula?? $Q = m \cdot C_p \cdot \Delta T$??
130 $Q = m \cdot C_p \cdot \Delta T$? ? ? $Q = m \cdot C_p \cdot \Delta T$? Where ?? = $Q = m \cdot C_p \cdot \Delta T$? $Q = m \cdot C_p \cdot \Delta T$? $Q = m \cdot C_p \cdot \Delta T$? $Q = m \cdot C_p \cdot \Delta T$?
131 $Q = m \cdot C_p \cdot \Delta T$? $Q = m \cdot C_p \cdot \Delta T$? © 2021 Global Journals

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133 The general conservation equation for any process can be written as: required for the production of
134 formaldehyde and the optimization of each routes of production and in each of the reactor types. Finally,
135 the physical properties would be presented in tabular form below ??Reuss et al., 2003). Jaja et al, (2020),
136 Methane is a major component of flared gas as well as natural gas and its composition varies from 70 to 90% in
137 both cases.

138 (3) (2) (1) (4) (5) (6) (7) (8)

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140 5 (d) Mechanical Design

141 A vessel must be designed to withstand the maximum pressure to which it is likely to be subjected in operation.
142 For vessels under internal pressure, the design pressure is normally taken as the pressure at which the relief device
143 is set. This will normally be 5 to 10 per cent above the normal working pressure, to avoid spurious operation
144 during minor process upsets. When deciding the design pressure, the hydrostatic pressure in the base of the
145 column should be added to the operating pressure if significant.

146 Vessels subject to external pressure should be designed to resist the maximum differential pressure that is
147 likely to occur in service. Vessels likely to be subjected to vacuum should be designed for a full negative pressure
148 of 1 bar unless felted with an effective and reliable vacuum breaker.

149 6 (e) Cost Estimation and Economic Evaluation

150 Economic evaluation is very important for the proposed plant. We have to be able to estimate and decide between
151 either native design and for project evaluation. Chemical plants are built to make profit and estimate of the
152 investment is required and the cost of production are needed before the profitability for a project is the sum of
153 the fixed and working capital.

154 Fixed capital is the total cost of the plant ready to start up. It is the cost paid to the contractors. Working
155 capital is the additional investment needed, over and above the fixed capital to start up the plant and operate
156 it to the point when income is earned. Most of the working capital is recovered from at the end of the project.
157 The full detail of the costing is given in the appendix.

158 III. Design Simulation (Hysys) This section represents a process simulation of plant design for the production
159 of Formaldehyde from flared gas. The simulation covers the following equipments/units: Figure 1 shows the full
160 PFD of the Hysys design Simulation Where formaldehyde from flared gas using the reaction between absorbed
161 methane gas from flared gas and oxygen. The procedure begins with compressing of flared gasses using a
162 compressor. The component of interest being methane is being compressed and mixed with air stream inside
163 a mixer and then sent to a conversion reactor where reaction of methane and oxygen occurs to Formaldehyde,

164 Carbon [iv] oxide and water as products. The overhead products from the conversion reactor is being cooled and
165 sent to a Continuous Stirred Tank Reactor [CSTR] for further reaction and more yield of the formaldehyde.

166 The product from the CSTR is being sent to the heat exchanger for further hitting to the desired temperature
167 and subsequently sent to the storage tank Year 2021(D D D) C

168 for storage. The process was able to convert about 90% of methane and the yield of Formaldehyde is up
169 to 45% making the process very economical to set up a plant for the production process using flared gas and
170 trapping methane as base component of reaction. This is a new innovation in the technology of the production
171 The following results of material balance with manual calculation compared with Hysys simulation is presented
172 in tables below for each unit.

173 7 Streams

174 Manual calc. Hysys Simulation % Deviation In Table 4.1 above the mass flow rate of Flared Gas Stream (S
175 1) for Hysys simulation is 1.2×10^4 kg/hr while that for the manual calculation is 1.23×10^4 kg/hr with a
176 deviation of 2.5%. the molar flow rate for Hysys simulation was found to be 600.10 kgmole/hr while that of
177 manual calculation is 600.50 kgmole/hr with a deviation of 0.7% we also observe that since this unit is a single
178 input, single output stream and applying the principles of conservation of mass, input mass equals output mass,
179 hence the output been Compressed Flared Gas has the same mass and molar flow rates of the input stream which
180 is Flared Gas as well as the same deviation.

181 8 Streams

182 Manual calc.

183 9 Hysys Simulation % Deviation

184 Air (S 3) Mass Flow (kg/hr) 1.1×10^4 In Table 4.2 above the mass flow rate of the Air Stream is 1×10^4 kg/hr
185 for Hysys simulation while for manual calculation is found to be 1.1×10^4 kg/hr having a deviation of 10%.
186 The molar flow rate for the Hysys simulation is 343.3 kgmole/hr while that of the manual calculation is 343.3
187 kgmole/hr having a deviation of 0.9%. This Flared Gas stream has been stated in the discussion of Table 4.1,
188 however we are to note that Air stream (S 3) and Flared Gas Stream (S 2) are both input streams respectively
189 which are mixed inside a mixer to produce an outlet stream Mixed Product (S 4) having a mass flow rate of 2.20
190 $\times 10^4$ kg/hr for Hysys simulation and 2.10×10^4 kg/hr for manual calculation with a 4.5%. the molar flow rate
191 of this stream is 947.10 kgmole/hr for Hysys simulation and 947.40 for manual calculation with a deviation of
192 3%. Applying the principles of conservation of mass to this unit shows that if mass flow rates of the inlet streams
193 are added together the results equals the mass flow rate of the outlet stream which makes our results to be valid
194 for inflow of mass is equal to outflow of mass. In Table 4.3 the mass flow rate of the Mixed Product Stream (S
195 4) for Hysys simulation is 2.20×10^4 kg/hr while the manual calculation is 2.10×10^4 kg/hr with deviation
196 of 4.5%. The molar flow rate of the Mixed Product Stream (S 4) is 947.10 kgmole/hr for Hysys simulation and
197 947.40 kgmole/hr for manual calculation with a deviation of 3.0%. We also observe that since this unit is a single
198 input, single Output Stream and applying the principles of conversation of mass, input mass equals output mass,
199 hence the output been Vapour Product (S 5) has same mass and molar flow rates of the Input Stream as well
200 as the same % Deviation. Also the Extent of Reaction for this unit for Hysys simulation is 24.27. The fractional
201 conversion for Hysys simulation is 0.1102 while for manual calculation is 0.1105.

202 10 Streams

203 11 Streams

204 12 b) Energy Balance Results

205 The following results of energy balance with manual calculation compared with Hysys simulation is presented in
206 tables below for each unit.

207 13 Streams

208 Manual calc. Hysys Simulation % Deviation In Table 4.8 it is observed that the heat flow of the air stream is
209 zero because the temperature of this stream equals its reference temperature hence no heat flow. Also the heat
210 flow of Compressed Gas Stream (S 2) and Mixed Stream (S 4) are equal.

211 14 Streams

212 Manual calc. Hysys Simulation % Deviation

213 In Table 4.9 above the flow of Mixed Stream (S 4) and Vapour Product Stream (S 5) are equal since it is a
214 Single Input, Single Output Stream and also in with the principles of conservation of energy. In Table 4.11 the
215 sum of the heat flow Formaldehyde Liquid Stream (S 7) and Hot Water Inlet Stream (S 10) equals to the sum
216 of the heat flow of Formaldehyde Liquid Out Stream (S 9) and Water Stream (S 11) which is in line with the

217 principles of conservation of energy which states that inflow of energy is equal to outflow of energy provided that
218 the system is a steady state process and no chemical reaction occurs. In Table 4.12 the design parameters such
219 as Column Height, Column Diameter, Cross-sectional Area, Volume, Space time, Space Velocity, Thickness and
220 Corrosion Allowance was compared with Hysys simulation and Manual calculation and the maximum deviation
221 was found to be 3.2%.

222 15 Streams

223 16 b) Design /Sizing Results

224 The equipment design and sizing of each equipment of the plant is presented in the table below, for manual
225 calculation compared to Hysys Simulation. In Table 4.15 Heat Exchanger Design Parameter was compared
226 between Hysys simulation and manual calculation and the maximum deviation was found to be 0.2%

227 17 V. Sensitivity Analysis

228 The functional parameters such as length of Reactor, Diameter, Space time, Space velocity were studied to see
229 how they change with conversion and are presented in figures -to C Figure 1 demonstrates the profile variation
230 of length of the reactor varying with conversion. The results in the profile gives an increase of the length of
231 reactors value with conversion increase. The length of reactor values increased from 0 m to 0.76m due to increase
232 in conversion from 0 to 0.9. the increase in length resulted to increase in volume of the reactor and decrease in
233 the rate of reaction values. The volume of the reactor is a function of length and rate of reaction.

234 18 b) Diameter of Reactor with Conversion

235 Figure Conversion

236 Similarly, figure ?? demonstrates the variation of the diameter the variation of the diameter of the reactor for
237 the production of formaldehyde with conversion. The relationship is such that the length increases with increase
238 in conversion and results to values such that when $D=0$, $X_A=0$ and $D=0.27m$, $X_A=0.9$. since the volume
239 of reactor increases, the length and diameter of the reactor too increases to achieved the production of ethylene
240 oxide and proper sizing of the reactor. 3 depicts the variation of space time of reactor varying with conversion.
241 The profile of the space time is exponentially increasing with conversion starting from 05-0.035hr when X_A
242 $=0-0.9$ respectively. Space time is defined as the time taken for one reactor feed volume converted to product.
243 From the results, the space time values are very small meaning the reaction is a fast one. Increasing the space
244 time values, leads to increase in the value of the reactor and higher yields of the product formed. Figure 4 shows
245 the graph of space velocity varying with conversion. The universe of space time gives the space velocity's values.
246 The space velocity's values are higher and increases from 0-600hr⁻¹ when conversion increases too from 0-0.1
247 and then drops exponentially from 600-10hr⁻¹ when conversion increases from 0.1-0.9. The space velocity should
248 be reduced to achieve higher yield at lower cost as shown from the profile plot.

249 19 c) Space Time with Conversion

250 20 d) Space Velocity with Conversion

251 21 e) Volume of Reactor with Conversion

252 22 VI. Conclusion

253 The design of a 10,000 ton/yr Formaldehyde plant has been executed. The design considered first the material
254 balance of the plant using the principles of conservation of mass which states that for steady state process
255 the inflow of mass equals the outflow of mass, hence the mass balance of each unit/equipment was extensively
256 evaluated, the principles of conservation of energy which states that outflow of energy equals inflow of energy
257 for a steady state process was applied to evaluate the flow of energy for each stream. The design also considered
258 other aspect such as equipment sizing/design specification, mechanical design, costing and economic evaluation,
259 instrumentation and process control, layout, safety and environmental consideration and finally Hysys design
260 simulation. Comparison of the material balance results between manual calculation and Aspen Hysys simulation
261 and the highest difference was 0.8% for the energy balance result the difference between the manual calculation
262 and Aspen Hysys simulation was 0.5% for the sizing results, the highest difference between the manual calculation
263 and Aspen Hysys simulation was 0.3%.

264 Mechanical design to determine the thickness of vessels to withstand pressure was also considered as we as
265 adding corrosion allowance. A detailed cost estimation and economic evaluation was analyzed to determine the
266 profitability of the plant before setting up and it is given in the appendix.

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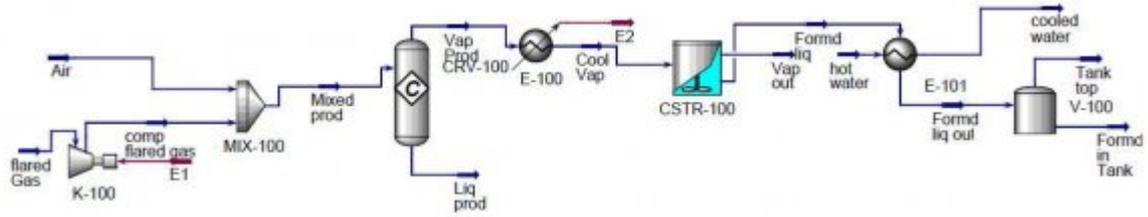


Figure 1:

4

4

1 x 10 4

10

[Note: 1: Comparison of Material Balance Result of Hysys Simulation with Manual Calculation for Compression Unit]

Figure 2: Table 4 .

42

Figure 3: Table 4 . 2 :

	Manual calc.	Hysys Simulation	% De- via- tion
Vapour Product (S 5)			
Mass Flow (kg/hr)	2.10 x 10 4	2.20 x 10 4	4.5
Molar Flow (kgmole/hr)	947.40	947.10	3.0
Cooled Vapour (S 6)			
Mass Flow (kg/hr)	2.10 x 10 4	2.20 x 10 4	4.5
Molar Flow (kgmole/hr)	947.40	947.10	3.0
In Table 4.4 the mass flow rate of the input stream Vapour Product has been stated in the discussion of Table 4.3, this unit contains a single input, single output streams. Hence, the same mass and molar flow rate of the Vapour Product Stream (S 5) is the Streams	Manual calc.	Hysys Simulation	% De- via- tion
Cooled Vapour (S 6)			
Mass Flow (kg/hr)	2.10 x 10 4	2.20 x 10 4	4.5
Molar Flow (kgmole/hr)	947.40	947.10	3.0
Formaldehyde Liquid (S 7)			
Mass Flow (kg/hr)	888.5	888.7	0.2
Molar Flow (kgmole/hr)	45.04	45.03	0.3

Figure 4: Table 4 . 3 :

Figure 5: Table 4 . 4 :

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Figure 6: Table 4 . 5 :

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Flared Gas (S 1)			
Temperature (?)	25	25	0.0
Pressure (kpa)	101.3	101.3	0.0
Heat Flow (kJ/hr)	-	-4.686e7	4.7
	4.682e7		
(E1)			
Temperature (?)	-	-	
Pressure (kpa)	-	-	
Heat Flow (kJ/hr)	3.421e5	3.427e5	1.4
Compressed Gas (S 2)			
Temperature (?)	38.84	38.84	0.0
Pressure (kpa)	120	120	0.0
Heat Flow (kJ/hr)	-	-4.6478e7	1.3
	4.6479e7		

In Table 4.7 above the heat flow of Stream (S 1) and Stream (E1) when added equals the heat flow of stream (S 2) and this is in line with the principles of Streams

Conservation of Energy for a steady state process and chemical reaction occurring.

	Manual calc.	Hysys Simulation	% Deviation
Compressed Gas (S 2)			
Temperature (?)	38.84	38.84	0.0

Figure 7: Table 4 . 6 :

47

Figure 8: Table 4 . 7 :

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Figure 9: Table 4 . 8 :

	Manual calc.	Hysys Simulation	% Devi- ation
Vapour Product (S 5)			
Temperature (?)	34.84	34.84	0.0
Pressure (kpa)	101.3	101.3	0.0
Heat Flow (kJ/hr)	-4.6478e7	-4.6478e7	5.4
(E 2)			
Temperature (?)	-	-	
Pressure (kpa)	-	-	
Heat Flow (kJ/hr)	2.636e7	2.636e7	0.0
Cooled Vapour (S 6)			
Temperature (?)	800	800	0.0
Pressure (kpa)	101.3	101.3	0.0
Heat Flow (kJ/hr)	-7.283e7	-7.285e7	2.4
In table 4.10 the sum of the Heat Flow of Stream E2 and cooled Vapour Stream equals that of Vapour		Product Stream (S 5) which is line with the prin- ciple of conservation of en- ergy.	
Streams	Manual calc.	Hysys Simulation	% Devi- ation
Cooled Vapour (S 6)			
Temperature (?)	800	800	0.0
Pressure (kpa)	101.3	101.3	0.0
Heat Flow (kJ/hr)	-7.283e7	-7.285e7	2.4
Formaldehyde Liquid (S 7)			

Figure 10: Table 4 . 9 :

Figure 11: Table 4 . 10 :

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Figure 12: Table 4 .

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Streams	Manual calc.	Hysys Simulation	% Deviation
Formaldehyde Liquid (S 7)			
Temperature (?)	80	80	0.0
Pressure (kpa)	101.3	101.3	0.0
Heat Flow (kJ/hr)	-1.169e7	-1.167e7	3.0
Formaldehyde Liquid Out (S 9)			
Temperature (?)	120	120	0.0
Pressure (kpa)	101.3	101.3	0.0
Heat Flow (kJ/hr)	-1.154e7	-1.156e7	3.6
Hot Water Inlet (S 10)			
Temperature (?)	200	200	0.0
Pressure (kpa)	101.3	101.3	0.0
Heat Flow (kJ/hr)	-1.160e7	-1.162e7	3.2
Cooled Water Outlet (S 11)			
Temperature (?)	195	195	0.0
Pressure (kpa)	101.3	101.3	0.0
Heat Flow (kJ/hr)	-1.175e7	-1.174e7	1.4

Figure 13: Table 4 .

413

Design/Sizing Item	Hysys Simulation	Manual Calculation	% Deviation
Flow Type			
Materials of Construction	Stainless steel	Stainless steel	
Column Height	3.86	3.84	2.4
Column Diameter	2.57	2.54	5.3
Cross Sectional Area	5.18	5.17	5.6
Volume	20	21	4.8
Space Time	0.43	0.42	2.3
Space Velocity	2.32	2.34	6.3
Thickness	18.63	18.65	3.1
Corrosion allowance	2.00	2.00	0.00

In Table 4.13 the design parameters such as Column Height, Column Diameter, Cross-sectional Area, Volume, Space time, Space Velocity, Thickness and Corrosion Allowance was compared with Hysys simulation and Manual calculation and the maximum deviation was found to be 6.3%.

Figure 14: Table 4 . 13 :

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Design/Sizing Item	Hysys Simulation	Manual Calculation	% Deviation
Flow Type			
Materials of Construction	Stainless steel	Stainless steel	
Column Height (m)	5.54	5.56	0.36
Column Diameter(m)	3.72	3.71	1.40
Cross Sectional Area(m ²)	10.80	10.79	1.30
Volume(m ³)	60.02	60.00	3.30
Space Time(hr)	0.74	0.75	1.33
Space Velocity(hr ⁻¹)	1.35	1.33	6.06
Thickness(mm)	21.60	21.59	1.67
Corrosion allowance(mm)	2.00	2.00	0.00

In Table 4.14 the design parameters such as Column Height, Column Diameter, Cross-sectional Area, Volume, Space time, Space Velocity, Thickness and Corrosion Allowance was compared with Hysys simulation and Manual calculation and the maximum deviation was found to be 6.06%.

Figure 15: Table 4 . 14 :

4

Design/Sizing Item	Hysys Simulation	Manual Calculation	% De- via- tion
Equipment Name	Shell and tube heat exchanger	Shell and tube heat exchanger	
Objective.	Cooling the reactor effluent	Cooling the reactor effluent	
Equipment Number	U-007	U-007	
Designer	MUESI NOBLE PG.2017/02618 MUESI NOBLE PG.2017/02618		
Type	Split ring floating head (two shell four tubes)	Split ring floating head (two shell four tubes)	
Utility	Brackish Water	Brackish Water	
Insulation	Foam Glass	Foam Glass	
Heat load Q (kw)	945	947	0.0
Heat transfer Area (m ²)	53.4	53.5	0.2
LMTD (°C)	32	32.1	0.2
U (W/m ² K)	640	640.3	0.1
Inlet temperature) °C)	80	80	0.0
Shell Diameter (mm)	476	476	0.0
Shell coefficient W/m ² C	1516	1516.4	0.2
Outlet temperature (°C)	40	40	0.0
Baffle spacing (25% cut)	95.2	95.2	0.0
Shell material	Carbon steel	Carbon steel	
Inlet temperature (°C)	25	25	0.0
Tube Diameter (mm)	20/16	20/16	0.0
od/id)	20/16	20/16	
Tube length (m)	4.83	4.83	0.0
Pitch type	Triangular	Triangular	
Outlet temperature (°C)	40	40	0.0
Number of Tubes	172	172.2	0.0
Tube material	Carbon alloy	Carbon alloy	
Pitch	25mm	25mm	0.0

Figure 16: Table 4 .

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