The Kinematics of a Puma Robot using Dual Quaternions

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Abstract

This chapter presents mainly, on the light of both main concepts; The first being the screw motion or/ and dual quaternions kinematics while the second concerns the classical 'Denavit and Hartenberg parameters' method, the direct kinematics of a Puma 560 robot.Kinematics analysis studies the relative motions, such as, first of all, the displacement in space of the end effector of a given robot, and thus its velocity and acceleration, associated with the links of the given robot that is usually designed so that it can position its end-effector with a three degree-of-freedom of translation and three degree-of-freedom of orientation within its workspace.

Index terms— dual quaternions, forward kinematics, screw motion, denavit and hartenberg parameters.

1 Introduction

any research students have a great deal of trouble understanding essentially what quaternions are [1], [2], [3] and how they can represent rotation. So when the subject of dualquaternions is presented, it is usually not welcomed with open arms. Dual-quaternions are a break from the norm (i.e., matrices) which we hope to entice the reader into supporting willingly to represent their rigid transforms.

The reader should walk away from this analysis with a clear understanding of what dual-quaternions are and how they can be used [4]. First we begin with a short recent and related work that emphasises the power of dual-quaternions:

The dual-quaternion has been around since 1882 [5], [6], [7] but has gained less attention compared to quaternions alone; while the most recent work which has taken hold and has demonstrated the practicality of dual-quaternions, both in robotics and computer graphics can be resumed in: -Kavan [8] demonstrated the advantages of dual-quaternions in character skinning and blending. -Ivo [9] extended Kavan's work with dual-quaternions and q-tangents as an alternative method for representing rigid transforms instead of matrices, and gives evidence that the results can be faster with accumulated transformations of joints if the inferences per vertex are large enough. -Selig [10] address the key problem in computer games. -Vasilakis [11] discussed skeleton-based rigid-skinning for character animation. -Kuang [12] presented a strategy for creating real-time animation of clothed body movement.-Pham [13] solved linked chain inverse kinematic (IK) problems using Jacobian matrix in the dual-quaternion space. -Malte [14] used a mean of multiple computational (MMC) model with dualquaternions to model bodies. -Ge [15] demonstrated dual-quaternions to be an efficient and practical method for interpolating three-dimensional motions. -Yang -Hsing [16] calculated the relative orientation using dualquaternions. -Perez [17] formulated dynamic constraints for articulated robotic systems using dualquaternions.-Further reading on the subject of dual numbers and derivatives is presented by Gino [18].

In the last three decades, the field of robotics has widened its range of applications, due to recent developments in the major domains of robotics like kinematics, dynamics and control, which leads to the sudden growth of robotic applications in areas such as manufacturing, medical surgeries, defense, space vehicles, under-water explorations etc.

To use robotic manipulators in real-life applications, the first step is to obtain the accurate kinematic model [19]. In this context, a lot of research has been carried out in the literature, which leads to the evolution of

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new modeling schemes along with the refinement of existing methodologies describing the kinematics of robotic manipulators.

First of all, examples of basic solid movements such as rotations, translations, their combinations and general screw motions are studied using both (4x4) rigid body transformations and dual quaternions so that the reader could compare and note the similarity of the results obtained using one or the other method. Both dual quaternions technique as well as its counterpart the classical 'Denavit and Hartenberg parameters method' are finally applied to the first three degree of freedom of a Puma 560 robot. Finally, we and the reader, can observe that the two methods confirm exactly one another by giving us the same results for the considered application, while noting that the fastest, simplest more straightforward and easiest to apply method, is undoubtedly the one using dual quaternions. As a result this chapter may as well act as a beginners guide to the practicality of using dual-quaternions to represent the rotations and translations in character-based hierarchies.

elements of screw theory can be traced to the work of Chasles and Poinsot [20], [21], in the early 1800's and Whittaker [22]. Using the theorems of Chasles and Poinsot as a starting point, Robert S. Ball developed [23] a complete theory of screws which he published in 1900. Throughout the development of kinematics, numerous mathematic theories [24] and tools have been introduced and applied. The first pioneer effort for kinematic modeling of robotic manipulators was made by Denavit and Hartenberg in introducing a consistent and concise method to assign reference coordinate frames to serial manipulators, allowing the (4×4) homogeneous transformation matrices to be used (in 1955) [25], followed by Lie groups and Lie Algebra by J.M Selig and others, [26], [27], [28]) and quaternions and dual quaternions introduced by Yang and Freudenstein (1964) [29], see also Bottema and Roth (1979) [30] and McCarthy (1990) [31].The original D-H parameter method has many counterparts: Distal variant, proximal variant, ?to name but a few. There even exist different options for these counterparts.

In this method, four parameters, popularly known as D-H parameters, are defined to provide the geometric description to serial mechanisms. Out of the four, two are known as link parameters, which describe the relative location of two attached axes in space. These link (See appendix 10,3,1.) parameters are: The link length (a_i) and the link twist (? i).

The remaining two parameters are described as joint parameters, which describe the connection of any link to its neighboring link. These are the joint offset (d_i) and the joint angle (? i).

Modeling the movement of the rigid body by the theory of the helicoidal axis: a combination of an amount of rotation about and an amount of translation along a certain axis, hence the term helicoidal axis is used in various fields such as computer vision and biomechanics. The application of this theory in the field of robotics is taking more and more space. We can consider the motion of a joint segment as a series of finite displacements. In this case the movement is characterized by an angle of rotation about and an amount of translation along an axis defined in space by its position and its orientation. This axis is referred to as the finite helicoidal axis (FHA), because of the discretization of the movement into a series of displacements. On the other hand and by taking the continuity of the movement into account, this movement will be characterized by a rotational speed (angular velocity) about and translation speed along an axis defined by the instantaneous position and orientation in space. One speaks in this case of an instantaneous helicoidal axis (IHA).The application of the helicoidal theory with its two versions (FHA and IHA) is used to describe and understand the joint movement, and to study in biomechanics, for example, the different positioning techniques of prothèses. Thus there are several methods to estimate the helicoidal axis from a set of points representing a rigid body.

Any displacement of a rigid body is a helicoidal motion which may be decomposed into an angular rotational movement about and a linear translational movement along a certain axis in 3D space. The methods differ in the way of mathematically representing these two movements. These movements can be expressed using rotation matrices and translation vectors, homogeneous matrices, unit quaternions, dual quaternions, ... The two representations; using (3x3) matrices or (4x4) homogeneous matrices and dual quaternions will be simultaneously used for all and each examples or applications studied so that comparisons for each case could be done.

2 II.

3 Dual Quaternions a) « Product type » dual quaternions

The dual quaternions have two forms thus two readings which are complementary and simultaneous: The first is the « product type » description:?? ? ?? = ??? ?? + ?? ?? ?? .?? ?? 2 ? With: ?? ?? = ?cos ð ??"ð ??" 2 , n. sin ð ??"ð ??" 2 ? = ?cos ð ??"ð ??" 2 , sin ð ??"ð ??" 2 . ?? ?? , sin ð ??"ð ??" 2 . ?? ?? , sin ð ??"ð ??" 2 . ?? ?? ?

and ?? ?? = (0,??? ?? , ?? ?? , ?? ?? ?= (0 ,{??}) Then, the transformation is: Note that this form resembles that used for classic quaternions; using the dual angle and the dual unitary vector instead of the classical ones.?? ? ?? = ??? ?? + ?? ?? ?? .?? ?? 2 ? = ?cos

And as a matter of fact: The screw displacement is the dual angle ?? ? = ?? + ?? d, along the screw axis defined by the dual vector ?? ? or ??? or in our case ?? ? = n +?? m; such that we will obtain (respecting the rules of derivation and multiplication of dual numbers), dual vectors, quaternions and dual quaternions (see appendix 10,2. and eq (A15)):?? ? =?cos ?? ? 2 , sin ?? ? 2 ?? ?? = [cos ?? 2 ? ?? ?? 2 sin ?? 2 , (sin ?? 2 +

105 ?? ?? 2 cos ?? 2) (n +?? m)] = cos ?? 2 ??? ?? 2 sin ?? 2 , n sin ?? 2 +?? (n ?? 2 cos ?? 2 + sin ?? 2 m) =
106 (cos ?? 2 , n sin ?? 2) + ??(? ?? 2 sin ?? 2 , sin ?? 2 m + n ?? 2 cos ?? 2) (2)
107 The geometric interpretation of these quantities is related to the screw-type motion. The angle ?? is the
108 angle of rotation around n, the vector unit n represents the direction of the rotation axis. The element d is the
109 translation or the displacement amplitude along the vector n, m being the vector moment of the vector axis n
110 relative to the origin of the axes. The vector m is an unambiguous description of the position of an axis in space,
111 in accordance with the properties of Plückér coordinates defining lines in space.
112 This form gives another interesting use: Whereas the classics quaternions can only represent rotations whose
113 axes pass through the origin O of the coordinate system (O, x, y, z), the dual quaternions can represent rotations
114 about arbitrary axes in space, translations as well as any combination of both these two basic spatial motions.
115 These two forms « product type » eq (1) or « ???????? ???????? » ???? (2) represent the same motion that
116 describe the same movement 'the screw motion': The vector m = (m x , m y , m z) is the moment of the vector
117 n about the origin of reference (O, x, y, z); it is named the moment of the axis n, with: ?? ? = ?? + ?? d with d
118 being the amplitude of the translation along the dual vector ?? ? = n +?? m with m = p x n (the green vector
119 see figure 1) that defines the vector according to Plücker coordinates, p, (the blue vecor), being the vector that
120 gives the position of n ,(the red vector), using the vector OO 1 (see figure (1)).III.
121 The parameters of the transformation, the angle ??, the axis of rotation n, the magnitude of the translation d
122 and the moment m are the four characteristics of all, any and every 3D rigid body transformation (4x4) matrix,
123 a screw motion or a helicoidal movement of any kind (or type).
124 Using quaternions the first rotation will be written; since?? 1 2 = ?? 4 then cos ?? 1 2 = sin ?? 1 2 = ?2 2
125 ?? 1 = (?2 2 , ?2 2 , 0 , 0) ; having ?? 1 2 = ?? 4 then cos ?? 1 2 = sin ?? 1 2 = ?2 2
126 The second rotation will have the form:?? 2 = (?2 2 , 0 , ?2 2 , 0)
127 The final composition of the two movements will be given by the quaternion ?? such that:?? = ?? 2 . ?? 1 =
128 (?2 2 , 0 , ?2 2 , 0) . (?2 2 , ?2 2 , 0 , 0) = (1 2 , 1 2 , 1 2 , ?**1 2**
129) Using quaternion's definition (A5) and quaternions properties:?? = ((1 2 , ?3 2 (1 ?3 , 1 ?3 , ? 1 ?3)) or
130 ((1 2 ,? ?3 2 (? 1 ?3 ,? 1 ?3 , 1**?3**
131))
132 It is then easy to extract both the amplitude and the resulting axis of the rotation from the result q: In fact
133 the two solutions represent the same and similar solution since for any q we have q (??, n) = q (???, ?n).
134 Using our classical (3x3) rigid transformations we get:R 21 = R 2 .R 1 = ? 0 0 1 0 1 0 ?1 0 0 ? ? 1 0 0 0 0 ?1
135 0 1 0 ? = ? 0 1 0 0 0 ?1 ?1 0 0 ?
136 Here it is very important to note that unlike the quaternion method we cannot extract the needed results
137 easily and straightforwardly but we must follow a long and sometimes complicated process (determinant, trace,
138 Whichever used technique we will find: A rotation of ?? =)) and that will imply ?? i = 120 º around the axis n
139 = Using MATLAB (See Appendix 10,1.) we can calculate easily both the two quaternions multiplications: q=
140 n1 = q2.q1 and q i = n2 = q1.q2 and the two equivalent product of matrices1 ?3 ? 1 1 1 , or ?? i = ? 120 º
141 around the axis (-n) = 1 ?3 ?? ?1 1 ?1 ; Which of course will imply that: ?? 1 . ?? 2 ? ?? 2 . ?? 1 Using
142 matrices : R i = R 1 R 2 = ? 1 0 0 0 0 ?1 0 1 0 ? ? 0 0 1 0 1 0 ?1 0 0 ? = ? 0 0 1 1 0 0 0 1 0 ? ? R ii = R 2
143 RR 21 = R 2 R 1 and R i = R 1 R 2 .
144 The Kinematics of a Puma Robot using Dual Quaternions IV.

4   Important Notes: What about Translations?

146 We must recall that rotations act on translations, the reverse being not true; in fact when multiplying by blocks:
147 For a rotation followed by a translation:? ?? ?? 0 1 ? ? ?? 0 0 1 ? = ? ?? ?? 0 1
148 ? ; the rotation is not affected by the translation.
149 While for a translation followed by a rotation:? ?? 0 0 1 ? ? ?? ?? 0 1 ? = ? ?? ???? 0 1
150 ? ; the translation is affected by the rotation.
151 When translations are performed first we can thus assume that the translation vector of the resulting matrix
152 product; Rt acts as the translation vector t of a rotation followed by a translation .Or more generally speaking
153 considering two six degree of freedom general rigid body transformations T 1 followed by T 2 we will have:T 2
154 .T 1 = ? ?? 2 ?? 2 0 1 ? ? ?? 1 ?? 1 0 1 ? = ? ?? 2 ?? 1 ?? 2 ?? 1 + ?? 2 0 1 ? = ? ?? ?? 0 1 ?
155 The translation vector t of the product of the two transformations is? ?? 1 = ?? 2 ?? 1 + ?? 2 = ? ?? 2 0 0
156 1 ? ? ?? 1 1 + ? ?? 2 1
157 The same analysis as the last one could then be done whatever the order and the number of the successive
158 transformations being performed over the rigid body: The final result of the products of all the undertaken rigid
159 body transformations will be finally the helicoidal, the helical or the screw motion given by the (4x4) matrix:[T]
160 = T n ? T i ...T 2 .T 1 = ? ?? ?? 0 1 ?**(3)**
161 With T i representing either a rotation, a translation, a rotation followed by a translation, a translation
162 followed by a rotation or even simply a no movement (ie: the 4x4 identity matrix I).
163 Any screw motion would be given by the following (4x4) matrix [T]:? ?? ?? 0 1 ? = ? ?? ?? 0 1 ? ? ?? (??,
164 ??) ? p 2?? ?? 0 1 ? ? ?? ? ?? 0 1 ? = ? ??(??, ??) ? p 2?? ?? + (?? ? ??(??, ??))?? 0 1 ? = [T]**(3)**
165 The middle matrix is a screw about a line through the origin; that is, a rotation of ?? radians around the axis
166 n followed by a translation along n. The outer matrices conjugate the screw and serve to place the line at an

arbitrary position in space. The parameter p is the pitch of the screw, it gives the distance advanced along the axis for every complete turn, exactly like the pitch on the thread of an ordinary nut or bolt. When the pitch is zero the screw is a pure rotation, positive pitches correspond to right hand threads and negative pitches to left handed threads.

To show that a general rigid motion is a screw motion, we must show how to put a general transformation into the form derived above. The unit vector in the direction of the line n is easy since it must be the eigenvector of the rotation matrix corresponding to the unit eigenvalue.(This fails if R = I, that is if the motion is a pure translation). The vector u is more difficult to find since it is the position vector of any point on the rotation axis. However we can uniquely specify u by requiring that it is normal to the rotation axis. So we impose the extra restriction that n.u = 0. So to put the general matrix ? ?? ?? ?? ?? ? into the above form we must solve the following system of linear equations: All we need to do now is to solve the equation system:?? ?? ???? ?? + (?? ? ??)?? = t Now n.Ru = n.u = 0,(?? ? ??)?? = (t -(??. t) ??) ;

This is possible even though det (?? ? ??) = 0, since the equations will be consistent.

This entire analysis established through this long paragraph concerning the helicoidal motion or rigid (4x4) transformation matrix [T] is contained in only one line enclosed in its counterpart dual quaternion ?? ? of the form:

The Kinematics of a Puma Robot using Dual Quaternions Year 2020 Global Journal of Researches in Engineering ( ) Volume Xx X Issue I V ersion I H V. Screw Motion ?? ? = ?cos ?? ? 2 , sin ?? ? 2 ?? ?? = ?? ? ?? . . ?? ? ?? . . ?? ? 2 .?? ? 1 = ?cos ?? 2 ,

sin

T 2 .T 1 = ? 1 0 0 1 0 0 0 1 ?1 0 0 0 0 0 0 1 ? ? 0 0 1 0 0 ?1 1 0 0 0 1 0 0 0 0 1 ? = ? 0 0 1 1 1 0 0 1 0 0 0 1 0 0 0 1 ?**(4)**

The rotation part of the product corresponds to that of the precedent example of successive rotationsR i = R 1 R 2

with amplitude ?? = ; its translation part being t = ? 1 0 1

We can find its pitch p =2?? ?? (n. t) = 2?? 2?? 3 1 ?3 ? 1 1 1 . ? 1 0 1 = 6 ?3 = 2?3

The axis of rotation will keep its same original direction n =1 ?3 ? 1 1 1

, it will go through a new centre C given by the shifting vector u which could be found by the linear equations system :(I -R) u = t - ?? ?? ???? n ?? 1 0 ?1 1 1 0 0 ?1 1 ? ? ?? ?? ?? ?? ?? ?? = ? 1 0 1 ? 2?? 3.2?? 6 ?3 ? ? ? ? ? 1 ?3 1 ?3 1 ?3 = ? 1 0 1 ? 2 ?3 ? ? ? ? ? 1 ?3 1 ?3 1 ?3 = ? ? ? ? ? ? 1 3 2 3 1 3

The vector translation T (or t) of the movement ? 1 0 1 is the sum of the two main perpendicular vectors T 1 + T 2 such as T 1 is to be chosen parallel to n while the rest T 2 is the translation vector part responsible for the shifting of the axis to its final position through the new center C as such we have: So that to confirm these results ; we can finally check the following conjugation matrices :T 1 = ? ? ? ? ?? ? ? 0 0 1 0 1 0 0 1 0 0 ?2 3 ?1 3 0 0 0 1 ? ? ? ? ? ? ? 0 0 1 2 3 1 0 0 1 0 0 2 3 2 3 0 0 0 1 ? ? ? ? ? ? ? 0 0 1 0 1 0 0 1 0 0 2 3 1 3 0 0 0 1? ? ? = ? 0 0 1 1 1 0 0 1 0 0 0 1 0 0 0 1 ? ? (4) Or, ? ? ? 0 0 1 2 3 1 0 0 1 0 0 0 1 3 0 0 0 1 ? ? ? ? ? ? ? 0 0 1 2 3 1 0 0 1 0 0 2 3 2 3 0 0 0 1 ? ? ? ? ? ? ? 0 0 1 ?2 3 1 0 0 1 0 0 0 ?1 3 0 0 0 1 ? ? ? = ? 0 0 1 1 1 0 0 1 0 0 0 1 0 0 0 1 ? ? (4)

Or finally;? ? ? 0 0 1 1 3 1 0 0 1 0 0 ?1 3 0 0 0 1 ? ? ? ? ? ? ? 0 0 1 2 3 1 0 0 1 0 0 2 3 2 3 0 0 0 1 ? ? ? ? ? ? ? 0 0 1 ?1 3 1 0 0 1 0 0 1 3 0 0 0 1 ? ? ? = ? 0 0 1 1 1 0 0 1 0 0 0 1 0 0 0 1 ? ? (4)

Whenever necessary, Matlab was, throughout the chapter implemented, concerning all kinds of products or multiplication of quaternions or matrices.

5 VII.

The Same General Example using Dual Quaternions?? ? = ?? + ???? ?? = ?? ?? + ?? 2 ??? ?? ?? + ?? ?? ?? + ?? ?? ?????? ?? = ?? + ?? ???? 2

The two transformations T 1 and T 2 are basic centered helicoidal movements through the origin O of the axes, that can be written:

For the first movement around and along Oy:?? ? 1 = ?? 1 + ?? 2 ?? ?? 1 = ?? ? ?? = (c , 0 , s , 0) + ?? 2 (? s?? ?? , 0 , c ?? ?? , 0) = (cos ?? 4 , 0 , sin ?? 4 , 0) + ?? 2 (? sin ?? 4 . 1 , 0 , cos ?? 4 . 1 , 0) = (?2 2 , 0 , ?2 2 , 0) + ?? 2 (? ?2 2 , 0 , ?2 2 , 0)

followed by the second movement around and along Ox:?? ? 2 = ?? 2 + ?? 2 ?? ?? 2 = ?? ? ?? = (c , ?? , 0 , 0) + ?? 2 (? s?? ?? , c ?? ?? , 0, 0) = (cos ?? 4 , sin ?? 4 , 0, 0) + ?? 2 (? sin ?? 4 . 1 , cos ?? 4 . 1 , 0, 0) = (?2 2 , ?2 2 , 0 , 0) + ?? 2 (? ?2 2 , ?2 2 , 0 , 0)

The dual quaternion product of the two screw movements is: ?? ? 2 . ?? ? 1 = (?? 2 + ?? 2 ?? ?? 2).(?? 1 + ?? 2 ?? ?? 1) = ?? 2 . ?? 1 + ?? 2 (?? 2 . ?? ?? 1 + ?? ?? 2 . ??

At this stage we know the complete integrality of informations concerning this movement thanks to our magic, rapid and powerful dual quaternion :The rotation part, as seen before, having amplitude ?? = We can also have the vector part: ?m sin?? 2 + ?? 2 ?? cos ?? 2 ? = (0 , 0 ,**1 2**

) which implies:m x ?3 2 + ?3 3 1 ?3 1 2 = m x ?3 2 + 1 6 = 0 ; m y ?3 2 + ?3 3 1 ?3 1 2 = m y ?3 2 + 1 6 = 0 and m z ?3 2 + ?3 3 1 ?3 1 2 = m z ?3 2 + 1 6 = 1 2

We can then deduce the vector moment m =? ? ? ? ? ?1 3?3 ?1 3?3 2 3?3

Finally we can have the right position of the shifted axis u that have the same direction as the rotation axis n by defining the coordinates u_x, u_y and u_z of a point or a center C belonging to it so that:$m = u$? n Or ? ? ? ? ? ?1 3?3 ?1 3?3 2 3?3 = ? $u_x u_y u_z$? 1 ?3 ? 1 1 1 = 1 ?3 ? u_y ? $u_z u_z$? $u_x u_x$? u_y implying that: u_y ? u_z = ?1 3 ; u_z ? u_x = ?1 3 and u_x ? u_y = 2 3

Which confirm the same obtained results eq (5) using the (4x4) rigid transformation matrix:?? ?? ? ?? ?? = 1 3 ; ??? ?? + ?? ?? = ?**2 3**

; and? ?? ?? + ?? ?? = 1 3**(5)**

VIII. Application 2: Kinematics of the Puma 560 Robot

The first three joints of this manipulator (Waist, Shoulder, Elbow) characterize for the first joint to be a rotation about a vertical axis , for the second and the third rotations about horizontal axes whose movements are identified by the variables q_1 , q_2 , and q_3 . The last three joints, which constitute the wrist of the robot arm, are characterized by the rotations q_4 , q_5 , and q_6 whose axes intersect at the center of the wrist (See appendix 10,3. Figures (3),(4) and Table 1 for the forward kinematic solution using the Denavit and Hartenberg convention.

The elegant , most accurate , rapid and finally the best manner to get the forward kinematic solutions of this Puma 560 robot is to use the dual quaternions:

For the sake of comparaison let us choose the same home position for the robot with its geometry (a_i and d_i) given in table (1) and the same absolute home initial frame (x_0 , y_0 , z_0) with its origin O taken in link1 at the intersection of the base axis with the link1 axis (see figure (3)), assuming mobile frames at the centers of the six rotations: (x_n , y_n , z_n) which axes remain parallel to the The Kinematics of a Puma Robot using Dual Quaternions 'home position' or initial axes (x_0 , y_0 , z_0). Let us begin, with the first two rotations using either equations A3 or A14 from appendix 10,2,1. to find the new vector position of the center O_3 (a_2 , d_2 , 0):?? ? 1 ?? ? 2 ?? ? ?? ?? ? ? 2 * ?? ? ? 1 * = ?? ? 1 (?? ? 2 ??? ? ??) ?? ? ? 2 * ??? ? ? 1 * (7) ?? ? 2 ?? ? ?? ?? ? ? 2 * = (c_2 , 0 , s_2 , 0) [1+ ?? (a_2 , d_2 , 0)] (c_2 , 0 , ?s_2 , 0)

Using correctly the rules for both quaternions eq (A1) and dual quaternions multiplications eq (A7) we have :?? ? 2 ?? ? ?? = (c_2 , 0 , s_2 , 0) + ?? (?$s_2 d_2$, $c_2 a_2$, $c_2 d_2$, ?$s_2 a_2$)

and?? ? 2 ?? ? ?? ?? ? ? 2 * = 1 + ?? (0 , $a_2 \cos$?? 2 , d_2 , ?$a_2 \sin$?? 2) thus ?? ? 1 ?? ? 2 ?? ? ?? ?? ? ? 2 * ?? ? ? 1 * = (c_1 , 0 , 0 , s_1)[1 + ?? (0 , $a_2 \cos$?? 2 , d_2 , ?$a_2 \sin$?? 2) (c_1 , 0 , 0 , ? s_1)

Performing the product and using the trigonometric properties we can have the new quaternion vector position:1 + ?? (0 , $a_2 \cos$?? 2 $\cos$?? 1 ? ?? 2 ?????? ?? 1 , $a_2 \cos$?? 2 ?????? ?? 1 + $d_2 \cos$?? 1 , ?$a_2 \sin$?? 2)

or the three coordinates vector:? a ?? 2 ?????? ?? 1 ? ?? 2 ?????? ?? 1 a_2 ?????? ?? 2 ?????? ?? 1 + ?? 2 ?????? ?? 1 ?a_2 ?????? ?? 2

This result is confirmed (see appendix 10,3,2.) by the fourth or last column of the matrix :?? 0 2 = ?? 0 1 ?? 1 2 = $R_1 R_2$ = ? ?? 1 0 -?? 1 0 ?? 1 0 ?? 1 0 0 ?1 0 0 0 0 1 ? ? ?? 2 ??? 2 0 ?? 2 ?? 2 ?? 2 ?? 2 0 ?? 2 ?? 2 0 0 1 ?? 2 0 0 0 1 ? = ? ?? 1 ?? 2 ??? 1 ?? 2 ? ?? 1 ?? 2 ?? 1 ?? 2 ? ?? 2 ?? 1 ?? 1 ?? 2 ??? 1 ?? 2 ?? 1 ?? 2 ?? 1 + ?? 2 ?? 1 ??? 2 ??? 2 0 ??? 2 ?? 2 0 0 0 1

6 ?

The third rotation of the third link is around the axis $O_3 y_3$, with the center O_3 being displaced or shifted and thus having the position coordinates with respect to the asolute frame O_3 (a_2 , d_2 , 0).

Note: The conjugation (technique could be used in its dual quaternion form or its (4x4) rigid transformation form. The dual quaternion (definition (2) may be used instead; The moment m, w-r -t the axis of rotation?? ? = ?? ? =?$\cos y_3$, is m = ? a_2 ?? 2 0 ?? 0 1 0 = ? 0 0 a_2 so that ?? ? 3 = [?? 3 , (0, ?? 3 , 0)]+ ???0, {(0,0, a_2 ?? 3 }? (?? ? 1 ?? ? 2)?? ? 3 ?? ? ?? ?? ? ? 3 * (?? ? ? 2 * ?? ? ? 1 *) = (c_1 , 0 , 0 , s_1) (c_2 , 0 , s_2 , 0) ?? ? 3 ?? ? ?? ?? ? ? 3 * (?? 2 , 0 , ??? 2 , 0) (?? 1 , 0 , 0 , ??? 1)

To find the new vector position of the wrist center O_4 :($a_2 + a_3$, $d_2 + d_3$, 0) = (A, D, 0) result of the three successives rotations we must start from the central operation namely :?? ? ??3 = ?? ? 3 ?? ? ?? ?? ? ? 3 * = [(?? 3 , 0 , ?? 3 , 0)+ ?? (0,0,?? 2 ?? 3)] [(1+?? (A, D, 0))] [?? ? ? 3 *] = [(?? 3 , 0 , ?? 3 , 0) + ??(0,0,?? 2 ?? 3)+??(??? 3 D, ?? 3 A , ?? 3 D,??? 3 A)] [?? ? ? 3 *]= [(?? 3 , 0 , ?? 3 , 0 +??(??? 3 D, ?? 3 A , ?? 3 D , ?? 3 (?A)] [(?? 3 , 0 , ??? 3 , 0)+ ?? (0,0,?? 2 ?? 3)] = (?? 3 2 + ?? 3 2 , 0 , ??? 3 ?? 3 + ?? 3 ?? 3 , 0) +??(??? 3 ?? 3 D + ?? 3 ?? 3 D , ?? 3 2 ?? 2 + ?? 3 2 A + ?? 3 2 (?? 2 ?A), ?? 3 2 D + ?? 3 2 D , ?? 3 ?? 3 ?? 2 ??? 3 ?? 3 A + ?? 2 ?? 3 ?? 3 ??? 3 ?? 3 A)

Using the basic trigonometric rules and properties we can write the solution vector:q ? v_3 = q ? 3 q ? v q ? ? 3 * = 1+ ? (0 , a_2 + $a_3 \cos$? 3 , d_2 + d_3 , ? $a_3 \sin$? 3) = 1+ ? (a_2 + $a_3 \cos$? 3 , d_2 + d_3 , ? $a_3 \sin$? 3)

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For a better use of space we may adopt to write our result dual quaternions vectors under the form:? ? ? scalar part O x coord. O y coord. O z coord.

So that the precedent result could be written ?? ? ??3 = ? 0 a 2 + a 3 cos ?? 3)](?? 2 , 0 , ??? 2 , 0) = (c 2 , 0 , s 2 , 0)? 1 + ?? ? ? 0 a 2 + a 3 cos ?? 3 d 2 + d 3 ? a 3 sin ?? 3 ? ? ?? ? ? 2 * ? = ? ? ? ? (?? 2 , 0 , ?? 2 , 0) + ?? ? ??? 2 (d 2 + d 3) ?? 2 (a 2 + a 3 cos ?? 3) ??? 2 a 3 sin ?? 3 ?? 2 (d 2 + d 3) ? ?? 2 a 3 sin ?? 3 ??? 2 (a 2 + a 3 cos ?? 3) ? ? ? ? ? ? (?? 2 , 0 , ??? 2 , 0) = (?? 2 2 + ?? 2 2 ,0, ??? 2 ?? 2 +?? 2 ?? 2 , 0)+?? ? ? ? ??? 2 ?? 2 (d 2 + d 3) + ?? 2 ?? 2 (d 2 + d 3) ?? 2 2 (a 2 + a 3 cos ?? 3) ??? 2 ?? 2 a 3 sin ?? 3 ?? 2 2 (d 2 + d 3) + ?? 2 2 (d 2 + d 3) ??? 2 ?? 2 a 3 sin ?? 3 ??? 2 2 (a 2 + a 3 cos ?? 3) ? ?? 2 2 a 3 sin ?? 3 ??? 2 ?? 2 (a 2 + a 3 cos ?? 3)??? 2 ?? 2 (a 2 + a 3 cos ?? 3) + ?? 2 2 a 3 sin ?? 3 ? ? ? ? = 1+ ?? ? ? ? 0 ?? 2 2 (a 2 + a 3 cos ?? 3) -?? 2 ?? 2 a 3 sin ?? 3 ?? 2 2 (d 2 + d 3) + ?? 2 2 (d 2 + d 3) ??? 2 ?? 2 a 3 sin ?? 3 ??? 2 2 (a 2 + a 3 cos ?? 3) ? ?? 2 2 a 3 sin ?? 3 -?? 2 ?? 2 (a 2 + a 3 cos ?? 3)??? 2 ?? 2 (a 2 + a 3 cos ?? 3) + ?? 2 2 a 3 sin ?? 3 ? ? ? = ? 0 cos ?? 2 (a 2 + a 3 cos ?? 3) ? a 3 sin ?? 2 sin ?? 3 (d 2 + d 3) ?a 3 cos ?? 2 sin ?? 3 ? sin ?? 2 (a 2 + a 3 cos ?? 3) ? =

We can finally get the transformed vector ?? ? ??2 :?? ? ??2 =1+ ?? [(a 3 cos (?? 2 + ?? 3) + a 2 cos ?? 2 , (d 2 + d 3) , ?a 3 sin (?? 2 + ?? 3) ?a 2 sin ?? 2)] (c 1 , 0 ,0 , s 1) ?? ? ??2 (?? 1 , 0, 0, ??? 1) = (c 1 , 0, 0, s 1) [1+?? (a 3 cos (?? 2 + ?? 3) + a 2 cos ?? 2 , (d 2 + d 3) , ?a 3 sin (?? 2 + ?? 3) ?a 2 sin ?? 2)] ?? ? ? 1 * (c 1 , 0 , 0 , s 1) ? ? ? ? ? 1 + ?? ? ? 0 a 3 cos (?? 2 + ?? 3) + a 2 cos ?? 2 d 2 + d 3 ?a 3 sin (?? 2 + ?? 3) -a 2 sin ?? 2 ? ? ? ? ? ? ? ?? ? ? 1 * ? = ? ? ? ? (?? 1 , 0, 0, ?? 1) + ?? ? ? a 3 ?? 1 sin (?? 2 + ?? 3) + a 2 ?? 1 sin ?? 2 a 3 ?? 1 cos (?? 2 + ?? 3) + a 2 ?? 1 cos ?? 2 ? ?? 1 (d 2 + d 3) ?? 1 (d 2 + d 3) + a 3 ?? 1 cos (?? 2 + ?? 3) + a 2 s 1 cos ?? 2 ?a 3 ?? 1 sin (?? 2 + ?? 3) -a 2 ?? 1 sin ?? 2) ? ? ? ? ? ? ? ?? ? ? 1 * ? =

The Kinematics of a Puma Robot using Dual Quaternions

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We can finally perform the first but last transformation given by the following dual quaternions products:(c 1 , 0 , 0 , s 1) (c 2 , 0 , s 2 , 0) ?? ? 3 ?? ? ?? ?? ? ? 3 * (?? 2 , 0 , ??? 2 , 0)(?? 1 , 0, 0, ??? 1) = ? (?? 1 , 0 , 0, ?? 1) + ?? ? a 3 ?? 1 sin (?? 2 + ?? 3) + a 2 ?? 1 sin ?? 2 a 3 ?? 1 cos (?? 2 + ?? 3) + a 2 ?? 1 cos ?? 2 ? ?? 1 (d 2 + d 3) ?? 1 (d 2 + d 3) + a 3 ?? 1 cos (?? 2 + ?? 3) + a 2 s 1 cos ?? 2 ?a 3 ?? 1 sin (?? 2 + ?? 3) -a 2 ?? 1 sin ?? 2 ? ? (?? 1 , 0 , 0, ??? 1) = (?? 1 2 + ?? 1 2 ,0, ??? 1 ?? 1 + ?? 1 ?? 1 ,0) + ?? ? ? ? a 3 ?? 1 ?? 1 sin (?? 2 + ?? 3) + a 2 ?? 1 ?? 1 sin ?? 2 ? a 3 ?? 1 ?? 1 sin (?? 2 + ?? 3) ? a 2 ?? 1 ?? 1 sin ?? 2 a 3 ?? 1 2 cos (?? 2 + ?? 3) + a 2 ?? 1 2 cos ?? 2 ? ?? 1 ?? 1 (d 2 + d 3) ? ?? 1 ?? 1 (d 2 + d 3) ? a 3 ?? 1 2 cos (?? 2 + ?? 3) ? a 2 ?? 1 2 cos ?? 2 ?? 1 2 (d 2 + d 3) + a 3 ?? 1 ?? 1 cos (?? 2 + ?? 3) + a 2 ?? 1 s 1 cos ?? 2 + a 3 ?? 1 ?? 1 cos (?? 2 + ?? 3) + a 2 ?? 1 ?? 1 cos ?? 2 ? ?? 1 2 (d 2 + d 3) ?a 3 ?? 1 2 sin (?? 2 + ?? 3) -a 2 ?? 1 2 sin ?? 2 ? a 3 ?? 1 2 sin (?? 2 + ?? 3) ? a 2 ?? 1 2 sin ?? 2 ? ? ? = 1+ ?? ? ? 0 a 3 ?? 1 2 ?? 23 + a 2 ?? 1 2 ?? 2 ? ?? 1 ?? 1 (d 2 + d 3) ? ?? 1 ?? 1 (d 2 + d 3) ? a 3 ?? 1 2 ?? 23 ? a 2 ?? 1 2 cos ?? 2 ?? 1 2 (d 2 + d 3) + a 3 ?? 1 ?? 1 ?? 23 + a 2 ?? 1 s 1 cos ?? 2 + a 3 ?? 1 ?? 1 ?? 23 + a 2 ?? 1 ?? 1 cos ?? 2 ? ?? 1 2 (d 2 + d 3) ?a 3 ?? 1 2 ?? 23 -a 2 ?? 1 2 sin ?? 2 ? a 3 ?? 1 2 ?? 23 ? a 2 ?? 1 2 sin ?? 2 ? ? With ?? 23 = cos (?? 2 + ?? 3) and ?? 23 = sin (?? 2 + ?? 3)

The result vector is then:? ???????? 1 (a 2 ???????? 2 + a 3 ?? 23) ? ???????? 1 (d 2 + d 3) ???????? 1 (a 2 ???????? 2 + a 3 ?? 23) + ???????? 1 ((d 2 + d 3) ? (a 2 ???????? 2 + a 3 ?? 23)

9 ?

Which is confirmed by the last column (see appendix (10, 3, 2.) of the matrix ?? 0 3 .

We can also, using the Denavit and Hartenberg formalism or the dual quaternions alike easily calculate the coordinates of the terminal element (or the end effector) and so the final positioning of our Puma 560 robot relative to the base or fixed absolute frame.

10 IX.

11 Conclusion

We hope that the reader should not get us wrong: We never pretend that the D-H parameters method is wrong or obsolete and that it should be a thing of the past; recognising that this important classical method was the precursor that enlightened the path to modern robotics; we only say that there exist through the DQ parameters another short, free of singularities and easy to work with, when dealing with robot direct kinematics. On the light of the obtained results one has to say that the most perfect (not suffering singularities of any kind), easiest and rapid way to perform a 3D rigid transformation of any sort is to use the dual quaternion that caracterise that movement. Most of all we are free to use the 3D space, being sure that no loss of degree of freedom or guinball lock of any sort can never happen. Using a D-H parameters method or any of its counterparts means a choice of different sort of embarassing and somehow awkward three axes frames to be created and then allocated to each arm/ link; 'providing' our robot or mecanism with different direction axes and angles with very much complicated choice of signs (concerning the directions and the angles alike) to be chosen subject to some rules depending on the chosen method and model of robot.

Choosing to use dual quaternions we only need to know the constants or values that concern the construction or space geometry of the given robot (directions (orientations and axes) , rotations ,distances, lengths of links)

345 to evaluate its kinematics without any threat to be lost in the maze or a jungle of choices .Most of all, it will
346 prevent us from using the only other existing method, or one of its options, which is that of the Denavit and
347 Hartenberg parameters that mainly consists of:

348 The Kinematics of a Puma Robot using Dual Quaternions Year 2020 Global Journal of Researches in
349 Engineering ( ) Volume Xx X Issue I V ersion I H 1. Choosing 3D frames attached to each link upon certain
350 conditions /conventions, 2. Schematic of the numbering of bodies and joints in a robotic manipulator, following
351 the convention for attaching reference frames to the bodies, this will help to create: 3. A table for exact definition
352 of the four parameters, a i , ? i , d i , and ? i , that locate one frame relative to another, 4. The (4x4) rigid
353 transformation matrix that will have the given form : ?? ?? ? ?? ?? . (See 10,3.)

354 This chapter provided a taste of the potential advantages of dual-quaternions, and one can only imagine the
355 further future possibilities that they can offer. For example, there is a deeper investigation of the mathematical
356 properties of dual-quaternions (e.g., zero divisions). There is also the concept of dual-dualquaternions (i.e., dual
357 numbers within dual numbers) and calculus for multi-parametric objects for the reader to pursue if he desires.

358 We should emphasize on the fact that Matlab software was used, throughout this work and whenever necessary,
359 concerning all kinds of products or multiplication of quaternions or rigid transformation matrices.

360 Finally we hope all efforts should be conjugated to create a common 'PROJECT MATLAB QUATER-
361 NION/MATRIX platform' to be used for the straightforward calculations and manipulation of Quaternions
362 and / or Dual Quaternions as well as conversions from or into 3D or 4D rigid body matrices.

12 X.

13 Appendices a) Quaternion-Matlab Implementation Class:

365 » % See paragraph 3; Example 1: Rotations represented by Quaternions » % A first rotation of angle ?/2 around
366 the x -axis ,q1 , followed by a rotation of angle ?/2 around the y -axis , q2 will result in a rotation given by the
367 product n1 = q2.q1 : » q1 =[cos(pi/4) sin(pi/4) 0 0]; q2 =[cos(pi/4) 0 sin(pi/4) 0]; » n1 = quatmultiply (q2,q1)
368 n1 = 0.5000 0.5000 0.5000 -0.5000 » % If the order is inversed the result will be given by the quaternion n2 =
369 q1.q2 » n2 = quatmultiply (q1,q2) n2 = 0.5000 0.5000 0.5000 0.5000 » % Using 3*3 matrices; if the rotation R1
370 is performed first the rotation product is R2*R1:R1 = [1 0 0;0 0 -1;0 1 0]; R2 = [0 0 1; 0 1 0;-1 0 0]; prod1 =
371 R2*R1 prod1 = 0 1 0 0 0 -1 -1 0 0 » % if the order is inversed the multiplication will be R1*R2: prod2 = R1*R2
372 prod2 = 0 0 1 1 0 0 0 1 0 i.

14 Quaternions or rotation representation

374 Quaternions were first discovered and described by the Irish mathematician Sir Rowan Hamilton in 1843. Indeed
375 quaternion's representation and axis-angle representation are very similar.

376 Both are represented by the four dimensional vectors. Quaternions also implicitly represent the rotation of
377 a rigid body about an axis. It also provides better means of key frame interpolation and doesn't suffer from
378 singularity problems.

379 The definition of a quaternion can be given as (s, m) or (s, ?? x , ?? y , ?? z) where m is a 3D vector, so
380 quaternions are like imaginary (complex) numbers with the real scalar part s and the imaginary vector part m.

381 Thus it can be also written as: s + ?? x i + ?? y j + ?? z k.

382 There are conversion methods between quaternions, axis-angle and rotation matrix.

383 Common operations such as addition, inner product etc can be defined over quaternions. Given the definition
384 of ?? 1 and ?? 2 :?? 1 = ?? 1 + ?? x1 ?? + ?? y1 ?? + ?? z1 ?? or ?? 1 = (?? 1 , m 1) ?? 2 = ?? 2 + ?? x2
385 ?? + ?? y2 ?? + ?? z2 ?? or ?? 2 = (?? 2 , m 2)

386 Addition operation is defined as:?? 1 + ?? 2 = (?? 1 + ?? 2 , m 1 + m 2) = (?? 1 + ?? 2) + (?? x1 + ??
387 x2)i + (?? y1 + ?? y2)j + (?? z1 + ?? z2)k

388 dot (scalar, inner): product operation(.) as:?? 1 . ?? 2 = ?? 1 . ?? 2 + m 1 . m 2

389 Quaternion multiplication is non commutative, but it is associative. Multiplication identity element is defined
390 as: (1, (0, 0, 0)) We can also perform the multiplication in the imaginary number domain using the definitions:??
391 2 = ?? 2 = ?? 2 = ?1; ??. ?? = ?? , ??. ?? = ?? , ??. ?? = ?? ; ??. ?? = ? ?? , ??. ?? = ? ?? , ??. ?? = ? ??

392 Equations (A1) to (A15) state the definitions, rules and properties of dual quaternion algebra. Quaternion
393 multiplication (?) is defined as:?? 1 ??? 2 = (?? 1 . ?? 2 -m 1 . m 2 , ?? 1 . m 2 + ?? 2 . m 1 + m 1 ?m 2)
394 (A1)

395 Each quaternion has a conjugate ?? * (except zero quaternion) defined by:?? * = (s, -m) (A2)

396 and an inverse ?? ?1 = (The Kinematics of a Puma Robot using Dual Quaternions rotations can be combined
397 into one unit quaternion q R = q R1 .q R2 . q R3 .... q RN It is also possible to rotate a vector directly by using
398 quaternion multiplication. To do this, we must define a 3D vector V = (v x , v y , v z) that we want to rotate
399 in quaternion definition as q v = (0, v) = 0 + v x i+ v y j+ v z k. The rotated vector V ? = (v x ?, v y ?, v z
400 ?) can be defined asq v' = (0, v ?) = 0 + v x ?i + v y ?j + v z ?k

401 Noting that, in quaternion rotation ?? ?1 = ?? * (For unit quaternion). So, rotation of q v by quaternion q
402 can be calculated as:q v' = q ? q v ? ?? ?1 = q ? q v ? ?? * (A3)

403 And, assuming another quaternion rotation p, two rotations can be applied to the vector V such as:q v' = p
404 ?(q ? q v ? ?? ?1) ? ?? ?1 = (p ?q)? q v ? (?? ?1 ? ?? ?1) = C ? q v ? ?? ?1 (A4)

Providing that quaternion C = (p ? q) is a combinaison of the precedent quaternions q and p .

The equation implies that vector V is first rotated by the rotation represented by q followed by the rotation p.

A quaternion q that defines a rotation about (around) the axis n denoted by the unit vector (n x , n y , n z) of an angle ?? could be written as :q = cos ?? 2 + sin ?? 2

(n x i + n y j + n z k) (A5) This same quaternion represents a rotation of amplitude (? ??) around the opposite axis (?n)

ii. Dual quaternions Dual Quaternions (DQ) were proposed by William Kingdom Clifford in 1873.They are an extension of quaternions. They represent both rotations and translations whose composition is defined as a rigid transformation.

They are represented by the following eight dimensional vector:?? ? = (?? ?, ?? ?) = (s , ?? x , ?? y , ?? z , ?? ?? ?? , ?? ?? ?? , ?? ?? ?? , ?? ?? ??) = (?? ?, ?? ? , ?? ? , ?? ?) (A6)

Such that:?? ? = ?? + ???? ?? = s + ?? x i + ?? y j + ?? z k + ?? (?? ?? ?? + ?? ?? ?? + ?? ?? ?? + ?? ?? ??)

Dual quaternion multiplication is defined by:?? ? 1 ? ?? ? 2 = ?? 1 ? ?? 2 + ?? (?? 1 ? ?? 2 ?? + ?? 1 ?? ? ?? 2) (A7)

With ?? 2 = 0; ?? being the second order nilpotent dual factor. The dual conjugate (analogous to complex conjugate) is denoted by:?? ? ? = ?? -???? ?? (A8)

This conjugate operator can lead to the definition of the inverse of ?? ? which is: The translation T on the vector ?? ? can be computed by: ?? ? ?? ? = ?? ? ?? ??? ? ?? ??? ? ? ?? * So fortunately using def (A9), we have: ?? ? ?1 = 1 ?? ? = ?? ? ? ?? ? ? 1 ?? ? =?? ? ? ?? * = ?? ? ?? = 1+ ?? ?? 2 ,?? ? ?? ? = ???(?? ? ? ?? ? ?? ??? ? ? *) ? ???? * = (??? ? ?? ?) ? ?? ? ?? ? (?? ? ? * ? ???? *) = ?? ? ? ?? ? ?? ? ?? ?? * (A11)

It is very important to notice that the most inner transformation of the equation is applied first with an inside to outside manner. In eq (22), ?? ? is the first transformation followed by the second one ??.

The successive composition or combination of unit DQ rotation ?? ? ?? = R followed by a DQ translation ?? ? ?? = 1+ ?? 2 ??? ?? ?? + ?? ?? ?? + ?? ?? ?? ? will give:?? ? ?? ? ?? ? ?? = (1+ ?? 2 ??? ?? ?? + ?? ?? ?? + ?? ?? ?? ?) ? q R = q R + ?? 2 ??? ?? ?? + ?? ?? ?? + ?? ?? ?? ?? q R = R + ?? ???? 2 (A12) Its inverse being: (R + ?? ???? 2) ?1 = ?? * ? ?? * ?? 2

If the translation is applied first:?? ? ?? ? ?? ? ?? = ?? ? ?? ?(1 + ?? 2 ??? ?? ?? + ?? ?? ?? + ?? ?? ?? ?) = q R + ?? ? ?? ? ?? 2 ??? ?? ?? + ?? ?? ?? + ?? ?? ?? ? q R = R + ?? ???? 2 (A13) Its inverse being: (R + ?? ???? 2) ?1 = ?? * ? ???? * 2 v. Several transformations

Suppose that the vector V in its dual quaternion form ?? ? ?? = 1 + ?? ?? is under a sequence of rigid transformations represented by the dual quaternions ?? ? 1 , ?? ? 2 , . . . , ?? ? n . The resulting vector is encapsulated in the dual quaternion:1+ ?? ?? ? = ?? ? n ? (?? ? n?1 ? ?.? (?? ? 1 ? (1+ ?? ??) ? ?? ? ? * 1) ? ?..? ?? ? ? * n?1) ? ?? ? ? * n (A14) = (?? ? n ????? ? 1) ? (1+ ?? ??) ? (?? ? ? * 1 ? ?. ? ?? ? ? * n)

We denote the product dual quaternion as ?? ? = ?? ? n ????? ? 1 . The effect is equivalent to a single rigid transformation represented by ?? ?; namely,1+ ?? ?? ? = ?? ? ? (1+ ?? ??) ? ?? ? ? * .

Using dual numbers and plucker coordinates and introducing the following dual angle and dual vector we can write:?? ? = ?? + ???? and ?? ? = ?? + ????

It can be easily shown that:

The Kinematics of a Puma Robot using The steps for this technique are as follows:

Dual Quaternions cos ?? + ???? 2 = cos ?? 2 ??? ?? 2 sin ??

1. Numbering of the constituent segments of the manipulator arm from the base to the terminal element. The zero referential is associated with the base of it, and the order n to the terminal element (end effector); 2. Definition of the main axes of each segment:

? If z i and z i-1 do not intersect we choose x i so as to be the parallel with the axis perpendicular to z i and z i-1 . ? If z i and z i-1 are collinear, x i is chosen in the plane perpendicular to z i-1 .

3. Fix the four geometric parameters: d i , ? i , a i , ?? ?? (see Figure(4)) for each joint such as:

The Kinematics of a Puma Robot using Dual Quaternions ? d i coordinate of the origin O i on the axis z i-1 For a slide d i is a variable and for a hinge d i is a constant. ? ? i is the angle obtained by screwing x i-1 to x i around the axis z i-1 .For a slide ?? ?? is a constant and for a hinge ?? ?? is a variable. ? a i is the distance between the axes z i and z i-1 measured on the axis x i negative from its origin up to the intersection with the axis z i-1 .

? ? 1 is the angle between z i et z i-1 obtained by screwing z i-1 to z i around x i . Finally, the homogeneous DH displacement matrix [?? ????? ??] which binds together the rotation and the translation is formed . Its left upper part defines the rotation matrix ?? ????? ?? and on its right the translation vector [?? ???1 ??] : ? ?? ???1 ?? ?? ???1 ?? 0 0 0 1 ?**(9)**

The definition of the frames associated with the links according to the Denavit and Hartenberg convention is as follows: Link1: Frame (x 0 ,y 0 ,z 0) ;The origin O is taken in link1 at the intersection of the base axis with the link1 axis. z 0 axis of rotation, + z 0 upwards.+ y 0 coincides with the axis of the link 1 and the axis + z 1 .y 1 is parallel to the link 2.

Link 2: Frame (x 1 ,y 1 ,z 1) ;The origin coincides with the origin of the frame (x 0 ,y 0 ,z 0 ,) .z 1 axis of rotation, + z 1 is perpendicular to the link 2 and parallel to the axis + z 2 .+ y 1 downwards, superimposed
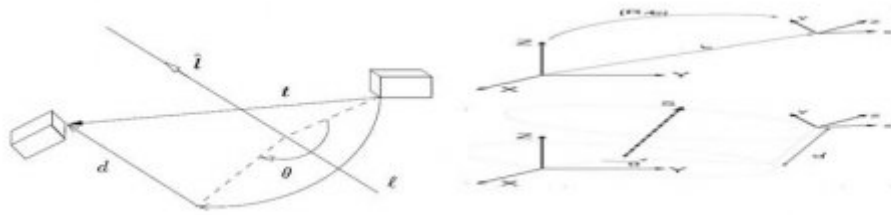
with the axis of the base and parallel with y 2 .+ x 1 is parallel to the link 2. Link 3: Frame (x 2 ,y 2 ,z 2) ;The origin is taken in link 2 at the intersection of the axis of the link 2 with the axis of the joint 3.z 2 axis of rotation, + z 2 is perpendicular to link 2 and axis z 3 .+ y 2 downwards, opposite with + z 3 .+ x 2 is parallel to the link 2. Link 4: Frame (x 3 , y 3 , z 3); The origin is taken in link 3.z 3 axis of rotation, + z 3 towards the wrist and perpendicular to +z 4 .+ y 3 is perpendicular to the link 2, and parallel to +z 4 .+ x 3 is parallel to the link 2.

Link 5: Frame (x 4 ,y 4 ,z 4) ;The origin is taken at the center of the wrist.z 4 axis of rotation, + z 4 is perpendicular to link 2 superposed with +z 5 . + y 4 is opposite to + z 5 .+ x 4 is parallel to link 2. Link 6: Frame (x 5 ,y 5 , z 5) ;The origin coïncides with the origin of the link (x 4 ,y 4 , z 4).z 5 axis of rotation, +z 5 towards the effector parallel to +z 6 .+ y 5 coïncides with the axis of joint 5.+ y 5 is perpendicular to the axis of joint 5.

The end effector: Frame (x 6 ,y 6 ,z 6) ;The origin coïncides with the origins of the links (x 4 ,y 4 , z 4) and (x 5 , y 5 , z 5). The distance d 6 is not shown in Table (I)..This distance varies according to the effector used for the application (the effector is the tool attached to the wrist on the last articulation of the robot for the manipulation of the objects). In this application the distance between the end of the effector and the axis of the wrist is assumed to be null d 6 = 0.

The dynamics of the last three articulations is negligible compared to the first three. Therefore, we have been interested in studying the movement of the three first joints of the PUMA 560 robot arm fixing the others to the original position (i.e., wrist attached to the original position: q 4 = q 5 = q 6 = 0).

Such that we will have :?? 0 2 = ?? 0 1 ?? 1 2 = ? ?? 1 0 -?? 1 0 ?? 1 0 ?? 1 0 0 ?1 0 0 0 0 0 1 ? ? ?? 2 ??? 2 0 ?? 2 ?? 2 ?? 2 ?? 2 0 ?? 2 ?? 2 0 0 1 ?? 2 0 0 0 1 ? = ? ?? 1 ?? 2 ??? 1 ?? 2 ? ?? 1 ?? 2 ?? 1 ?? 2 ? ?? 2 ?? 1 ?? 1 ?? 2 ??? 1 ?? 2 ?? 1 ?? 2 ?? 2 ?? 1 + ?? 2 ?? 1 ??? 2 ??? 2 0 ??? 2 ?? 2 0 0 0 1 ?**(15)**

We can also write:

And finally write ?? 03 = ?? 0 2 ?? 2 3 = ? ?? 1 ?? 2 ??? 1 ?? 2 ? ?? 1 ?? 2 ?? 1 ?? 2 ? ?? 2 ?? 1 ?? 1 ?? 2 ??? 1 ?? 2 ?? 1 ?? 2 ?? 2 ?? 1 + ?? 2 ?? 1 ??? 2 ??? 2 0 ??? 2 ?? 2 0 0 0 1 ? ? ?? 3 0 ?? 3 ?? 3 ?? 3 ?? 3 0 ? ?? 3 ?? 3 ?? 3 0 1 0 ?? 3 0 0 0 1 ? =

The Kinematics of a Puma Robot using Dual Quaternions [1] [2]

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Figure 1: 2 ?? 2 ?? 2)Figure 1 :

1

Figure 2: Example 1 :

Figure 3:

Figure 4:

i Numéro de la liaison	α_i (degrés)	θ_i Variable	a_i (mètres)	d_i (mètres)
1	-90	q_1	0	0
2	0	q_2	a_2	d_2
3	$+90$	q_3	a_3	d_3
4	-90	q_4	0	d_4
5	$+90$	q_4	0	0
6	0	q_5	0	$-$

Figure 5:

$$= \text{s } 2 + ?? \text{ x } \quad 2 \ + \ ?? \quad 2 + ?? \text{ z } \quad 2 = ?? \ ? \ ?? \qquad \begin{array}{c} 1 \ |??| \ ) \ 2 \ ?? \ * \ ; \ (?? \ ? \ 0) \\ \text{y} \end{array} \qquad \text{Where } |??| \ 2$$

*[Note: * = ?? * ? ??]*

Figure 6:

then $?? \ ? \ ?? \ ? = ?? \ ? \ ?? \ ??? \ ? \ ?? \ ??? \ ? \ ? \ ?? \ * = ?? \ ? \ ?? \ ??? \ ? \ ?? \ ??? \ ? \quad ??$
$?? = [1 + \ ?? \ ?? \ ?? \ ?? \ )] ? [1 + 2 \qquad\qquad\qquad\qquad\qquad 2$

Figure 7:

With ?? ???1 ??   =   ?????? ?? ?? ?????? ? ?? ?????? ?? ?? ????? ?? ?? ?????? ? ?? ????? ?? ?? ????
?

0   ?????? ? ??

And   ?? ???1 ??   =??? ?? ?????? ?? ??
                                                      ?? ?? ?????? ?? ??
                                                      ?? ??
    Figure (4??????? ?? ?????? ?? ?? sin ? ??   ???????   ??
                                                      ??????   ??   ??
                                                      ?????? ? ??
           0   0   0

Figure 8:

1

Figure 9: Table 1 :

.1 *

Combining these two conjugation operators will lead to the formalization of DQ transformation on 3D points. Use of both conjugations on ?? ? can be denoted ?? ? ? * .Using definitions (A2), (A6) and (A8) we finally have:

It is well know that we can use dual quaternions to represent a general transformation subject to the following constraints:

The DQ screw motion operator ?? ?: = (??, ?? ??) must be of unit magnitude:

This requirement means two distinct conditions or constraints:

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