

Linear Parallelepipedic Electric Machine: Static Study of the Moving Plate

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Abstract

Magnetic suspension, which replaces a mechanical guide means with a magnetic guide system, allows much lower losses. Magnetic suspension is a perfect candidate for holding and guiding the moving plate (rotor) of the linear parallelepipedic electric machine. It is an innovative solution to replace either conventional ball bearings or very sophisticated and expensive active magnetic bearings. The passive centering device with permanent magnets is used because it is combined with a system for compensating friction forces. In order to master the stable control of the centering device, we need to know all its static characteristics (without rotational movement). The normal force is calculated by the finite element method using the ANSYS MAXWELL software.

Index terms— magnetic suspension - mechanical guidance - magnetic guidance - linear machine

1 Introduction

The solutions envisaged to keep the moving plate (rotor) in translation at very high speed can be hydrodynamic or magnetic.

Hydrodynamic solutions can be implemented within the linear electric machine requiring high translation speeds. The principle is based on the use of on which the part in translation will be supported during its movement. The fluid in question can be a liquid lubricant such as oil or a gaseous carrier such as air under pressure. In both cases the film thus formed between the two fixed stators and the moving plate of the machine is very thin in relation to the total system. The capacities of this solution are very high. For example, the large alternators of the turbines of the Grand Maison dam, located in the French Alps, have a vertical axis of rotation and are equipped with axial oil stops for rotational guidance.

Magnetic fields are used to generate forces in many actuators. These actuators only operate with one degree of freedom. In the case of a linear machine in translation, for example, only magnetic forces that allow the moving plate (rotor) to move are used. When all the degrees of freedom of a moving plate in magnetic solution are controlled by electromagnets, the magnetic solution is said to be active as in figure ?? (the current is servo-controlled to keep the moving plate in a fixed position. The magnetic solution needs a power supply to operate, a power supply, a control and position sensors are required). In order to simplify some solutions, magnetic solutions based on magnets can be used. Stability will be ensured by one or more active bearings. These solutions are called passive solutions (passive solutions are autonomous and very simple to realize. They are with permanent magnets or variable reluctance).

2 Fig. 1: Active principle

Magnetic solutions are used in areas where mechanical systems reach their limits: high speed range (the absence of contact in a magnetic solution makes it possible to reach very high speeds); a range in which friction and wear must be minimized (friction is almost non-existent in a fully magnetic solution because there is no contact between moving and stationary parts and the bearing life is unlimited) ; a range in which high precision is

43 required (an active magnetic solution, controlled by a servo drive, allows the moving plate to be positioned with
 44 great precision) and, a range in which temperature variation is significant (a magnetic solution, made of suitable
 45 materials, is capable of operating at extreme temperatures) [1] [2].

46 Magnetic solutions are used in very different fields. They can support parts weighing a few grams such as
 47 electric meter disks up to machines weighing several tons such as linear electric machines. The main applications
 48 are: the application of magnetic solutions in space is the use of flywheels to stabilize a satellite or to store
 49 energy. Magnetic solutions can be used to equip machining spindles (Figure 2) and turbo molecular pumps
 50 can be used to obtain a very high vacuum thanks to a turbine rotating at high speed, (Figure 3). Industrial
 51 solutions are more focused on the hydrodynamic regime. There are self-lubricating plates or plates on the
 52 market, impregnated with specific oils and coated with a solid lubricating film: molybdenum disulfide (MoS₂).
 53 The self-lubricating plates allow a continuous operation. The performance and safety of the self-lubricating plates
 54 depend on the grade of metal alloy and the nature of the lubricant. The performance is related to operating and
 55 environmental conditions: dynamic load; speed; temperature; atmosphere and corrosive or non-oil compatible
 56 liquids. Maintenance is almost non-existent; the operation of the plates requires no maintenance. The presence
 57 of the lubricant film is permanent, resulting in a good coefficient of friction, silent operation and good corrosion
 58 resistance.

59 3 Linear Electric Machine Description

60 The stators of the linear electric machine are made of a magnetic circuit in M300-35A rectangular form, in
 61 laminated sheets equipped with the slots intended for three-phase winding aluminum bars. The magnetic circuit
 62 is laminated in stacked plates cut to their thickness. The number of stacked plates is proportional to the width
 63 of the magnetic circuit. The plate is punch-cut in a single operation from a strip of sheet metal, first insulated
 64 on both sides by a phenolic class H varnish. The plate hole profile has a circle shaped that will help stack plates
 65 for the appropriate height of the magnetic circuit to be dipped in the oven.

66 The side of the plate bore has 36 slots intended to receive the winding bars after stacking [5].

67 The winding is three-phase-series bar star. Each bar is a rectangular aluminum section to ensure transverse
 68 field compensation of Roëbel slot process. Bar winding has several advantages over traditional winding: good
 69 slot filling factor (greater than 95%); minimization of solid insulation and the potential difference between bars;
 70 better performance; and good thermal behavior in the slot.

71 Linear electric machine is protected by an aluminum cover called enclosure against ingress of moisture, dust,
 72 atmospheric impurities and any foreign materials.

73 The moving plate consists of a permanent magnets made of NdFeB (alternating North-South), which are
 74 magnetized in the transversal direction. The magnets are glued to a brass frame. The friction sheet is made of
 75 bronze 0.1 mm thick to ensure strength and mechanical rigidity. Anaerobic glue (polymerized in the absence of
 76 air) of acrylic type is used. The linear electric motor is a parallelepipedic structure with two air gaps (Fig. 4).

77 4 Centering and Plating Forces

78 The main problem encountered in the design of air gap structure is in the control of the mechanical clearances
 79 necessary to allow the permanent movement of the moving plate [6], [7], [8]. This problem is very difficult to
 80 control due to the magnetic gap which must be as small as possible to avoid penalizing the tangential magnetic
 81 pressure. The moving plate is thin in the multi-air gap structure and therefore not very rigid. Moving plates
 82 made of magnets, therefore, tend to rub against the fixed stators. It is necessary to control the forces that are
 83 perpendicular to the active surfaces. In Linear machines have been and continue to be designed considering a
 84 large variety of topologies. Linear machines are flat or tubular. They have a long stator: the mover is shorter
 85 than the stator or a short stator: the mover is longer than the stator. The stator slots are of single layer type or
 86 double layer one. Beyond energy efficiency, linear machine concepts exhibit: high velocity, high acceleration, high
 87 accuracy of the position sensing and high lifetime with less maintenance [4]. linear electrical machines with
 88 a parallelepipedic multi-air gap structure, figure ??, we have: $e_1 + e_2 = e$; $e_1 = e - e_y$; $e_2 = e + e_y$; e
 89 theoretical mechanical air gap; e_1 upper air gap; e_2 lower air gap and e_y offset; F_1 attraction force created by
 90 stator 1; F_2 attraction force created by stator 2; F the sum of the forces applied to the moving plate. Each of
 91 the two stators exerts an attractive force on the moving plate (rotor). These two oppositely directed forces have
 92 a modulus which is related to the size of the air gap facing each other, as well as to the current flowing through
 93 the coils necessary for position control. Let us consider the equilibrium of the moving plate, i.e. the sum of the
 94 forces along the y-axis.

95 Under ideal conditions, normal forces are the same and counteract from side to side (the weight of the moving
 96 plate is neglected) (Figure ??a). Force F_1 should be of the same modulus as force F_2 , the equilibrium position
 97 of the moving plate being centered in the middle of the two stationary stators.

98 5 Fig. 5: Centring and decentring force

99 There is no perfect centering in practice. The air gap exists and a driving force is created giving rise to a normal
 100 force which will influence the performance of the linear electric machine. This asymmetrical position generates
 101 a force difference, applied perpendicularly to the movement, which tends to create friction between fixed and

102 moving plate (figure ??b). The balance must be restored $\sum F = 0$ ($F_1 + F_2 + F_3 = 0$). The
 103 moving plate must move towards the stator opposite the direction of application of force F in order to restore
 104 the balance. This is because the smaller the air gap, the higher the attractive force. By decreasing the air gap
 105 on one side and thus increasing it on the other, the equilibrium of forces is achieved within a certain limit. This
 106 limit is conditioned by the size of the air gap as well as the normal stiffness constant. The magnetic balance of
 107 the moving plate is very unstable. The phenomenon described above has caused many failures in the design of
 108 linear electrical machines with a multi-air gap structure with guided or friction plates. Operation is affected by
 109 high wear of the friction interfaces (friction).

110 In order to fully understand how magnetic solutions work; they must be compared to a mechanical system.
 111 When the stiffness constant is positive, it is assimilated to a spring which will oppose the displacement. Conversely,
 112 when the stiffness constant is negative, the solution favors deviation from the original position.

113 IV.

114 6 Calculation of Normal Force

115 The air gap is very important in the electromagnetic parameterization of a linear electric machine with a multi-air
 116 gap structure with guided or friction plates. This normal force which depends on the air gap is strictly related
 117 to the mutual position of all permanent magnets and stators [9], [10].

118 7 a) Analytical calculation of force

119 As the magnetic circuit changes its shape during operation (displacement of the moving plate), the force is
 120 calculated analytically using the virtual working principle and Maxwell's tensor methods. Here we use the
 121 principle of virtual work.

122 Faraday's Law of Induction presents the voltage induced in the winding, which creates a current that tends to
 123 resist flux changes. The voltage equation for the winding is written as follows: The transformed energy is given
 124 by the equation: $W = \int u i dt = \int i^2 R dt + \int i d\psi$ (3)

125 $\int i^2 R dt$ is energy transformed into heat and $\int i d\psi$ is reversible energy. The virtual displacement principle
 126 allows the driving force to be calculated analytically. The calculation is carried out at maximum displacement. F
 127 $= \frac{dW}{dx} = i \frac{d\psi}{dx}$ (4)

128 x is the displacement of the mobile (m); W : the magnetic energy (J); B : magnetic induction (T); H : magnetic
 129 field (A/m) and V : volume (m^3).

130 8 b) Calculation by the finite element method

131 The finite element method uses the same principle; it is applied over the pattern of the linear electric machine.
 132 The table below gives all the dimensions of the prototype. The suspension consists of NdFeB (neodymium-iron-
 133 boron) permanent magnets and the two stationary stators are made of metal sheet grade M300-35A, where on
 134 the side of stator 1 there is an air gap of 0.2 mm, on the side of stator 2 there is an air gap of 0.4 mm (figure ??).

135 Fig. ??: Cross-section of the linear machine From Figure ??, we can estimate that linearity is important
 136 enough to consider normal stiffness to be constant. We can deduce the following characteristics:

137 The normal stiffness (N/m) is equal to the variation of the normal stress on the variation of the air gap.

138 The current stiffness (N/A/mm²) is equal to the variation of the total force on the variation of the current
 139 density.

140 These calculated parameters are used to dimension the analytical model.

141 The simple model established around an operating point makes it possible to control the suspension, in
 142 Laplace's formalism, by placing oneself around any point to be enslaved.

143 The mechanics allows us to link the normal force $F_N(p)$ with the acceleration $\ddot{y}(p)$ and the mass of the
 144 moving plate (M). $F_N(p) = M \ddot{y}(p)$ (5)

145 By integrating the acceleration, we obtain the velocity $\dot{y}(p)$, and by integrating again, the position $y(p)$.

146 The normal force is proportional to the square of the induction (B^2), thus the square of the flux (ψ^2). F_N
 147 $= B^2 \frac{d\psi^2}{dx} = 2\psi \frac{dB}{dx} \psi$ (7)

148 V.

149 9 Control/Command Mode a) Spring compensation

150 The principle is to take up exactly the force of attraction between the moving plate and the two stationary
 151 stators by means of an adjustable spreading force between the two stationary stators, see figure 4. Adjusting the
 152 gap between the two stators to cancel friction. Flatness is obtained from the dial gauge by manipulating the
 153 eight screws of the guide device.

154 10 b) Compensation by coupling tangential and normal forces

155 The coupling of forces to compensate for frictional forces is a path to be explored. The variation in spring stiffness
 156 creates a damping effect to compensate for friction forces. The principle consists in modifying the spring stiffness

157 during the operation of the linear parallelepipedic electric machine (displacement of the moving plate) in order
 158 to compensate the friction forces.

159 ? In the centered position (moving plate), the sound pressure at the output of the sound line delivers a sound
 160 power to the moving plate. It moves with a speed V .

161 ? $0 < t < t_d$, the compensating force created by the springs provides a reaction force to keep the moving plate
 162 centred during operation of the linear parallelepipedic electric machine, where t_d is the time taken to cover the
 163 half stroke.

164 The coupling between two forces to transfer energy to a servo force, allows the recovery of vibration energy
 165 from the moving plate, as shown in figure ??.

166 **11 Fig. 9: Coupling of tangential and normal forces**

167 At the level of the correctors, the normal force (in y) can be controlled by a conventional corrector. The addition
 168 of another proportional corrector will allow to control the current according to the following displacement x .

169 ? Modeling of the tangential force (in x).

170 The centered position is changed by the control current when a disturbance occurs. The reaction force is
 171 obtained by multiplying the compensation force in x by the following displacement x .

172 ? Modeling of the normal force (in y).

173 We add a link between the tangential and normal forces. The link constant is calculated by the finite element
 174 method. The reaction force is obtained by multiplying the compensation force in y by the following displacement
 175 y . The model of the normal force is identical to that of the tangential force: the force (in y) and the position (in
 176 y) are governed by the same equation.

177 **12 VI.**

178 **13 Conclusion**

179 This paper focused on the magnetic suspension systems and the control systems using permanent magnets. The
 180 determination of the normal stress, stiffness's as a function of the mechanical air gap and current density was
 181 done by the finite element method using the ANSYS MAXWELL software. The air gap is quite small and very
 182 important in the electromagnetic parameterization of a linear parallelepipedic electric machine with guided or
 183 friction moving parts. The normal force depends on the air gap and is strictly related to the mutual position of
 all permanent magnets and stators. ¹

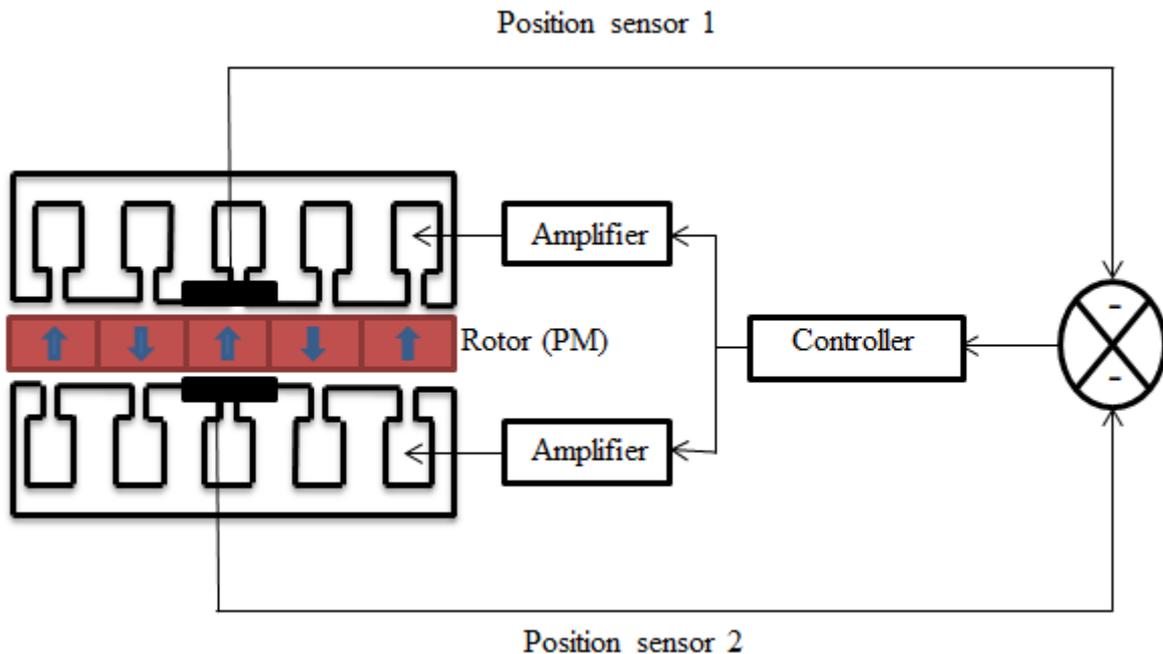


Figure 1: Fig. 2 :

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3

Figure 2: Fig. 3 :

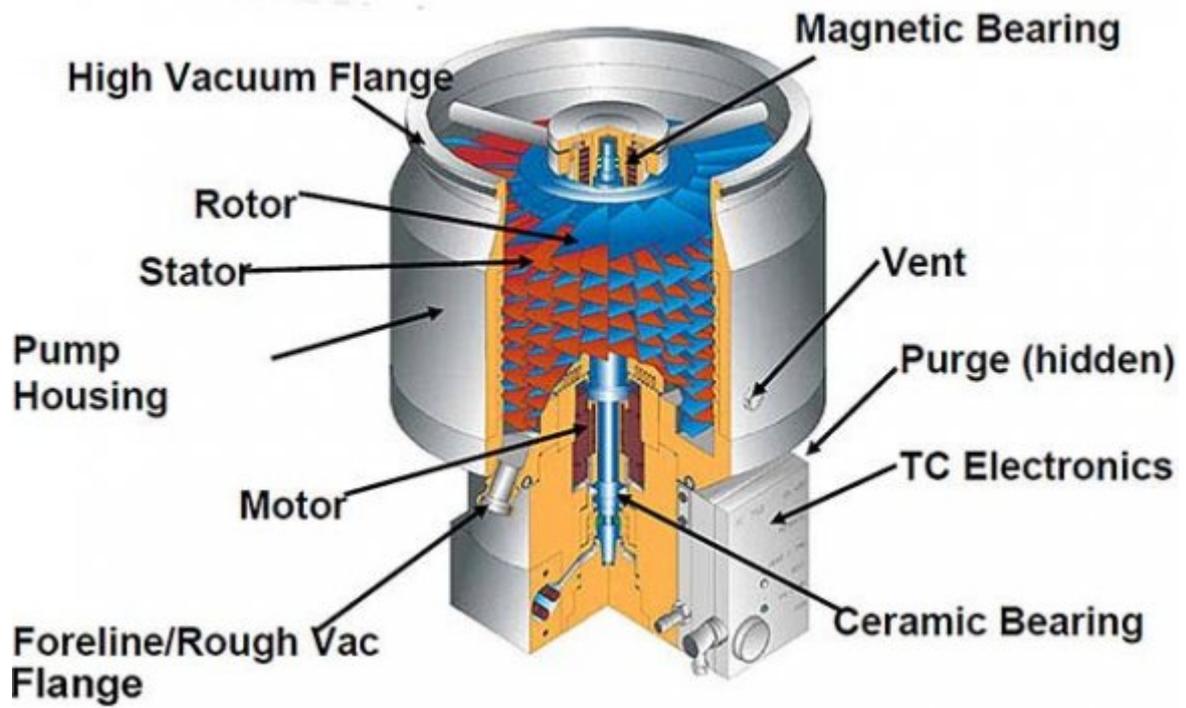


Figure 3: Linear

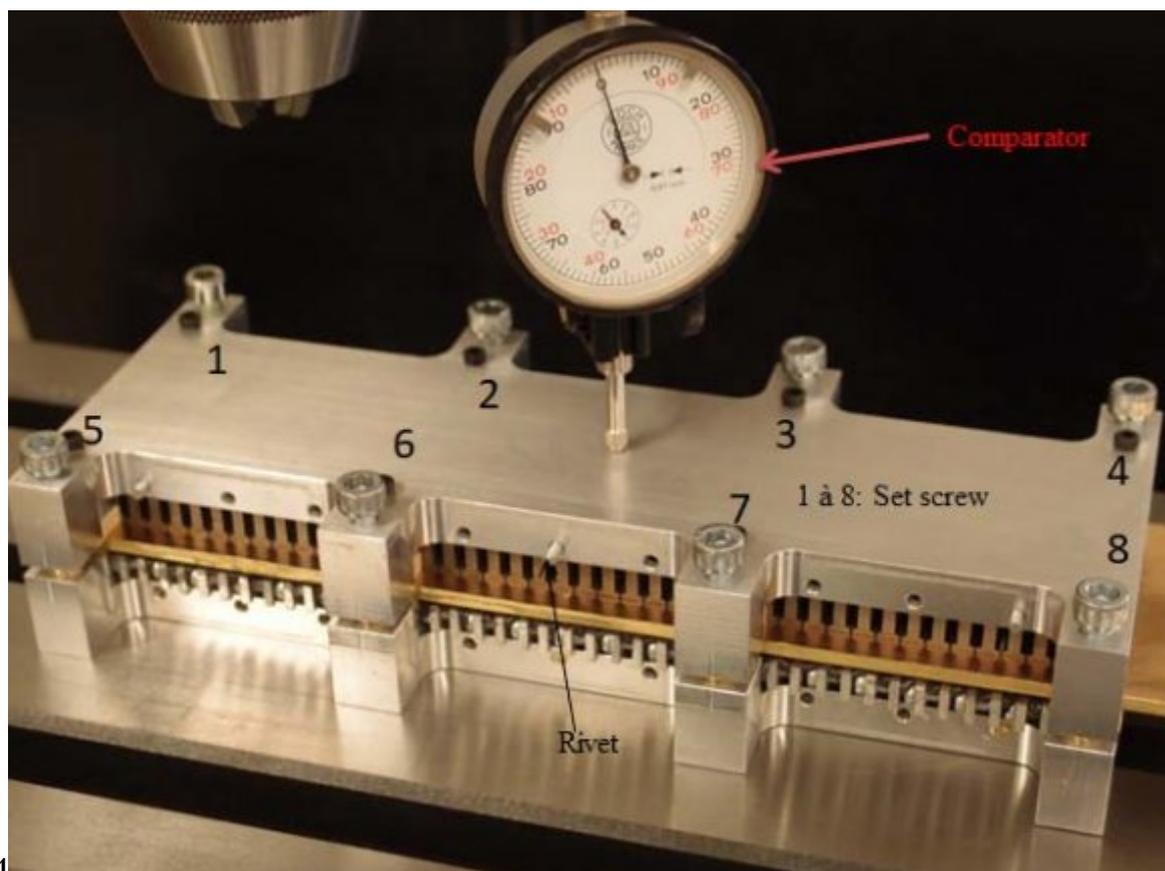


Figure 4: Fig. 4 :

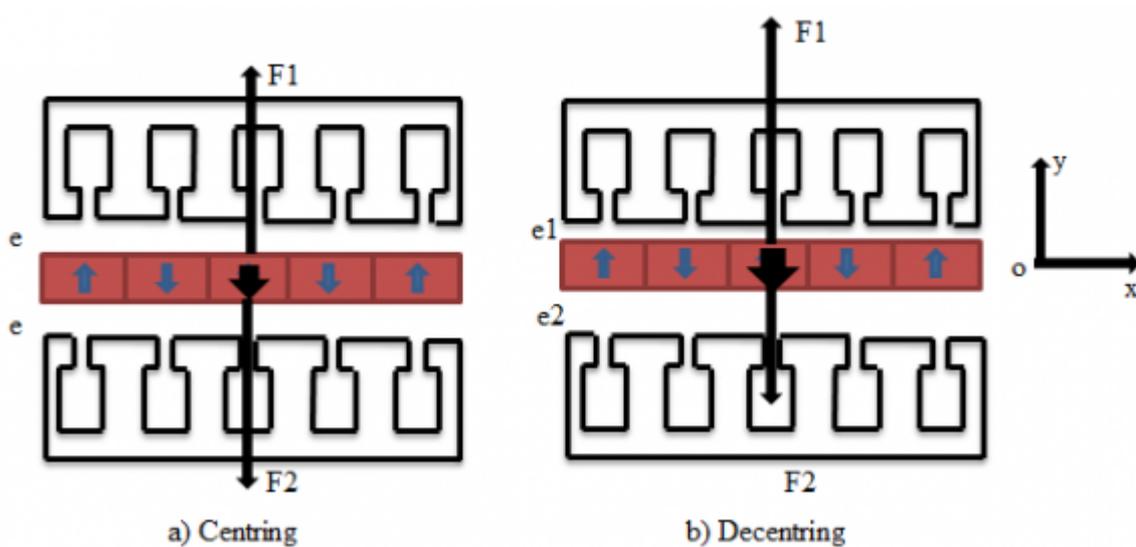


Figure 5:

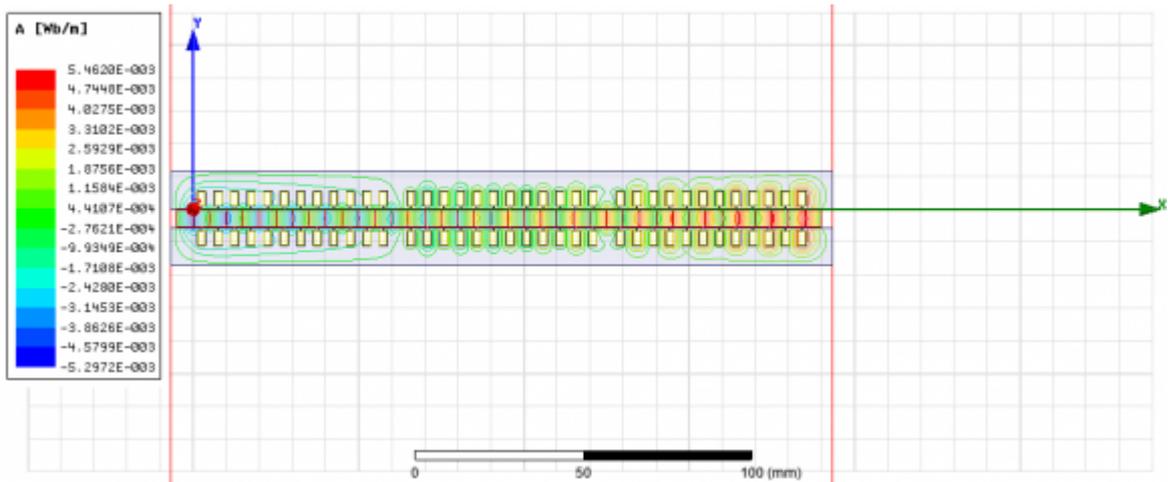
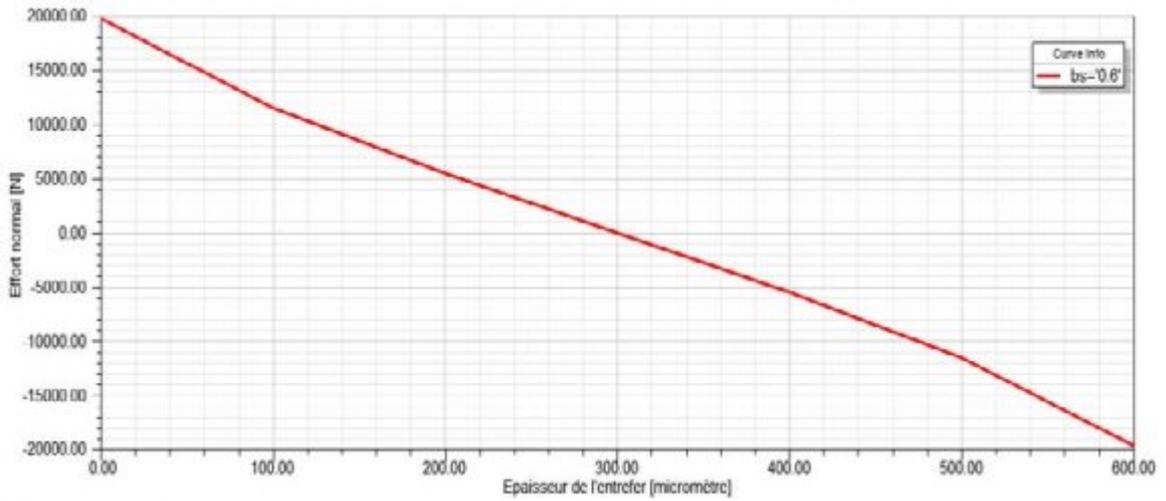
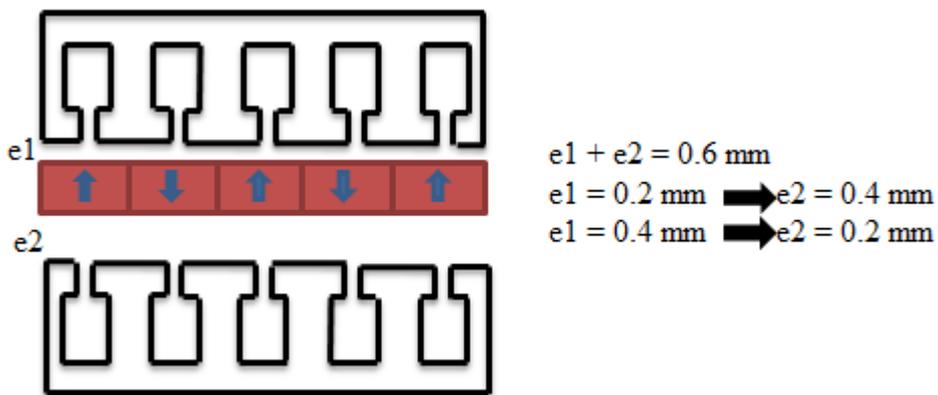


Figure 6:



16

Figure 7: Table 1 :Figure 6



67

Figure 8: Fig. 6 :Fig. 7 :

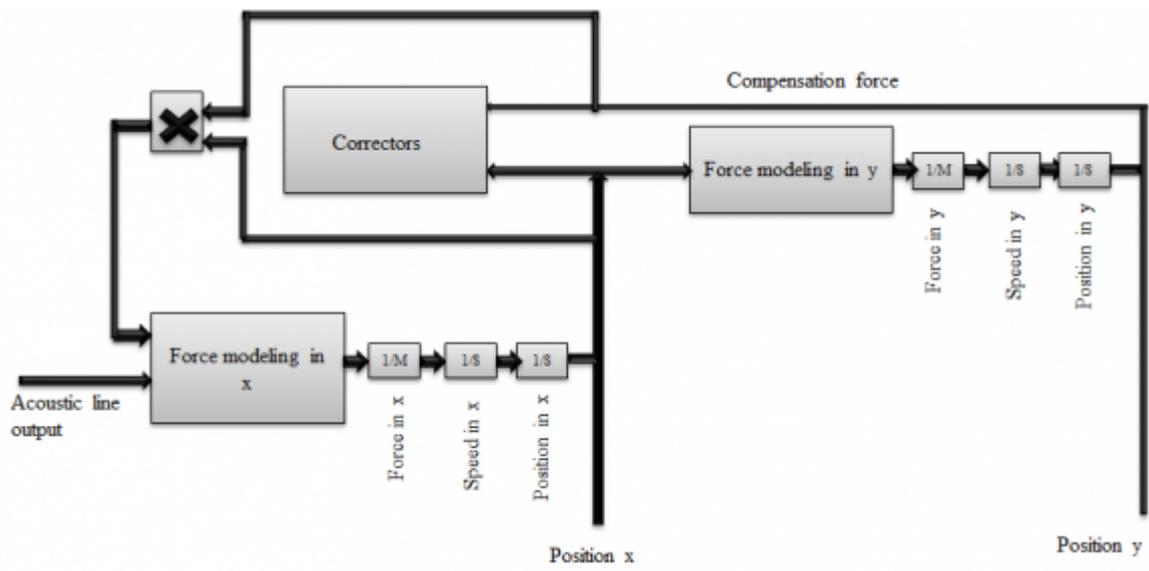


Figure 9: Linear

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