

1 Machinability of Nickel Chromium Case Hardened Steel (EN36C)

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6 **Abstract**

7 Nickel Chromium Case Hardened Steel (EN36C) is surface hardened low carbon steel provided
8 with a strong core prepared by the thermo-mechanical process. Owing to high strength,
9 corrosion resistance, shock resistance, and good fracture toughness properties this kind of steel
10 is used. Heavy duty crane shafts, airplane gears, cam, rollers, truck construction, some
11 structural members and other more are the applications of this steel. It is compatible with
12 dynamic conditions where the load is fluctuating with time, but the rigorous amount of
13 temperature develops due to friction. The paper presents the experimental study on
14 machinability of the EN36C steel. Experimentation was carried out by Chemical vapor
15 deposition (CVD) coated carbide tool. Speed, feed and depth of cuts are the input parameters
16 and chip reduction coefficient, material removal rate (MRR) and Von Mises stress are the
17 output responses. The input parameters were assigned with code and arranged in 33 factorial
18 design forms according to the Design of Experiment (DOE).

19

20 *Index terms*— machinability; chip thickness; strain hardening; von mises stress.21 **1 Introduction**

22 Steel has a vital role in the manufacturing industries. As per manufacturing is concerned, the material should be
23 deformable but so far as functioning is related material must not deform during its application. For designing
24 any mechanical component made out of steel, it is necessary to know about the working environment of the
25 component. For maintaining the required conditions, the steel needs to be alloying, and heat treated followed by
26 some other processes.

27 Case hardening of steel is used to improve the mechanical property of steel such as wear resistance without
28 affecting the inner core. The alloying elements take care the strength of the inner core and the thermomechanical
29 processes hardens the outer surface. There are many methods by which case hardening can be achieved; some
30 among them are surface coatings, diffusion methods, carburising methods, applied energy methods, etc. Energy
31 applied method which includes flame hardening, induction heating, laser surface heat treatment, and laser
32 transformation hardening is the case hardening process used for EN36C steel.

33 The work presented aimed at experimental investigation of the Von Mises stresses generated during dry turning
34 of EN36C steel. The work focuses on the chip formation process which was the result of the input process
35 parameters applied during machining. Chip formation and its thickness showed the extent of the rigorous plastic
36 deformation of the material. The plastic deformation of material causes the generation of the Von Mises stress
37 during machining. The generated Von Mises stress lies in the flow zone during the process of chip formation.
38 There are many experimental ways to determine the stresses generated in the material during machining which
39 requires some extra setup such as dynamometer installation, the force measuring sensors and many more which
40 makes the whole machining process complex. Considering the material properties such as Strength coefficient 'K'
41 and strain hardening exponent 'n' and the chip reduction coefficient '?' evaluation of Von Mises stress has been
42 carried. The chips formed during machining of EN36C steel are sometimes twisted and curl with an irregular
43 surface which creates a problem of direct measurement of its length and width. Therefore we considered the length
44 and weight of a chip to evaluate the cut chip thickness. The weight of the chip takes care of the inaccuracies

45 occurred for the determination of the cut chip thickness. Chips are further subjected to SEM examination and
46 analysis continues.

47 2 II.

48 3 Literature Review

49 Kaushal Pratap Singh et al. [1] used Taguchi optimization technique to optimize input process parameters so
50 to improve surface finish and material removal rate (MRR) during turning operation of EN36 steel. In the
51 experiment, researchers adopted three levels (wet, dry, neutral) of the cutting environment with different spindle
52 speed, feed, depth of cut, and nose radius. After performing the experiment and analysis, researchers concluded
53 that cutting parameters effects MRR by 0.33%, 0.276%, 0.222%, 0.503% and 0.840% respectively and surface
54 roughness by 0.105%, 0.412%, 0.261%, 0.703% and 0.447% respectively.

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57 6 I Version I

58 Manan Kulshreshtha [2] studied the effect of machining parameters over the surface roughness of EN36 steel
59 shafts by the use of carbide and cobaltbased tool insert using CNC lathe. Types of tool insert used, spindle
60 speed, feed rate and depth of cut are the input process parameters used. The sequence of the input parameters
61 was generated and considered according to Central Composite Design (CCD). As a result of the experiment, feed
62 rate contributes most and cutting speed contributes least as an input factor affecting the surface roughness. By
63 the use of Tungsten carbide tool, 2.1 micron was the optimum surface roughness value recorded at 0.2mm DOC,
64 10mm/min feed rate and 1200 rpm cutting speed.

65 However, by machining with cobalt insert, it was observed that 2.3 micron was the optimum surface roughness
66 value recorded at 0.2mm DOC, 15mm/min feed rate and 1200rpm cutting speed.

67 A.Venkata Vishnu et al. [3] used Taguchi approach to optimize the turning process parameters of EN36 alloy.
68 By using a Taguchi robust design approach, the optimum value of the selected control parameters was found
69 to improve the material removal rate. EN36 steel in annealed condition was the work material, CNC machine
70 with three types of tool inserts (Uncoated, PVD coated (TiAlN), CVD coated (CVD Al The result obtained
71 that MRR increases with increase in cutting speed and feed rate respectively and also MRR increases till the
72 moderate depth of cut and then decreases on increasing the depth of cut and at last MRR was maximum for the
73 Uncoated tooltip, moderate for CVD tool and minimum for PVD coated tool.

74 They concluded that 100m/min cutting speed, 0.4mm/rev feed, 1 mm depth of cut were the optimum values
75 and the uncoated tool was good for MRR.

76 7 III.

77 8 Experimental Analysis

78 For the assessment on machinability of EN36C steel, Von Mises stress and the chip formation mechanism are two
79 primary factors considered. The work material is of 110 mm diameter and 400 mm length dimension. The work
80 material is Nickel Chromium case hardened steel prepared by the thermo-mechanical process. For turning of the
81 work material, the present work employed Tungaloy made CVD (Chemical Vapour Deposition) coated (3 to 16
82 μm thick) carbide grades consisting of cemented carbide substrate TiCN tool insert. The coating over the tool
83 insert improves the hot hardness and oxidation resistance property of the tool, thus making the tool chemically
84 stable which increases the tool life and efficiency of machining.

85 9 b) Selection of process parameters

86 The input process parameters were selected based on the values available on the lathe. After mounting the work
87 material on the lathe, turning operation was carried out for 30 seconds for each experiment. The experiment
88 performed results in the formation of 27 different types of chips.

89 10 TrueStress Vs TrueStrain

90 From the true stress-true strain curve points were selected which lies between the yield stress point and the
91 ultimate stress point. Strain hardening exponent 'n' and strength coefficient 'k' values are available in the present
92 work obtained from plotting the points of true stress-true strain curve on log-log graph paper and extrapolating
93 the line to strain value 1. Value of 'K' is the value of true stress at true strain equals to 1 on the loglog graph
94 (Fig. ??). b CRC = $1.3334 - 0.0561x_1 - 0.0322x_2 - 0.0163x_3 - 0.2708x_1^2 + 0.1474x_2^2 + 0.0563x_3^2 + 0.0366x_1x_2 + 0.0183x_1x_3 - 0.0093x_2x_3$ (eq. i)

95 b VMS = $1810.7 - 76.2x_1 - 25.1x_2 - 7x_3 - 324x_1^2 + 265.7x_2^2 + 157.9x_3^2 + 101.5x_1x_2 + 129.5x_1x_3 - 374x_2x_3$ (eq. ii)

98 Where, $x_1 = \text{Speed}$.

99 $x_2 = \text{Feed}$.

100 $x_3 = \text{Depth of cut}$. engineering lab of NIT Silchar, SEM lab and material testing lab of IIT Kanpur to
conduct different experiments related to this project and to all other people who helped in success of this work.



Figure 1:

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102

1 2

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Figure 2:



Figure 3: Fig. 1 :

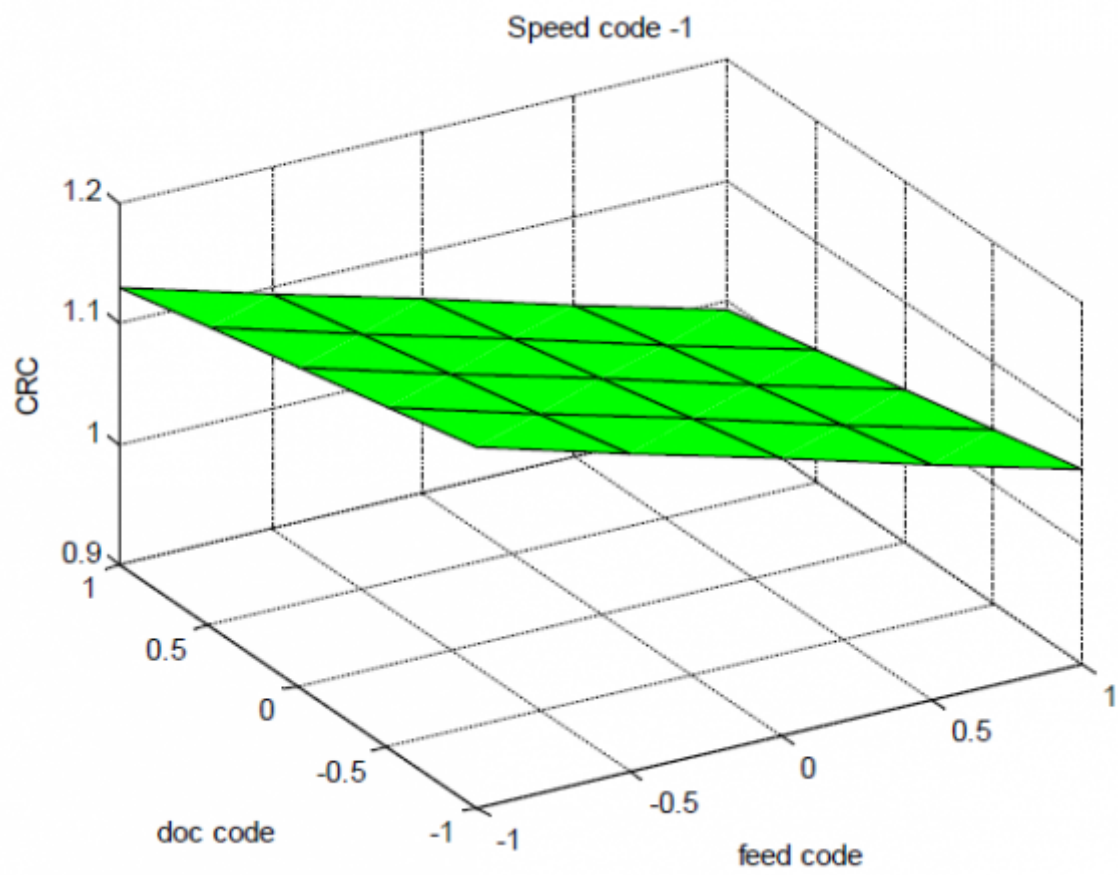


Figure 4: Fig. 2 (

2

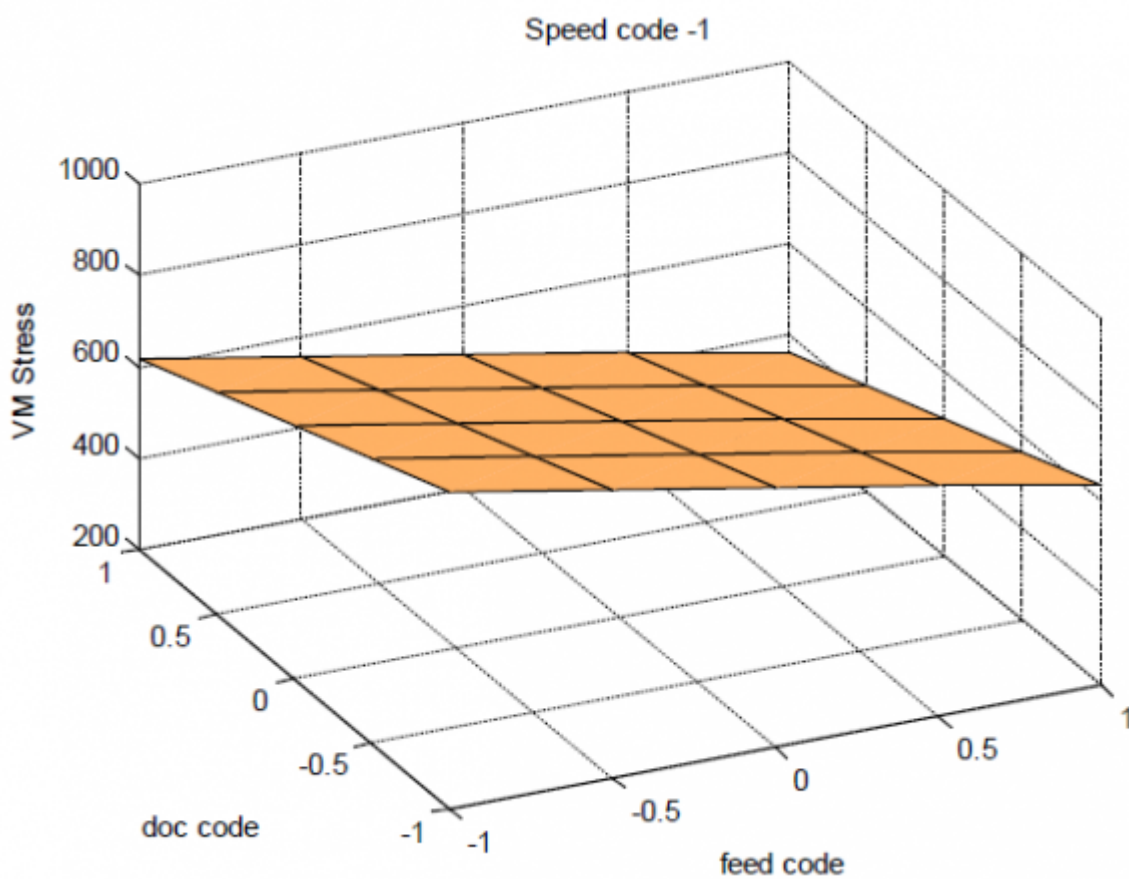
| |
|---------------------------------|
| $\sigma = 1495\epsilon^{0.178}$ |
|---------------------------------|

Figure 5: Fig. 2 (



3

Figure 6: Fig. 3 :



41

Figure 7: Fig. 4 : 1 Total

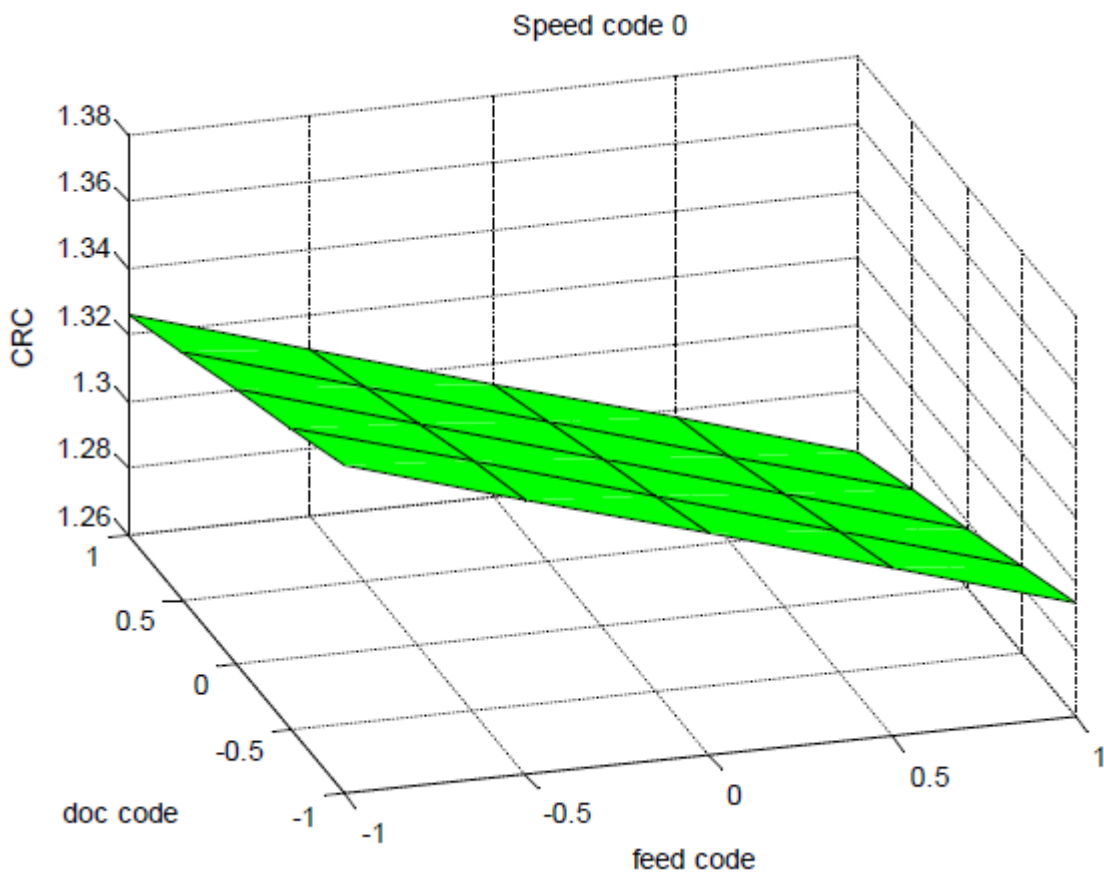
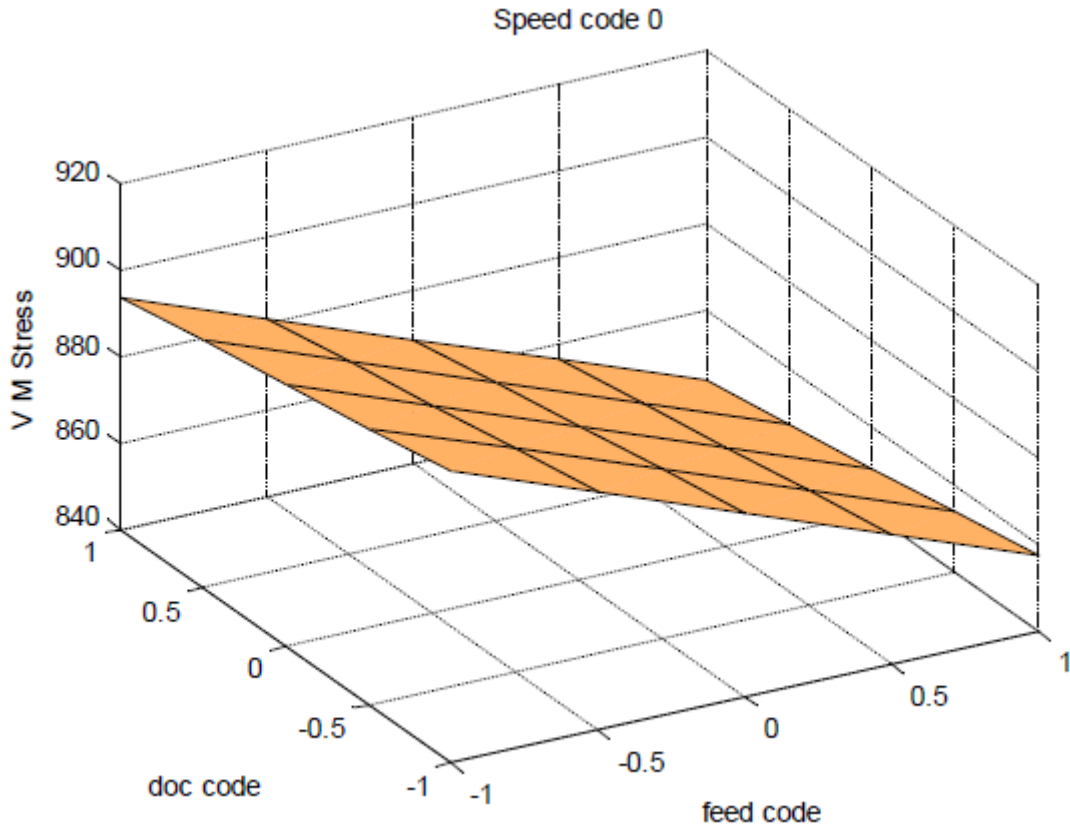
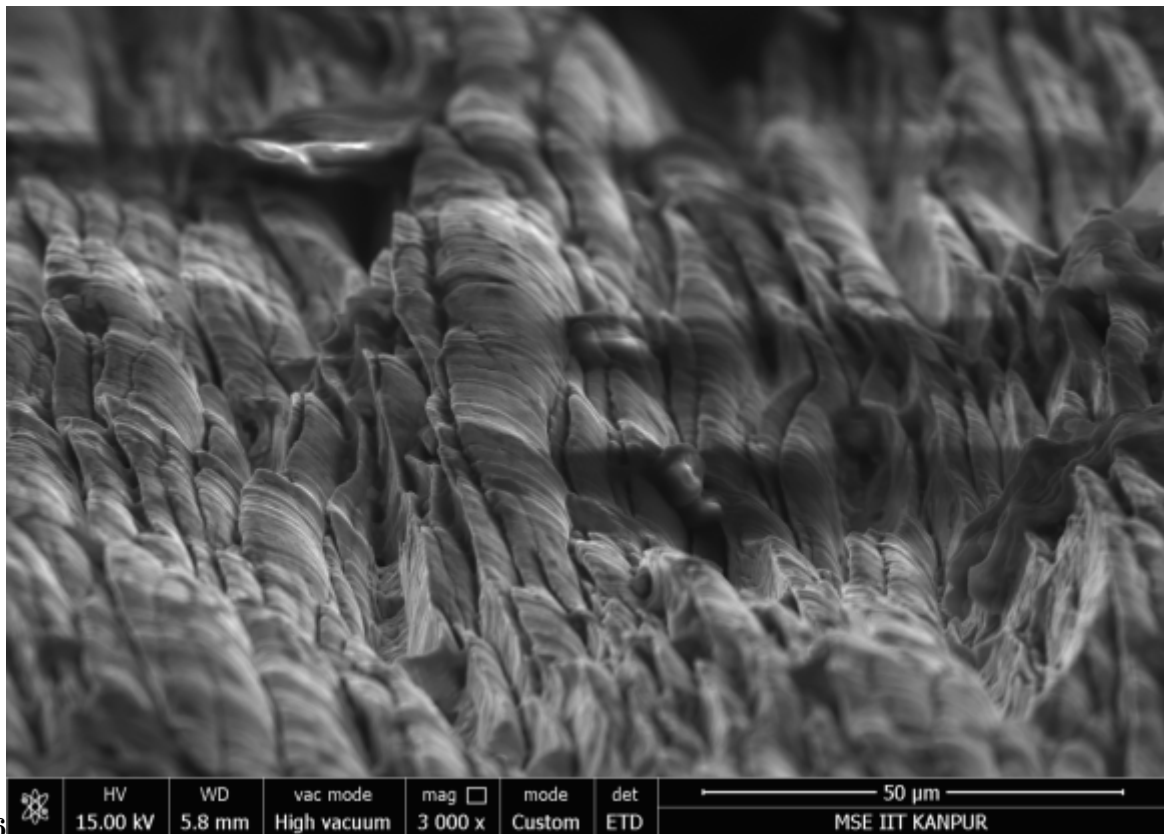


Figure 8:



5

Figure 9: Fig. 5 :



6

Figure 10: Fig. 6 :

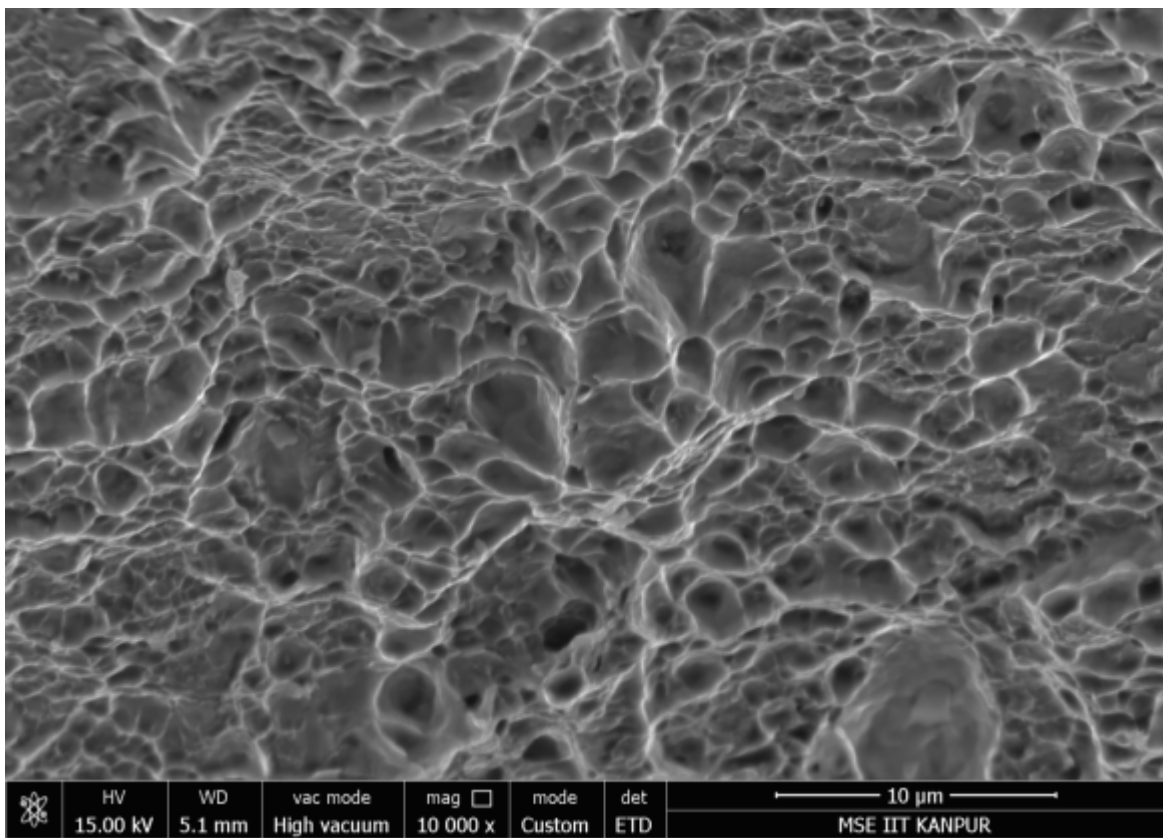
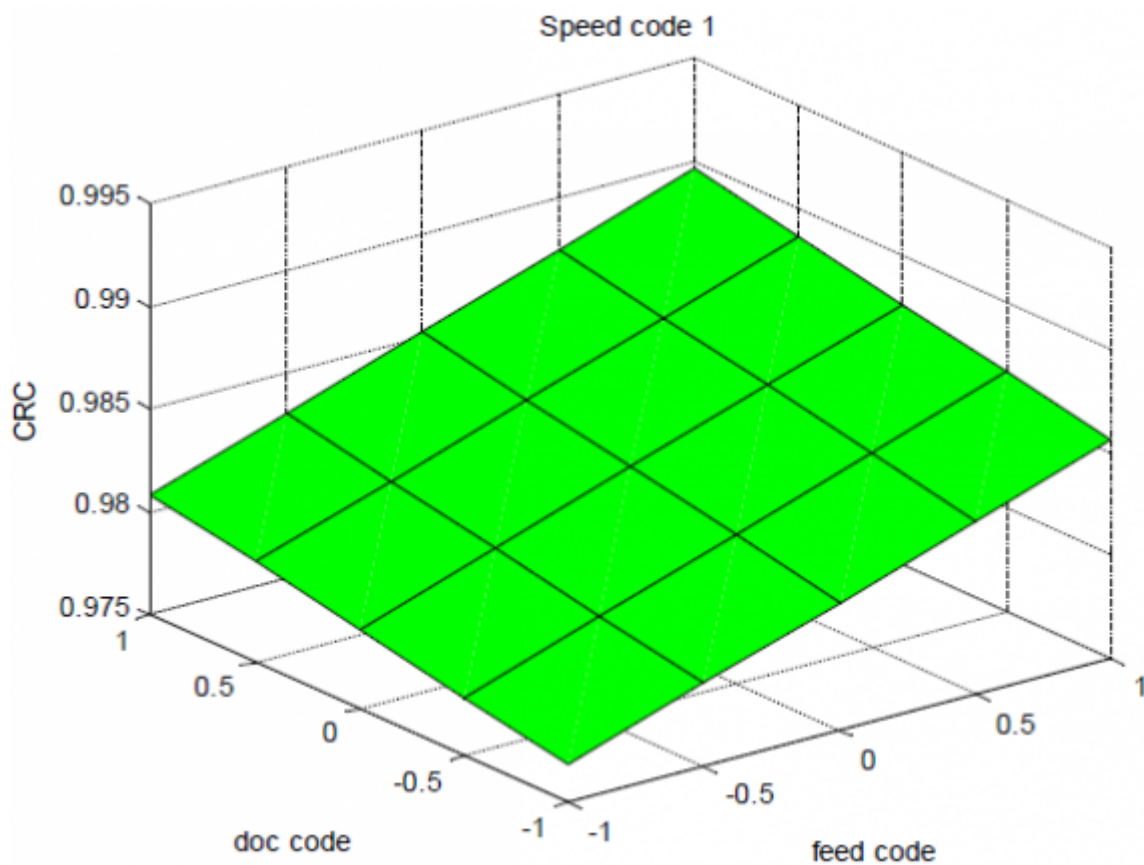
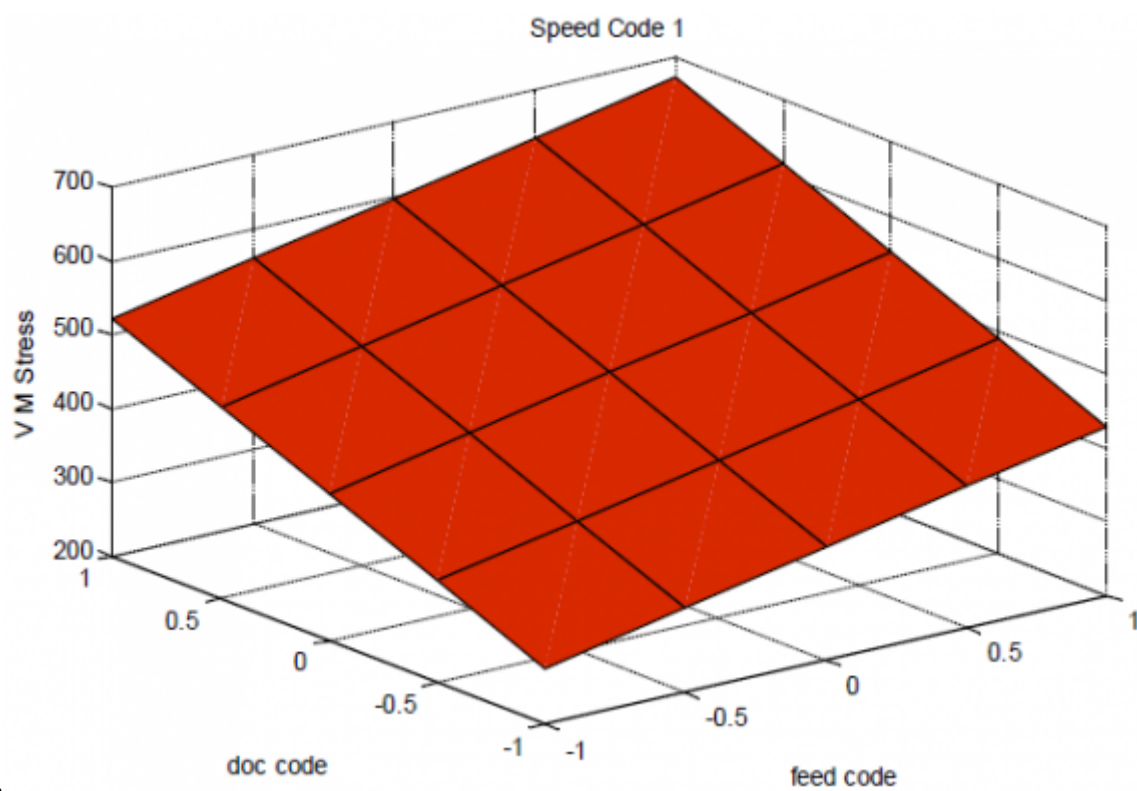


Figure 11:



7

Figure 12: Fig. 7 :



8

Figure 13: Fig. 8 :

1

%Fe

Balanced

The present work employed gear driven central lathe for turning the workpiece. Spindle speed range of 45 rpm to 1000 rpm, and feed a range of 0.06mm/rev to 1.72 mm/rev are values available in the central lathe.

%C %Mn%Si %P %Cr %Mo%Ni %Al %S
0.150.3860.1820.0160.8200.1313.10 0.0180.0199

Figure 14: Table 1 :

2

| Factors | Level 1 | Level 2 | Level 3 |
|---------------|---------|---------|---------|
| Coding | -1 | 0 | 1 |
| Speed (m/min) | 36 | 60 | 100 |
| Feed (mm/rev) | 0.49 | 0.63 | 0.86 |
| DOC (mm) | 0.67 | 1 | 1.5 |

Figure 15: Table 2 :

3

| S. No. | Velocity Code | Feed Code | DOC Code | V (m/min.) | f (mm/rev) | d (mm) |
|--------|---------------|-----------|----------|------------|------------|--------|
|--------|---------------|-----------|----------|------------|------------|--------|

Figure 16: Table 3 :

103 .1 Acknowledgement

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