

New Formulas for the Mutual Inductance and the Magnetic Force of the System: Thin Disk Coil (Pancake) with Inverse Radial Current Density and Thin Wall Solenoid with Constant Azimuthal Current Density

Cevdet Akyel

Received: 13 December 2017 Accepted: 31 December 2017 Published: 15 January 2018

Abstract

This paper deals with two coaxial circular coils (thin disk coil and thin wall solenoid) for which we calculated the electromagnetic quantities such as the mutual inductance and the magnetic force. The disk coil (pancake) is with the nonlinear inverse radial current and the wall solenoid with the constant current in the azimuthal direction. The circular coils with the nonlinear inverse radial current are well known as the Bitter coils, and the circular coils with the azimuthal current are well known as the ordinary coils. Also, the coils with the azimuthal current can serve as the superconducting coils. These calculations give the semi-analytical and the analytical expressions respectively for these electromagnetic quantities. Also, we presented the improved filament method as the comparative method.

Index terms—

1 I. Introduction

The computation of the electromagnetic quantities (magnetic field, self-inductance, mutual inductance, magnetic force, etc.) for the conventional circular coaxial coils with the constant azimuthal current density has been presented in many papers, books, monographs and studies [1][2][3][4][5][6][7][8][9][10][11][12][13][14][15][16][17][18][19]. The analytical, the semi-analytical and the numerical methods have been used to calculate these electromagnetic quantities. These calculations are used in many electromagnetic applications (tubular linear motors, magnetically controllable devices and sensors, current reactors, cochlear implants, defibrillators, instrumented orthopedic implants, in magnetic resonance imaging (MRI) systems, superconducting coils, and tokamaks, etc.).

Also, there are the nonconventional circular coils with the nonlinear inverse radial density current which are used in many technical applications such as the superconducting coils, the electromagnets for the the superconducting coils, the electromagnets for the production of the extremely powerful magnetic fields (Bitter coils) and the homopolar motors [20][21][22][23][24][25][26][27][28][29][30][31][32][33][34][35][36]. The calculation of the magnetic force and the mutual inductance for these coils is essential for the design of electromagnetic inductors. In this paper, we calculated these electromagnetic quantities for the coil's combination, the disk coil (pancake) with the nonlinear inverse radial current density (Bitter disk coil) and the wall solenoid with the constant azimuthal current density (superconducting wall solenoid). All expressions are obtained in the semi-analytical form (mutual inductance) and the closed form (magnetic force). Also, all singular case has been solved and given in the closed form. The results of these calculations are expressed over the elliptic integrals of the first kind and the Heuman's Lambda function and one simple friendly integral whose kernel function is the continuous function in all interval of the integration. We used the Gaussian numerical integration, [37][38]. The improved modified filament method for the presented configuration is given as the comparative method. We use the Matlab implementation to calculate the mutual inductance and the magnetic force by two independent methods.

2 II. Basic Expressions

The Bitter disk coil and the wall solenoid in the air are with the inverse radial current density and the uniform current density respectively [29][30], (See Fig. 1) as follow:

Figure 1: Bitter disk coil and thin solenoid the mutual inductance and magnetic force between these coils, are respectively $M = \frac{\mu_0}{4\pi} \int \int \frac{J_1 \cdot J_2}{r^3} dV_1 dV_2$ and $F = \int \int \frac{\mu_0}{4\pi} \frac{J_1 \cdot J_2}{r^3} dV_1 dV_2$ where $r = \sqrt{z^2 + \rho^2}$

Both configurations are in the air or a nonmagnetic and non-conducting environment. We obtain the integral form to calculate these two physical quantities.

3 III. Calculation Method

After four analytical integration M and F are respectively:

where, $M = \frac{\mu_0}{4\pi} \int \int \frac{J_1 \cdot J_2}{r^3} dV_1 dV_2$ and $F = \int \int \frac{\mu_0}{4\pi} \frac{J_1 \cdot J_2}{r^3} dV_1 dV_2$ where $r = \sqrt{z^2 + \rho^2}$

From general cases (6) and (7) it is possible to obtain the special and singular cases. The expression M is in a semi-analytical form where we need to solve the simple integral I on numerically by using the Gaussian integration for example. The expression S is in the closed form.

4 Singular Cases

Singular cases are in the analytical form (6) and (7) respectively: If $b = 0$ and $k = 1$ or $b = 0$ and $k = 0$. If $b = 0$ and $k = 1$ then $M = \frac{\mu_0}{4\pi} \int \int \frac{J_1 \cdot J_2}{r^3} dV_1 dV_2$

5 4

(1) If $b = 0$ and $k = 1$. All expressions in (6), (7), (8) and (9) are the complete elliptical integrals K, E and Π , Heuman's Lambda function [37][38]. $M = \frac{\mu_0}{4\pi} \int \int \frac{J_1 \cdot J_2}{r^3} dV_1 dV_2$

IV. Modified Filament Method

In this paper, we give the modified formulas for the mutual inductance and the magnetic force between two Bitter thick coils (See Fig. 2) using the filament method. Applying some modification in the mutual inductance calculation [30], we deduced the mutual inductance and the magnetic force between the Bitter disk and the wall solenoid as follows:

6 Examples

To validate the new approach we present some examples, which cover either the regular or the singular cases. In these examples, all coils are with the unit currents. Also, we define the coil dimensions. For the comparative filament method, the number of subdivisions for each coil is also given. Our goal is to verify the accuracy of this method, so that we will fix the number of subdivisions ($K = N = 3000$) in the following examples without taking into consideration the computational time in the calculations. The number of turn in each coil is 100. (6) and (7) we obtain: $M = 17.661179\text{mH}$ $F = 7.4710846\text{mN}$ From (10) and (11) we obtain: (6) and (7) we obtain: $M = 26.158014\text{mH}$ $F = 0\text{N}$ From (10) and (11) we obtain: a) Example1. Wall solenoid: $R = 2\text{m}$, $z_1 = 0\text{m}$, $z_2 = 1\text{m}$. Disk coil: $R_2 = 3\text{m}$, $R_4 = 4\text{m}$, $z_Q = 2\text{m}$. From ($M = 17.661179\text{mH}$ $F = 7.4710845\text{mN}$ b) Example2. Wall solenoid: $R = 2\text{m}$, $z_1 = 0\text{m}$, $z_2 = 1\text{m}$. Disk coil: $R_2 = 3\text{m}$, $R_4 = 4\text{m}$, $z_Q = 0.5\text{m}$. From ($M = 26.158014\text{mH}$ $F = 0\text{N}$ c) Example3. Wall solenoid: $R = 3\text{m}$, $z_1 = 0\text{m}$, $z_2 = 1\text{m}$. Disk coil: $R_2 = 3\text{m}$, $R_4 = 4\text{m}$, $z_Q = 2\text{m}$.

101 From (??) and (6) we obtain: $M = 36.827754\text{mH}$ $F = 20.338671\text{mN}$ From (??0) and (??1 This case is the
 102 singular case. From (??) and (6) we obtain: $M = 67.6203121\text{mH}$ $F = 45.309445\text{mN}$ From (??0) and (??1
 103 This case is the singular case. From (??) and (6) we obtain: $M = 83.323296\text{mH}$ $F = 49.855888\text{mN}$ From (10)
 104 and (11) we obtain: $M = 83.323370\text{mH}$ $F = 49.855568\text{mN}$ g) Example7.

105 Wall solenoid: $R = 4$ m, m , $z_1 = 0$ m, $z_2 = 1$ m. Disk coil: $R_2 = 3$ m, $R_4 = 4\text{m}$, $z_Q = 0$ m. This case is
 106 the singular case. From (??) and (6) we obtain: $M = 83.323296\text{mH}$ $F = -49.855888$ NmN From (10) and (11)
 107 This case is the singular case. From (??) and (6) we obtain: $M = 91.598922\text{mH}$ $F = 54.254023\text{mN}$ From (10)
 108 and (11) we obtain: $M = F = 54.258225\text{mN}$ i) Example9. Wall solenoid: $R = 3$ m, m , $z_1 = 0$ m, $z_2 = 1$ m, N_1
 109 $= 100$. Disk coil: $R_2 = 3$ m, $R_4 = 5\text{m}$, $z_Q = 0.6$ m, $N_2 = 100$.

110 This case is the singular case. From (??) and (6) we obtain: $M = 65.436644\text{mH}$ $F = 5.7050033\text{mN}$ From (
 111 ??0) and (??1) we obtain: $M = 65.436923\text{mH}$ $F = 5.7050600$ mN

112 By previous examples, we confirmed that all calculated results by two different methods are in an excellent
 113 agreement. The bold digits are significant with the same accuracy in both calculations.

114 7 V. Conclusion

115 The new accurate expressions for calculating two electromagnetic quantities such as the mutual inductance and
 116 the magnetic force are presented in this work. All expressions are in the semi-analytical and the closed form.
 117 We give the improved filament method as the comparative method. Results obtained by two different methods
 118 agree at least in five significant figures. Nomenclature I 1 : Current imposed in the disk (pancake) in (m) I 2 :
 119 Current imposed in the superconducting solenoid in (m) N 1 : number of turns of the pancake N 2 : number of
 120 turns of the solenoid R 1 and R 2 : Inner and outer radius of the pancake in (m) R: The radius of the solenoid
 in (m) z Q : Axial position to the pancake in (m)



Figure 1: F



Figure 2: Figure 2 :

2
Year 2018
12
XVIII Issue IV Version I
Journal of Researches in Engineering () Volume F
Global

4 2 2 , 4 2 ,

Figure 3:

Year 2018
13
XVIII Issue IV Version I
Journal of Researches in Engineering () Volume F
Global

Figure 4:

- 122 [Furlani (1993)] ‘A formula for the levitation force between magnetic disks’. E P Furlani . *IEEE Transactions on*
123 *Magnetics* Nov. 1993. 29 (6) p. .
- 124 [Coulomb (1983)] ‘A methodology for the determination of global quantities from a finite element analysis and
125 its applications to the evaluation of magnetic forces, torques and stiffness’. J L Coulomb . *IEEE Trans. Mag*
126 November 1983. 19 (6) p. .
- 127 [Mc et al. (1988)] ‘A tunable volume integration formulation for force calculation in finite-element based
128 computational magneto statics’. S Mc , J Fee , D A Webb , Loather . *IEEE Trans. Mag* Jan. 1988. 24
129 (1) p. .
- 130 [Tarnhuvud and Reichert (1988)] ‘Accuracy problems of force and torque calculation in FE-systems’. T Tarnhu-
131 vud , K Reichert . *IEEE Trans. Mag* January 1988. 24 (1) p. .
- 132 [Babic et al. ()] ‘Analytical calculation of the 3D magnetostatic field of a toroidal conductor with rectangular
133 cross section’. S Babic , S Milojkovic , Z Andjelic , B Krstajic , J S Salon . *IEEE Trans. Mag* 1988. 24 (2) p. .
- 134 [Babic and Akyel ()] *Calculation of Some Electromagnetic Quantities for Circular Thick Coil of Rectangular*
135 *Cross Section and Pancake with Inverse Radial Currents*, S Babic , S Akyel , C . 2018. IET Electric Power
136 Applications
- 137 [Jackson ()] *Classical Electrodynamics (second Edition)*, J D Jackson . 1975. New York: John Wiley & Sons. p.
138 848.
- 139 [Ravaud et al. (2010)] ‘Cylindrical magnets and coils: fields, forces and inductances’. R Ravaud , G Lemarquand
140 , S Babic , V Lemarquand , C Akyel . *IEEE Trans Magn* Sept. 2010. 46 (9) p. .
- 141 [Dwight ()] *Electrical Coils and Conductors*, H B Dwight . 1945. New York: McGraw-Hill Book Company.
- 142 [Demenko and Stachowiak ()] ‘Electromagnetic torque calculation using magnetic network methods’. A Demenko
143 , D Stachowiak . *COMPEL* 2008. 27 (1) p. .
- 144 [Conway ()] *Exact solutions for the magnetic fields of ax symmetric solenoids and current distributions*, J T
145 Conway . 2001. 37 p. .
- 146 [F New Formulas for the Mutual Inductance and the Magnetic Force of the System: Thin Disk Coil (Pancake) with Inverse Radia
147 ‘F New Formulas for the Mutual Inductance and the Magnetic Force of the System: Thin Disk Coil (Pancake)
148 with Inverse Radial Current Density and Thin Wall Solenoid with Constant Azimuthal Current Density and
149 electric force and torque computation’. *IEEE Trans. Mag* Sept., 1984. 20 (5) p. .
- 150 [Coulomb and Meunier ()] *Finite element implementation of virtual work principle for magnetic*, J L Coulomb ,
151 G Meunier . 2018.
- 152 [Snow (1954)] *Formulas for Computing Capacitance and Inductance*, C Snow . December 1954. 544. National
153 Bureau of Standards Circular Washington DC
- 154 [Furlani (1993)] ‘Formulas for the force and torque of axial couplings’. E P Furlani . *IEEE Transactions on*
155 *Magnetics* Sep. 1993. 29 (5) p. .
- 156 [Gradshteyn and Ryzhik ()] I S Gradshteyn , I M Ryzhik . *Table of Integrals, Series and Products*, (New York
157 and London) 1965. Academic Press Inc.
- 158 [Abramowitz and Stegun (1972)] ‘Handbook of Mathematical Functions’. M Abramowitz , I A Stegun . National
159 Bureau of Standards Applied Mathematics December 1972. 55 p. 595.
- 160 [Nakagawa et al. ()] ‘High field laboratory for superconducting materials’. Y Nakagawa , K Noto , Hoshia , K
161 Watanabe , S Miura , G Kido , Y Muto . *Physica B: Condensed Matter* 1989. 155 (1-3) p. . Institute for
162 Materials Research, Tohoku University
- 163 [Conway ()] ‘Inductance Calculations for Circular Coils of Rectangular Cross Section and Parallel Axes Using
164 Bessel and Struve Functions’. J T Conway . *IEEE Trans. Magn* 2010. 46 (1) p. .
- 165 [Grover ()] *Inductance Calculations, Chs. 2 and 13*, F W Grover . 1964. New York: Dover.
- 166 [Azzarboni et al. ()] ‘Magnetic field evaluation for thick annular conductors’. B Azzarboni , E Cardelli , M Raugi
167 , A Tellini , G Tina . *IEEE Trans. on Mag* 1993. 29 (3) p. .
- 168 [Babic ()] ‘Magnetic force between inclined circular coils (Lorentz approach)’. S I Babic , C . *Progress in*
169 *Electromagnetic Research B* 2012. 38 p. .
- 170 [Babic (2012)] ‘Magnetic force between inclined filaments placed in any desired position’. S Babic , C . *IEEE*
171 *Trans. Magn* Jan. 2012. 48 (1) p. .
- 172 [Akyel et al. ()] ‘Magnetic Force Calculation of Some Circular Coaxial Coils in Air’. C Akyel , S I Babic , S
173 Kincic , J P Lagacé . *Journal of Electromagnetic Waves and Applications* 2007. 21 (9) p. .
- 174 [Ren et al. ()] ‘Mutual Inductance and Force Calculations between Coaxial Bitter Coils and Superconducting
175 Coils with Rectangular Cross Section’. Y Ren , F Wang , G Kuang , W Chen , Y Tan , J Zhu , P He .
176 10.1007/s10948-010-1086-0. *J. Supercond. Nov. Magn* 2010.

- 177 [Babic and Akyel ()] ‘Mutual Inductance and Magnetic Force Calculations Between Thick Bitter Circular Coil
178 of Rectangular Cross Section with Inverse Radial Current and Thin Wall Superconducting Solenoid with
179 Constant Azimuthal Current’. S Babic , C Akyel . *WSEAS TRANSACTIONS on POWER SYSTEMS* 2224-
180 350X. 2018. 13.
- 181 [Babic and Akyel ()] ‘Mutual Inductance and Magnetic Force Calculations between Thick Coaxial Bitter Coil
182 of Rectangular Cross Section with Inverse Radial Current and Filamentary Circular Coil with Constan
183 Azimuthal Current’. S Babic , C Akyel . *IET Electric Power Applications* 2017. 11 (9) p. .
- 184 [Babic and Akyel ()] ‘Mutual Inductance and Magnetic Force Calculations between two Thick Coaxial Bitter
185 Coils of Rectangular Cross Section’. S Babic , C Akyel . *IET Electric Power Applications* 2017. 11 p. .
- 186 [Babic] ‘Mutual Inductance and Magnetic Force Calculations for Bitter Disk Coil (Pancake) with Nonlinear Ra-
187 dial Current and Filamentary Circular Coil with Azimuthal Current’. S Babic , S , C . 10.1155/2016/3654021.
188 ID 3654021. <http://dx.doi.org/10.1155/2016/3654021> *Advances in Electrical Engineering* Hindawi
189 Publishing Corporation. 2016.
- 190 [Babic and Akyel ()] ‘Mutual Inductance and Magnetic Force Calculations for Bitter Disk Coils (Pancakes)’. S
191 Babic , C Akyel . *Measurement & Technology* 2016. 10 p. . (IET Science)
- 192 [Babic et al. ()] ‘New expressions for calculating the magnetic field created by radial current in massive disks’. S
193 Babic , C Akyel , S J Salon , S Kincic . *IEEE Trans. Mag* 2002. 38 (2) p. .
- 194 [Babic ()] ‘New Formulas for Mutual Inductance and Axial Magnetic Force between Magnetically Coupled Coils:
195 Thick Circular Coil of the Rectangular Cross-Section-Thin Disk Coil (Pancake)’. S Babic , C . *IEEE Trans.*
196 *Magn* 2013. 49 (2) p. .
- 197 [Conway] ‘Non coaxial force and inductance calculations for bitter coils and coils with uniform radial current
198 distributions’. J T Conway . *Applied Superconductivity and Electromagnetic Devices (ASEMD), 2011*
199 *International Conference on*, p. .
- 200 [Sakai et al. ()] Y Sakai , K Inoue , H Maeda . *High-strength and high-conductivity Cu-Ag alloy sheets: new*
201 *promising conductor for high-field Bitter coils*, 1994. 30 p. .
- 202 [Bitter ()] ‘The Design of Powerful Electromagnets Part II. The Magnetizing Coil’. F Bitter . *Rev. Sci. Instrum*
203 1936. 7 (12) p. .
- 204 [Azzarboni et al. (1998)] ‘Threedimensional calculation of the magnetic field created by current-carrying massive
205 disks’. B Azzarboni , G A Saraceno , E Cardelli . *IEEE Trans. on Mag* Sept. 1998. 34 (5) p. .
- 206 [Conway ()] ‘Trigonometric Integrals for the magnetic field of the coil of rectangular cross section’. J T Conway
207 . *IEEE Trans. Magn* 2006. 42 (5) p. .
- 208 [Urankar (1982)] ‘Vector potential and magnetic field of current-carrying finite arc segment in analytical form,
209 Part III: Exact computation for rectangular cross section’. L Urankar . *IEEE Trans. Magn* Nov. 1982. 18 (6)
210 p. .