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Planar and Angular Modified Substrate Integrated Waveguide (SIW) Filter with Electromagnetic Bandgap(EBG) Structures S. Moitra¹ ¹ Dr. B C Roy Engineering College *Received: 15 December 2016 Accepted: 3 January 2017 Published: 15 January 2017* Abstract Designing of 1800 linear full mode substrate integrated waveguide(FMSIW) filter and a new

type of FMSIW filter bent with 900 angle have been proposed in this paper with a new type of
Electromagnetic bandgap structure, etched on the PEC surface (upper layer) of the main
structures to obtain the bandpass characteristics. Insertion loss is effectively low for both
(1800 FMSIW and 900 bent FMSIW) filters due to this distinct type of EBG structures.
Outcomes of Parametric analysis of the EBG structures have also been studied and presented

¹⁴ in graphical form. Entire experiments have been done with Neltec (NH-9320), the dielectric

¹⁵ constant of 3.2 and thickness of 0.8 mm. Proposed filters in this paper are used for microwave

¹⁶ Ku band applications. Both bandpass filters are compact in size, low in cost and easy to

¹⁷ fabricate. Moreover, 900 bent filters are more convenient in use where the linear filters are

18 restricted

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20 Index terms—1800 linear FMSIW filter, 900 bent FMSIW filter, ku-band, insertion loss (IL), EBG structure.

²¹ 1 Introduction

apid development in planer components is a result of growing interest in the field of wireless component design. 22 An effective approach in designing passive microwave component is the substrate integrated waveguide (SIW) 23 24 technology. In SIW dielectric material is sandwiched between two metal conducting plates and series of vias 25 are inserted in the other two sides thus forming a rectangular waveguidelike structure modified in planer form [1]. SIW inherits almost all of the advantages of conventional rectangular waveguide like low insertion loss, high 26 power handling capability in the microwave band and high-quality factor. Most of the properties of SIW like 27 dispersion characteristics, propagation constant and field pattern are similar to that of waveguide counterparts. 28 Several passive components like antennas, filters, power dividers and couplers are designed in the recent past 29 using the manifold benefits of SIW. Several filters [2], couplers [3], oscillators [4], slot array antennas [5], sixport 30 circuits [6], and circulators [7] are proposed since then. 31

In this paper, a conventional(linear) and a 90 o bent full mode SIW (FMSIW) bandpass filter embedded with new type of Electromagnetic Bandgap Structures are proposed, which exhibits the bandpass property of the microwave Ku-band.

35 For designing high Q-factor and low loss filters, SIW which is realized by metallic vias on low loss substrates 36 through printed circuit board is proved to be a useful technology [8]- [10]. In SIW fabrication process takes place 37 with using two rows of conducting cylindrical vias embedded in a dielectric substrate that connects two parallel 38 metal plates, and permit the implementation of a classical rectangular waveguide components in planar form, along with several printed passive circuitry, active devices and antennas as shown in Fig. 1. where, a s is the 39 separation between via rows (center to center), a d is the width of the structure, d is the diameter, p is the pitch 40 (as shown in Figure 1). The cut-off frequency of the SIW can be obtained by the following relation. Where c is 41 the velocity of light in vacuum. Introduction of EBG in 180 o FMSIW results in production of transmission zero 42

at around 15.04GHz, which complies the range of microwave Ku-band. The range of obtained passband is from

12.44 GHz to 14.53GHz with a minimum insertion loss of 0.71 dB. The E-field of the 180 FMSIW bandpass filter 44 is shown in Fig 6. Bending of 180 o FMSIW bandpass filter to 90 o FMSIW filter results in the production of 45 transmission zero at around 17.31GHz with a transmission bandwidth lies in the range of microwave Ku-band. 46 The range of obtained passband is from 14.61GHz to 15.97GHz with a minimum insertion loss of 0.58 dB. V. 47

2 II. 48

3 **Design** Equations 49

Parametric Analysis of EBG Structures 4 50

Microwave bandpass filter requires productive analysis of the technique to make the design effective. Several 51 useful parameters of EBG elements are varied and the output is studied in details in this paper. Effective 52 size of the EBG elements 'S 5 ' and the distance between successive EBG elements 'G v ' are studied. These 53 parameters are found to have significant effect over the insertion loss, transmission band and isolation of the 54 filter configurations. represents the variation which conveys that the stop band decreases from 16.59dB to 9.3dB 55 as the distance increases from 13.66mm to 13.76mm but after 11.76mm the stop band attenuation increases 56 with varying the distance by 0.1mm. The size of the EBG structures 'S 5' is also varied to achieve the size 57 58 of EBG structure vs. transmission bandwidth and size of EBG structure vs. stop band attenuation graph to 59 obtain greater control over passband and loss characteristics. ??ig 12. shows the Size of EBG structure vs. 60 Transmission bandwidth of EBG element. A clear observation is there that the transmission bandwidth slightly 61 decreases when the size of the EBG element increases from 0.1mm to 0.2mm and again increases by small value when the size is increased to 0.3mm and gradually decreases as the size increases by 0.4mm. Table 2. and Table 62 4. represents simulated outcomes of the linear (180 o) and 90 o bent FMSIW filters respectively. Based on the 63 parametric analysis presented in this paper, successfully achieves good filter performance like minimum loss and 64 high isolation property. 65 VI. 66

CONCLUSION $\mathbf{5}$ 67

In this article, a brief discussion is there for obtaining the bandpass characteristics of 180 o FMSIW filter and 90 68 o FMSIW filter. 180 o FMSIW filter loaded with EBG structures bent down to 90 o and analyzed the bandpass 69

characteristics for obtaining the desired passband. Bending of 180 o FMSIW filter to 90 o FMSIW filter and 70

implementation of EBG structures on both designs are found to serve the purpose quite effectively. For better 71

understanding, a detailed presentation for the analyses of several useful parameters of the EBG elements is there. 72 Additionally, with bending the linear filter, length has been decreased. Thus, 90 o bent filters are more flexible 73

than linear 180 o filters regarding the use and bandpass characteristics. Distance and size of 74

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Figure 1: Fig. 1 :



Figure 2: Fig 2 .



Figure 3: Fig. 2 :



Figure 4: Fig. 3:



Figure 5: Fig. 4 :



Figure 6: Fig. 5:



Figure 7: Fig. 6 :F



Figure 8:



Figure 9: Fig. 7:



Figure 10: Fig. 8:



Figure 11: Fig. 9 :



Figure 12: Fig. 10 : Fig. 11 :



Figure 13: F



Figure 14: Fig. 12 :



Figure 15: Fig. 13 :



Figure 16: Fig. 14 :



Figure 17: Fig. 15 :F



Figure 19: Fig. 17 :

1

Figure 20: Table 1 :

 $\mathbf{2}$

Figure 21: Table 2 :

Figure 22: Table 3 :

Figure 23: Table 4 :

75 .1 F

- ⁷⁶ EBG elements can be chosen to achieve a better result. In future, both filters can be used for such applications ⁷⁷ (radar and remote sensing operations) which complies the range of Ku band. Moreover, 90 o bent filters have
- the advantage to minimize the space complexity using its bending strategy and novel passband characteristics.
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