Impact of Seismic Load on Pier Forces in Different Type of RC Shear Walls in Concrete Frame Structures with Different Type of 2 Soil Condition 3 Mahdi Hosseini¹ 4 ¹ Jawaharlal Nehru Technological University Hyderabad 5 Received: 10 December 2016 Accepted: 4 January 2017 Published: 15 January 2017

Abstract 8

6

Shear walls are a type of structural system that provides lateral resistance to a building or 9 structure. They resist in-plane loads that are applied along its height. The applied load is 10 generally transferred to the wall by a diaphragm or collector or drag member. Shear walls are 11 analyzed to resist two types of forces: shear forces and uplift forces. Shear forces are created 12 throughout the height of the wall between the top and bottom shear wall connections. Uplift 13 forces exist on shear walls because the horizontal forces are applied to the top of the wall. 14 These uplift forces try to lift up one end of the wall and push the other end down. In some 15 cases, the uplift force is large enough to tip the wall over. Shear walls are analyzed to the 16 provide necessary lateral strength to resist horizontal forces. Shear walls are strong enough, to 17 transfer these horizontal forces to the next element in the load path below them. The seismic 18 motion that reaches a structure on the surface of the earth is influenced by local soil 19 conditions. The subsurface soil layers underlying the building foundation may amplify the 20 response of the building to earthquake motions originating in the bedrock. Three types soil 21 are considered here: Hard soil, Medium soil, soft soil. In the present work thirty story building 22 with C Shape, Box shape, E Shape, I shape and Plus shape RC Shear wall at the center in 23 Concrete Frame Structure with fixed support conditions under different type of soil for 24 earthquake zone V as per IS 1893 (part 1): 2002 in India are analyzed using software ETABS 25 by Dynamic analysis. All the analyses has been carried out as per the Indian Standard code 26 books. This paper aims to Study the effect of Seismic load on Pier Forces in Different Type of 27 RC Shear Walls in Concrete Frame Structures under Different Type of Soil Condition. 28 Estimation of Pier Forces such as; Pier Axial Force, Pier moment, Pier shear Force, Pier 29

Torsion, Time period and frequency and Modal Load Participation 30

I. Introduction a) Shear wall structure 1 34

he usefulness of shear walls in framing of buildings has long been recognized. Walls situated in advantageous 35 positions in a building can form an efficient lateral-force-resisting system, simultaneously fulfilling other functional 36 requirements. When a permanent and similar subdivision of floor areas in all stories is required as in the case 37 of hotels or apartment buildings, numerous shear walls can be utilized not only for lateral force resistance but 38 also to carry gravity loads. In such case, the floor by floor repetitive planning allows the walls to be vertically 39

³¹

³² Index terms— pier forces, response spectrum method, soft, , time period, frequency and modal load 33 participation ratios, C, Box, E, I and plus shapes

40 continuous which may serve simultaneously as excellent acoustic and fire insulators between the apartments.
41 Shear walls may be planar but are often of L-, T-, I-, or E, C, Box shaped section to better suit the planning
42 and to increase their flexural stiffness.

The positions of shear walls within a building are usually dictated by functional requirements. These may 43 or may not suit structural planning. The purpose of a building and consequent allocation of floor space may 44 dictate required arrangements of walls that can often be readily utilized for lateral force resistance. Building sites, 45 architectural interests or client's desire may lead the positions of walls that are undesirable from a structural point 46 of view. However, structural designers are often in the position to advice as to the most desirable locations for 47 shear walls in order to optimize seismic resistance. The major structural considerations for individual shear walls 48 will be aspects of symmetry in stiffness, torsional stability and available overturning capacity of the foundations 49 (Paulay and Priestley, 1992). movable partitions, permanent equipment, a part of the live load, etc. While 50 computing the seismic weight of columns and walls in any storey shall be equally distributed to the floors above 51 and below the storey. Earthquake forces experienced by a building result from ground motions (accelerations) 52 which are also fluctuating or dynamic in nature, in fact they reverse direction somewhat chaotically. The 53 magnitude of an earthquake force depends on the magnitude of an earthquake, distance from the earthquake 54 55 source(epicenter), local ground conditions that may amplify ground shaking (or dampen it), the weight(or mass) 56 of the structure, and the type of structural system and its ability to with stand abusive cyclic loading. In theory 57 and practice, the lateral force that a building experiences from an earthquake increases in direct proportion with 58 the acceleration of ground motion at the building site and the mass of the building (i.e., a doubling in ground motion acceleration or building mass will double the load). This theory rests on the simplicity and validity of 59 Newton's law of physics: F = m x a, where 'F' represents force, 'm' represents mass or weight, and 'a' represents 60 acceleration. For example, as a car accelerates forward, a force is imparted to the driver through the seat to push 61 him forward with the car(this force is equivalent to the weight of the driver multiplied by the acceleration or rate 62 of change in speed of the car). As the brake is applied, the car is decelerated and a force is imparted to the driver 63 by the seat-belt to push him back toward the seat. Similarly, as the ground accelerates back and forth during an 64 earthquake it imparts back-and-forth(cyclic) forces to a building through its foundation which is forced to move 65 with the ground. One can imagine a very light structure such as fabric tent that will be undamaged in almost 66 any earthquake but it will not survive high wind. The reason is the low mass (weight) of the tent. Therefore, 67 residential buildings generally perform reasonably well in earthquakes but are more vulnerable in high-wind load 68 69 prone areas. Regardless, the proper amount of bracing is required in both cases.

⁷⁰ 2 c) Importance of Seismic Design Codes

Ground vibration during earthquake cause forces and deformations in structures. Structures need to be designed
 withstand such forces and deformations. Seismic codes help to improve the behavior of structures so that may

73 withstand the earthquake effect without significant loss of life and property. Countries around the world have 74 procedures outlined in seismic code to help design engineers in the planning, designing, detailing and constructing

75 of structures.

⁷⁶ i. An earthquake resistant has four virtues in it, namely

The regulations in these standards do not ensure that structures suffer no damage during earthquake of all magnitude. But, to the extent possible, they ensure that structures are able to respond to earthquake shaking of moderate intensities without a. Good Structural Configuration Its size, shape and structural system carrying loads are such that they ensure a direct and smooth flow of inertia forces to the ground.

⁸¹ 3 b. Lateral Strength

The maximum lateral (horizontal) force that it can resist is such that the damage induced in it does not result in collapse.

c. Adequate Stiffness Its lateral load resisting system is such that the earthquake -indeed deformations in it do not damage its contents under low-to-moderate shaking.

d. Good Ductility Its capacity to undergo large deformations under severe earthquake shaking even after yielding is improved by favorable design and detailing strategies.

88 4 ii. Indian Seismic Codes

89 Seismic codes are unique to a particular region or country. They take into account the local seismology, accepted

- 90 level of seismic risk, buildings typologies, and materials and methods used in construction.
- 91 The

$_{92}$ 5 d) Site Selection

 $\mathbf{93}$ The seismic motion that reaches a structure on the surface of the earth is influenced by local soil conditions. The

94 subsurface soil layers underlying the building foundation may amplify the response of the building to earthquake 95 motions originating in the bedrock.

For soft soils the earthquake vibrations can be significantly amplified and hence the shaking of structures sited on soft soils can be much greater than structural damage and of heavy intensities wit out total collapse. soil investigation should be carried out to establish the allowable bearing capacity and nature of soil. The choice of
 a site for a building from the failure prevention for structures sited on hard soils. Hence the appropriate Global
 Journal of Researches in Engineering () Volume XVII Issue IV Version I

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Year 2017 E ground. The very loose sands or sensitive clays are liable to be destroyed by the earthquake, so much as to lose their original structure and thereby undergo compaction. This would result in large unequal settlements and damage the building. If the loose cohesion less soils are saturated with water they are likely to lose their shear resistance altogether during ground shaking. This leads to liquefaction. Although such soils can be compacted, for small buildings the operation may be too costly and the sites having these soils are better avoided.

For large building complexes, such as housing developments, new colonies, etc. this factor should be thoroughly 108 investigated and the site has to be selected appropriately. Therefore a site with sufficient bearing capacity and 109 free from the above defects should be chosen and its drainage condition improved so that no water accumulates 110 and saturates the ground especially close to the footing level. e) Bearing capacity of foundation soil i. Hard-Those 111 soils, which have an allowable bearing capacity of more than 10t/m2. ii. Medium-Those soils, which have an 112 allowable bearing capacity less than or equal to $10t/m^2$. iii. Soft-Those soils, which are liable to large differential 113 settlement or liquefaction during an earthquake. Soils must be avoided or compacted to improve them so as to 114 qualify them either as firm or stiff. The allowable bearing pressure shall be determined in accordance with IS: 115 1888-1982 load test (Revision 1992). It is a common practice to increase the allowable bearing pressure by one-116 third, i.e. 33%, while performing seismic analysis of the materials like massive crystalline bedrock sedimentary 117 rock, dense to very dense soil and heavily over consolidated cohesive soils, such as a stiff to hard clays. For the 118 structure to react to the motion, it needs to overcome its own inertia, which results in an interaction between the 119 structure and the soil. The extent to which the structural response may alter the characteristics of earthquake 120 motions observed at the foundation level depends on the relative mass and stiffness properties of the soil and the 121 structure. 122

Thus the physical property of the foundation medium is an important factor in the earthquake response of 123 structures supported on it. There are two aspects of building foundation interaction during earthquakes, which 124 are of primary importance to earthquake engineering. First, the response to earthquake motion of a structure 125 founded on a deformable soil can be significantly different from that would occur if the structure is supported on 126 a rigid foundation. Second, the motion recorded at the base of a structure or in the immediate vicinity can be 127 different from that which would have been recorded had there been no building. Observations of the response of 128 the buildings during earthquakes have shown that the response of typical structures can be markedly influenced 129 130 by the soil properties if the soils are sufficiently soft. Furthermore, for relatively rigid structures such as nuclear reactor containment structures, interaction effects can be important, even for relatively firm soils because the 131 important parameter apparently is not the stiffness of the soil, but the relative stiffness of the building and its 132 foundation. In terms of the dynamic properties of the building foundation system, past studies have shown that 133 the interaction will, in general, reduce the fundamental frequency of the system from that of the structure on a 134 rigid base, dissipate part of the vibrational energy of the building by wave radiation into the foundation medium 135 and modify the base motion of the structure in comparison to the free-field motion. Although all these effects 136 may be present in some degree for every structure, the important point is to establish under what conditions the 137 138 effects are of practical significance.

¹³⁹ 7 f) Seismic Behavior of RC Shear Wall

140 8 II. Methodology

Earthquake motion causes vibration of the structure leading to inertia forces. Thus a structure must be able to safely transmit the horizontal and the vertical inertia forces generated in the super structure through the foundation to the ground. Hence, for most of the ordinary structures, earthquake-resistant design requires ensuring that the structure has adequate lateral load carrying capacity. Seismic codes will guide a designer to safely design the structure for its intended purpose.

- 146 1. Equivalent Static Lateral Force Method (pseudo static method). 2. Dynamic Analysis.
- 147 i. Response spectrum method.
- 148 ii. Time history method.

¹⁴⁹ 9 a) Equivalent lateral Force (Seismic Coefficient) Method

This method of finding lateral forces is also known as the static method or the equivalent static method or the seismic coefficient method. The static method is the simplest one and it requires less computational effort and is based on formulae given in the code of practice.

In all the methods of analyzing a multi storey buildings recommended in the code, the structure is treated as discrete system having concentrated masses at floor levels which include the weight of columns and walls in any storey should be equally distributed to the floors above and below the storey. In addition, the appropriate amount of imposed load at this floor is also lumped with it. It is also assumed that the structure flexible and will deflect with respect to the position of foundation the lumped mass system reduces to the solution of a system of second order differential equations. These equations are formed by distribution, of mass and stiffness in a structure, together with its damping characteristics of the ground motion.

¹⁶⁰ 10 Dynamic Analysis

Dynamic analysis shall be performed to obtain the design seismic force, and its distribution in different levels along the height of the building, and in the various lateral load resisting element, for the following buildings:

The analysis of model for dynamic analysis of buildings with unusual configuration should be such that it adequately models the types of irregularities present in the building configuration. Buildings with plan irregularities, as defined in Table 4 of IS code: 1893-2002 cannot be modeled for dynamic analysis.

¹⁶⁶ 11 Dynamic analysis may be performed either by the TIME ¹⁶⁷ HISTORY METHOD or by the RESPONSE SPECTRUM ¹⁶⁸ METHOD Time History Method

The usage of this method shall be on an appropriate ground motion and shall be performed using accepted principles of dynamics. In this method, the mathematical model of the building is subjected to accelerations from earthquake records that represent the expected earthquake at the base of the structure.

172 12 Response Spectrum Method

The word spectrum in engineering conveys the idea that the response of buildings having a broad range of periods is summarized in a single graph. This method shall be performed using the design spectrum specified in code or by a site-specific design spectrum for a structure prepared at a project site. The values of damping for building may be taken as 2 and 5 percent of the critical, for the purposes of dynamic of steel and reinforce concrete buildings, respectively. For most buildings, inelastic response can be expected to occur during a major earthquake, implying that an inelastic analysis is more proper for design. However, in spite of the availability of nonlinear inelastic programs, they are not used in typical design practice because:

1. Their proper use requires knowledge of their inner workings and theories. design criteria, and 2. Result produced are difficult to interpret and apply to traditional design criteria, and 3. The necessary computations are expensive. Therefore, analysis in practice typically use linear elastic procedures based on the response spectrum method. The response spectrum analysis is the preferred method because it is easier to use.

184 13 III. Literature Review

Generally, the building configuration which is conceived by architects and then accepted by developer or owner may provide a narrow range of options for lateral-load resistant systems that can be utilized by structural engineers. By observing the following fundamental principles relevant to seismic responses, more suitable structural systems may be adopted (Paulay and Priestley, 1992):

1. To perform well in an earthquake, a building should possess simple and regular configurations. Buildings 189 with articulated plans such as T and L shapes should be avoided. 2. Symmetry in plans should be provided, 190 wherever possible. Lack of symmetry in plan may lead to significant torsional response, the reliable prediction of 191 192 which is often difficult. 3. An integrated foundation system should tie together all vertical structural elements in both principal directions. Foundation resting on different soil condition should preferably be avoided. 4. Lateral 193 force resisting systems with significantly different stiffness such as shear walls and frames within one building 194 should be arranged in such a way that at every level of the building, symmetry in lateral stiffness is not grossly 195 violated. Thus, undesirable torsional effects will be minimized. 196

Quite a few methods are available for the earthquake analysis of buildings; two of them are presented here: ??013) studied lateral displacement and inter-story drift on a square symmetric structure with walls at the centre and at the edges, and found that the presence of shear wall can affect the seismic behaviour of frame structure to large extent, and the shear wall increases the strength and stiffness of the structure.c) b) Global Journal of

Sagar K.et al., (2012) carried out linear dynamic analysis on two sixteen storey high buildings. It was concluded
 that shear walls are one of the most effective building elements in resisting lateral forces during earthquake.
 Providing shear walls in proper position minimizes effect and damages due to earthquake and winds.

Kumbhare P.S. et al., (2012) carried out a study on shear wall frame interaction systems and member forces. It was found that shear wall frame interaction systems are very effective in resisting lateral forces induced by earthquake. Placing shear wall away from center of gravity resulted in increase in the most of the members forces. It follows that shear walls should be coinciding with the centroid of the building.

Rahman A. et al., (2012) studied on drift analysis due to earthquake load on tall structures. In this study regular shaped structures have been considered. Estimation of drift was carried out for rigid frame structure, coupled shear wall structure and wall frame structure. Anshuman et al., (2011) conducted a research on solution of shear wall location in multi storey building. An earthquake load was calculated and applied to a fifteen storied building located in zone IV. It was observed

that the top deflection was reduced and reached within the permissible deflection after providing the shear wall.

Kameshwari B. et al., (2011) analyzed the effect of various configurations of shear walls on high-rise structure.

The drift and inter-storey drift of the structure in the following configurations of shear wall panels was studied and was compared with that of bare frame. Diagonal shear wall configuration was found to be effective for

- 217 structures in the earthquake prone areas.
- Based on the literature review, the salient objective of the present study have been identified as follows: ?

²¹⁹ 14 a) Details of The Building

A symmetrical building of plan 38.5m X 35.5m located with location in zone V, India is considered. Four bays of length 7.5m& one bays of length 8.5m along X -direction and Four bays of length 7.5m& one bays of length

5.5m along Y -direction are provided. Shear Wall is provided at the center core of building model.

223 **15** Structure 1:

In this model building with 30 storey is modeled as a (Dual frame system with shear wall (Plus Shape) at the center of building, The shear wall acts as vertical cantilever.

Structure 2: In this model building with 30 storey is modeled as (Dual frame system with shear wall (Box Shape) at the center of building ,The shear wall acts as vertical cantilever.

Structure 3: In this model building with 30 storey is modeled as (Dual frame system with shear wall (C-Shape) at the center of building, The shear wall acts as vertical cantilever.

Structure 4: In this model building with 30 storey is modeled as (Dual frame system with shear wall (E-230 Shape) at the center of building ,The shear wall acts as vertical cantilever. When a structure is subjected 231 to earthquake, it responds by vibrating. An example force can be resolved into three mutually perpendicular 232 directions two horizontal directions (X and Y directions) and the vertical direction (Z). This motion causes the 233 structure to vibrate or shake in all three directions; the predominant direction of shaking is horizontal. All the 234 structures are primarily designed for gravity loads-force equal to mass time's gravity in the vertical direction. 235 Because of the inherent factor used in the design specifications, most structures tend to be adequately protected 236 against vertical shaking. Vertical acceleration should also be considered in structures with large spans those in 237 which stability for design, or for overall stability analysis of structures. The basic intent of design theory for 238 earthquake resistant structures is that buildings should be able to resist minor earthquakes without damage, 239 resist moderate earthquakes without structural damage but with some non-structural damage. To avoid collapse 240 during a major earthquake, Members must be ductile enough to absorb and dissipate energy by post elastic 241 deformation. Redundancy in the structural system permits redistribution of internal forces in the event of the 242 failure of key elements. When the primary element or system yields or fails, the lateral force can be redistributed 243 to a secondary system to prevent progressive failure. 244

245 The result obtained from the analysis models will be discussed and compared as follows:

It is observed that? The time period is 6.298 Sec for structure1 and it is same for different type of soil.? 246 The Frequency is 0.159 cyc/sec for structure1 and it is same for different type of soil. ? The time period is 5.785 247 Sec for structure2 and it is same for different type of soil. ? The Frequency is 0.173 cyc/sec for structure2 and 248 it is same for different type of soil. ? The time period is 6.415 Sec for structure3 and it is same for different 249 type of soil. ? The Frequency is 0.156 cyc/sec for structure3 and it is same for different type of soil. ? The time 250 period is 6.375Sec for structure4 and it is same for different type of soil. ? The Frequency is 0.157 cyc/sec for 251 structure4 and it is same for different type of soil. ? The time period is 6.382 Sec for structure5 and it is same 252 for different type of soil. ? The Frequency is 0.157 cyc/sec for structure5 and it is same for different type of soil. 253

 $_{\rm 254}~$? Pier Shear Forces V3 in X direction for soft soil >Medium soil > hard soil.

? Pier Shear Forces V3 in X direction for soft soil >Medium soil > hard soil. ? Pier Torsion in X direction
for soft soil >Medium soil > hard soil. ? Pier Torsion in Y direction for soft soil <Medium soil < hard soil.

257 16 VII. Conclusions

In this paper, reinforced concrete shear wall buildings were analyzed with the procedures laid out in IS codes.
Seismic performance of building model is evaluated.

From the above results and discussions, following conclusions can be drawn: ? Building with box shape Shear 260 261 Walls provided at the center core showed better performance in terms of Pier Forces. ? The shear wall and 262 it is position has a significant influenced on the time period. The time period is not influenced by the type of 263 soil. ? There is considerable difference in Pier Moment with a Different type of soils and structures. ? There is considerable difference in Pier shear force with a Different type of soils and structures. ? There is not considerable 264 difference in Pier axial forces with a Different type of soils and structures. ? It is evident that Pier Torsion in X 265 direction for all structures in soft soil more than Medium soil and more than hard soil. ? It is evident that Pier 266 Torsion in Y direction for soft soil less than Medium soil and less than hard soil. ? shear is effected marginally by 267 placing of the shear wall, grouping of shear wall and type of soil. The shear is increased by adding shear wall due 268 to increase the seismic weight of the building. ? The moment resisting frame with shear walls are very good in 269

lateral force such as earthquake and wind force. The shear walls provide lateral load distribution by transferring 270 the wind and earthquake loads to the foundation. And also impact on the lateral stiffness of the system and also 271 carries gravity loads. ? It is evident that shear walls which are provided from the foundation to the rooftop, 272 are one of the excellent mean for providing earthquake resistant to multistory reinforced building with different 273 type of soil. ? The vertical reinforcement that is uniformly distributed in the shear wall shall not be less than 274 the horizontal reinforcement .This provision is particularly for squat walls (i.e. Height-to-width ratio is about 275 1.0). However, for walls whit height-to-width ratio less than 1.0, a major part of the shear force is resisted by the 276 vertical reinforcement. Hence, adequate vertical reinforcement should be provided for such walls. ? Based on 277 the analysis and discussion ,shear wall are very much suitable for resisting earthquake induced lateral forces in 278 multistoried structural systems when compared to multistoried structural systems whit out shear walls. They 279 can be made to behave in a ductile manner by adopting proper detailing techniques. ? According to IS-1893:2002 280 the number of modes to be used in the analysis should be such that the total sum of modal masses of all modes 281 considered is at least 90 percent of the total seismic mass. Here the maximum mass for structure 2 is 94.7 percent 282 and minimum mass for structure 1 is 86.71 percent. 283

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SEISMIC BEHAVIOUR...

- At each section along the heig shear wall carries
 - Axial Force P
 - Shear Force V
 - Bending Moment M

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Figure 1: Structure 5 : 2017 ETable 1 :Fig. 1 : 1 Fig. 2 : 1 Fig. 3 : 2 Fig. 4 : 2 Global 2017 EFig. 6 : 3 Fig. 5 : 3 Fig. 7 : 2017 EFig. 8 : 4 Fig. 9 : 2017 EFig. 10 :

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SEISMIC BEHAVIOUR ...

Shear demand is more in lower storeys



Figure 2:

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ARCHITECTURAL ASPECTS...

Shear wall building should not be narrow

- Earthquakes cause significant overturning effects
- Special care is required in design of their foundations



Figure 3:

ARCHITECTURAL ASPECTS ...

• Walls must be symmetrically placed in plan



Figure 4:

ARCHITECTURAL ASPECTS ...

Walls should be along perimeter of building

- Improves resistance to twist



Figure 5:

SHEAR WALLS...

Advantages of Shear Walls...

- Lesser lateral displacement than frames
- Lesser Damage to structural and non-structural elements





Figure 6:

SHEAR WALLS...



Figure 7:

SHEAR WALLS...

• Principal attributes

- Large Strength
- High Stiffness
- Ductility
 - Shear wall can be detailed to have large ductility



Figure 8:



Figure 9:





Figure 11:



5. d)

u)	
	Year 2017
	15
Regular buildings: Those greater than 40m in height in zones	() Volume XVII
IV and V, those greater than 90m in height in zone II and III.	Issue IV Version
Irregular buildings: All framed buildings higher than 12m	I E Researches in
	Engineering
in zones IV and V, and those greater than 40m in height	
in zones II and III.	

[Note: Sardar S.J. et al., (]

Figure 13:

Figure 14:

 $\mathbf{2}$

Table: Pier Forces Story Pier	Load	LocatiStructure -1 Structure -2 Structure -3 Structure -4 Structu
	Case/Cor	mbo

1ST	P3	12DLRLLEQXP -31716.3887 -33051.4245 -34550.8106	 6407 997107 969
1ST	P3	12DLRLLER X 10 m 31976.2637 - 33311.2995 - 34810.6856	 6627. 7346 87.137
1ST 1ST	P3 P3	12DLRLLEQYP -31716.3887 -25170.9557 -32781.7792 -1363 12DLRLLEQYPDmB1976.2637 -25430.8307 -33041.6542 -1376	31.3189 -33874.52 51.2564 -34134.39

[Note: Axial Force, P for structures with the load combination 1.2 (DL+LL+EQXP) &1.2 (DL+LL+EQYP) in soft soil]

Figure 15: Table 2 :

3

Table: Pie	er Forces		Structure -1 Structure -2 Structure -3 Structure -4 Struc	Structure -5
Story Pie	r	Load Locati	oR	РРРР
		Case/Combo		
			kN	kNkNkNkN
1ST	P3	12DLRLLEQ X AP	-31716.3887 -35888.3932 -35187.6619 -3330.9739	-
				33266
1ST	P3	12DLRLLEQ X oftor	n - 31976.2637 - 36148.2682 - 35447.5369 - 3460.9114	-
				33526
1ST	P3	12DLRLLEQ Ұ ф	-31716.3887 -25170.9557 -32781.7792 -13631.3189 -3	3874.5608
1ST	P3	12DLRLLEQ B ortor	n - 31976.2637 - 25430.8307 - 33041.6542 - 13761.2564 - 3	4134.4358

Figure 16: Table 3 :

$\mathbf{4}$

Table:	Load	Locati	Structure	-1	Structure	-2	Structure	-3
Pier	Case/Com	bToop	Structure -4	$4 \mathrm{Str}$	ructure -5 P	$\mathbf{P} \mathbf{P}$	P P kN kN	kΝ
Forces	12DL-	Bot-	kN kN -317	716.3	3887 -38331	.3385	5 -35736.061	16 -
Story	RLLE-	tom	983.1011 -3	312'	7.6731 -3197	6.26	37 -38591.2	135
Pier	QXP	Top	-35995.9366	5	-1113.0386	-3	3387.5481	-
1ST P3	12DL-	Bot-	31716.3887	-	-25170.9557	-3	82781.7792	-
1ST P3	RLLE-	tom	13631.3189		-33874.595	-3	1976.2637	-
1ST P3	QXP		25430.8307	-33(041.6542 - 13	8761.2	2564 -34134	1.47
1ST P3	12DL-							
	RLLE-							
	QYP							
	12DL-							
	RLLE-							
	QYP							
	Table: Pier Forces Story Pier 1ST P3 1ST P3 1ST P3 1ST P3	Table:LoadPierCase/ComForces12DL-StoryRLLE-PierQXP1ST P312DL-1ST P3RLLE-1ST P312DL-1ST P312DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-	Table:LoadLocatiPierCase/CombTopForces12DL-StoryRLLE-VariableTop1ST P312DL-1ST P3RLLE-1ST P3QXP1ST P312DL-RLLE-QYP1ST P312DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-	Table:LoadLocationPierCase/Comb TopStructureForces12DL-Bot-kN kN -317StoryRLLE-tom983.1011 -3PierQXPTop-35995.93661ST P312DL-Bot-31716.38871ST P3RLLE-tom13631.31891ST P3QXP25430.83071ST P312DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP	Table: Load Location function Pier Case/Comboo Structure -4 S	Table:LoadLocation functionInstructureInstructurePierCase/Comb TopStructure-4 Structure-5 PForces12DL-Bot-kN kN -31716.3887 -38331StoryRLLE-tom983.1011 -33127.6731 -3197PierQXPTop-35995.9366 -1113.03861ST P312DL-Bot-31716.3887 -25170.95571ST P3RLLE-tom13631.3189 -33874.5951ST P3QXP25430.8307 -33041.6542 -131ST P312DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-	Table:LoadLocatiostructure-1Structure-2PierCase/CombTopStructure-4Structure-5PPForces12DL-Bot-kN kN -31716.3887 -38331.3385StoryRLLE-tom983.1011 -33127.6731 -31976.26PierQXPTop-35995.9366 -1113.0386 -31ST P312DL-Bot-31716.3887 -25170.9557 -31ST P3RLLE-tom13631.3189 -33874.595 -31ST P3QXP25430.8307 -33041.6542 -13761.31ST P312DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-	Table:LoadLocati \Im tructure-1Structure-2StructurePierCase/CombTopStructure-4Structure-5PPPPNNForces12DL-Bot-kNkN-31716.3887-38331.3385-35736.063StoryRLLE-tom983.1011-33127.6731-31976.2637-38591.2PierQXPTop-35995.9366-1113.0386-33387.54811STP312DL-Bot-31716.3887-25170.9557-32781.77921STP3RLLE-tom13631.3189-33874.595-31976.26371STP3QXP25430.8307-33041.6542-13761.2564-341341STP312DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLLE-QYP12DL-RLE-QYP12DL-RLE-QYP12DL-RLE-QYP12DL-RLE-QYP12DL-RLE-QYP12DL-RLE-QYPRLE-NRLE-NRE-NRE-NRE-N<

Figure 17: Table 4 :

 $\mathbf{5}$

5 Structure	e -5	M3	kN -	-61.6944	-17.1098	11107.3586
			m			
Structure -		M2	kN -	-65.0181	-290.8369	-57.7674
			m			
-4 Structur	e -4	M3	kN -	1861.0597	6530.9935	-716.6361
			m			
Structure	-1	Location M2 M3 M2 M3 M2 M3 M2	kN-m	Top	Bottom	Top -10.326
Structure	-1		kN-m	429.3134	-796.6308	29494.5797
Structure	-2		kN-m	-285.376	-244.1397	0.9942
Structure	-2		kN	54.4708	-444.1125	19086.5309
Structure	-3		-m	1200.3755	-365.0748	0.9679
Structure	-3		kN	1.9394	-496.6401	18817.9303
Structure			-m	237.7991	403.2212	21.4569
			kN	-17.4689	21.225	
			-m			
			kN			
			-m			
		Load Case/Combo		12DLRLLEG	XIP2DLRLLEQX	XH2DLRLLE
Table:	Pier	Story Pier		1ST P3	1ST P3	1ST P3
Forces						

Figure 18: Table 5 :

6

medium soil

Figure 19: Table 6 :

7

м	for	Tables . Dier	Storr	I-N	1 C T	рэ	1 C T	DЭ	57 765	7	62 026'	7	<u> </u>	Voon
IVI	101		Story	KIN-	1001	гэ	101	гэ	-01.100	700	03.930	1	20	rear
stru	c-	Structure	Pier	m	12DL	R-	12DLR	(-	18572.3	599	58222.2	2947	2017	(
ture	\mathbf{s}	Forces -1	Load	kN-	LLEQ	QXP	LLEQ	ХP	1ST	P3	1ST	P3	Gloł	bal
with	ı	Structure -1	Case/C	Commbo	Top		Botton	n	12DLR	l-	12DLR	l-	Jour	mal
the	load	Structure -2	Loca-	kN-	723.87	721	-1333.0)941	LLEQ	ΥP	LLEQ	ΥP	of	$\operatorname{Re-}$
com	bi-	Structure -2	tion	m	-285.3	76	-244.13	397	Top	-	Botton	n	sear	ches
nati	on	Structure -3	M2	kN-	90.300)1	-739.23	339	10.3264	4	4.0607		in E	ngi-
1.2		Structure -3	M3	m	2004.6	5271	-609.67	748	49447.1	15	68956.4	455	neer	ing
(DL	+LL-	⊢ £KQuXcP ure -4	M2	kN-	2.5903	3	-826.14	452	0.9942		-3.6328	3	()
&1.2	2	Structure -4	M3	m	397.12	246	673.379	95	31874.5	5067	46716.3	3716	Volu	ıme
(DL	+LL-	⊢ £KQU∕c₽ ùre -5	M2	kN-	-30.97	03	37.629^{4}	4	0.9679		-4.8413	3	XVI	Ι
in ł	nard	Structure -5	M3	m	3853.6	5925	10781.'	7386	31425.9	9437	52818.2	2271	Issu	e IV
soil			M2	kN-	-69.87	'43	-528.53	339	38.0596	6	246.04	68	Vers	sion
			M3	m	-79.71	96	-15.749	96	-716.63	861	1031.43	388	I E	
			M2	kN-										
			M3	m										
				kN-										
				m										
				kN-										
				m										

Figure 20: Table 7 :

10

Force,	hardV2	V3	kN	11. 7818 -	11. 7818 -	5574. 0871	5574. 0871
V fe	or soilV2	V3	kΝ	587. 7046 -	587. 7046 -	4. 1106 4240.	4. 1106 4240.
structure	es V2	V3	kΝ	746. 9434 -	746. 9434 -	5328 - 1. 322	5328 -1. 322
with	V2	V3	kΝ	237. 0097 78.	237. 0097 78.	6112. 081 -1.	6112. 081 -1.
the loa	nd V2	V3	kΝ	93 -236. 7816	93 -236. 7816	6598 499.45	6598 499.45
combina	-		kN	1979. 4418 19.	1979. 4418 19.	59. 4249	59. 4249
tion 1	.2		kN	5999 18. 2771	5999 18. 2771	11328. 4845	11328.4845
(DL+LL	+EQXP)		kN	-131. 0456	-131.0456	34. 7721	34. 7721
&1.2	- ,		kN				
(DL+LL	+EQYP)		kN				
in	- ,						
	Sto	r		1ST P3 12D	1ST P3 12D	1ST P3 12D	1ST P3 12D
	у	Pier		LR LLEQXP	LR LLEQXP	LR LLEQYP	LR LLEQYP
	Ĺ	oad		Тор	B ottom	Тор	B ottom
	Cas	se/Con	ıbo	-		-	
	Loc	ea-					
	tior	1					

Figure 21: Table 10 :

8

soft soil

Figure 22: Table 8 :

9

medium soil

Figure 23: Table 9 :

11

Table: P	ier Forces		Structure -1 S	tructure -2	Structure -3	Structure -4 St	ructure -
Story	Pier	Load Locati Case/Combo	ionT	Т	Т	Т	Т
			kN-m	kN-m	kN-m	kN-m	kN-m
1ST	P3	12DLRLLEQXITop	-57.8883	-	-32.2595	-17.3115	-
				31.8229			33.9525
1ST	P3	12DLRLLEQX B otton	m -57.8883	-	-32.2595	-17.3115	-
				31.8229			33.9525
1ST	P3	12DLRLLEQYFop	46.5531	41.9152	92.9513	35.9013	85.1595
1ST	P3	12DLRLLEQY B otton	$m \ 46.5531$	41.9152	92.9513	35.9013	85.1595

Figure 24: Table 11 :

12

Pier Forces			Structure -1 Structure	-2 Structu	ire -3 Stru	cture -4 S	tructure
Pier	Load	Location	Т	Т	Т	Т	Т
	Case/Combo						
			kN-m	kN-m	kN-m	kN-m	kN-m
P3	12DLRLLEQXP	Top	-75.9256	-	-43.873	-	-
				43.2792		24.9942	46.173
P3	12DLRLLEQXP	Bottom	-75.9256	-	-43.873	-	-
				43.2792		24.9942	46.173
P3	12DLRLLEQYP	Top	66.1147	57.0047	126.4138	51.8336	115.81
P3	12DLRLLEQYP	Bottom	66.1147	57.0047	126.4138	51.8336	115.81
	Pier Forces Pier P3 P3 P3 P3 P3 P3	Pier Forces Pier Load Case/Combo P3 12DLRLLEQXP P3 12DLRLLEQXP P3 12DLRLLEQYP P3 12DLRLLEQYP P3 12DLRLLEQYP	Pier Forces PierLoad Case/ComboLocation LocationP312DLRLLEQXPTopP312DLRLLEQXP BottomP3 P312DLRLLEQYPTop 12DLRLLEQYPBottom	Pier ForcesStructure -1 StructurePierLoadLocationCase/ComboKN-mP312DLRLLEQXPTop-75.9256P312DLRLLEQXP Bottom-75.9256P312DLRLLEQYPTop66.1147P312DLRLLEQYPBottom66.1147	Pier ForcesStructure -1 Structure -2 StructurePierLoadLocationTCase/CombokN-mkN-mP312DLRLLEQXPTop-75.9256-P312DLRLLEQXP Bottom-75.9256-P312DLRLLEQXPTop66.114757.0047P312DLRLLEQYPTop66.114757.0047	Pier Forces Structure -1 Structure -2 Structure -3 Structure Pier Load Location T T Case/Combo KN-m KN-m KN-m P3 12DLRLLEQXPTop -75.9256 - -43.873 P3 12DLRLLEQXP Bottom -75.9256 - -43.873 P3 12DLRLLEQXP Top 66.1147 57.0047 126.4138 P3 12DLRLLEQYPBottom 66.1147 57.0047 126.4138	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

Figure 25: Table 12 :

$\mathbf{13}$

2 (DL+LL+EQXP) &1.2 (DL+LL+EQYP) in hard soil

Figure 26: Table 13 :

$\mathbf{14}$

Static Dynamic	% %	91.54 99.97	99.97
Dynamic	%	94.54	91.83
Static	%	99.99	99.97
Dynamic	%	94.59	91.85
Static	%	99.98	99.97
Static Dynamic	% %	99.99 94.7	$99.98 \ 91.46$
Static Dynamic	% %	99.82 86.71	$99.79 \ 87.46$
Item Type Item		Acceleration UX	Acceleration UY
Case		Modal	Modal

Figure 27: Table 14 :

15

	E
	-0
	Structure
	-5
	Structure
	4
Year 2017 26 Journal of Re-	Structure -1 Structure -2 Structure -4
searches in Engineering () Vol-	Structure -3 Structure -1 Structure -2 Structure -3
ume XVII Issue IV Version I E	
	Table: Pier Forces

Figure 28: Table 15 :

It is observed that

Shear Wall forces (Pier Forces) for structure 1

? For the Pier axial forces in X direction There is not

? Pier Torsion in X direction for soft soil
>Medium soil
> hard soil.
? Pier Torsion in Y direction for soft soil
<Medium soil

< hard soil.

It is observed that Shear Wall forces (Pier Forces) for structure 4

Pier axial forces Year? 2017 in X direction for soft Soil <Medium 28Globsbil < Hard soil ? Jour-Pier Moment M2 in nal X direction for soft of soil >medium soil Re- > hard soil.? searcheiser Moment M3 in in X direction for soft En- soil < medium soil gi-< hard soil. ? neer-Pier Moment M2 in Y direction for soft ing Ε soil <Medium soil () < hard soil. ? Vol- Pier Moment M3 in ume Y direction for soft XVIIsoil >Medium soil > Ishard soil. ? Pier Shear Forces V2 in sue X direction for soft IV Ver- soil <Medium soil <sion hard soil. ? Pier Ι Shear Forces V3 in X direction for soft soil > Medium soil >

hard soil. ?

considerable difference for soft Soil, Medium soil & Hard soil.

? Pier Moment M2 in X direction for soft soil < medium soil < hard soil.

? Pier Moment M3 in X direction for soft soil =medium

soil = hard soil. ? Pier Moment M2 in Y direction for soft soil = Medium soil = hard soil. ? Pier Moment M3 in Y direction for soft soil < Medium soil < hard soil. ? Pier Shear Forces V2 in X direction for soft soil =Medium soil = hard soil. ? Pier Shear Forces V3 in X direction for soft soil >Medium soil > hard soil. ? Pier Torsion in X direction for soft soil >Medium soil > hard soil. ? Pier Torsion in Y direction for soft soil <Medium soil < hard soil It is observed that Shear Wall forces (Pier Forces) for structure 2? Pier axial forces in X direction for soft Soil >Medium soil > Hard soil ? Pier Moment M2 in X direction for soft soil < medium soil < hard soil . ? Pier Moment M3 in X direction for soft soil <medium soil <hard soil . ? Pier Moment M2 in Y direction for soft soil = Medium soil = hard soil . ? Pier Moment M3 in Y direction for soft soil < Medium soil < hard soil . ? Pier Shear Forces V2 in X direction for soft soil >Medium soil > hard soil. ? Pier Shear Forces V3 in X direction for soft soil >Medium soil > hard soil. ? Pier Torsion in X direction for soft soil >Medium soil > hard soil. ? Pier Torsion in Y direction for soft soil < Medium soil < hard soil. It is observed that Shear Wall forces (Pier Forces) for structure 3? Pier axial forces in X direction for soft Soil >Medium soil > Hard soil

? Pier Moment M2 in X direction for soft soil <medium soil < hard soil.

? Pier Moment M3 in X direction for soft soil <medium soil < hard soil.

? Pier Moment M2 in Y direction for soft soil =Medium soil = hard soil.

? Pier Moment M3 in Y direction for soft soil < Medium soil < hard soil.

? Pier Shear Forces V2 in X direction for soft soil

<Medium soil < hard soil.

Year 2017 29 E

Figure 30:

- [Bureau Of Indian ()] Bureau Of Indian . Standards: IS 875. Dead loads on buildings and Structures, (New Delhi, India) 1987. (part 1)
- [Bureau Of Indian and Standards ()] Bureau Of Indian , Standards . Live loads on buildings and Structures,
 (New Delhi, India) 1987. 875. (part 2)
- [Chopra ()] A K Chopra . Dynamics of Structures: Theory and Application to Earthquake Engineering, 2012.
 Pearson Education. (4th edition)
- [Bureau Of Indian ()] Criteria for earthquake resistant design of structures: Part 1 General provisions and
 buildings, Bureau Of Indian . Standards: IS 1893. 2002. New Delhi, India.
- [Rahangdale and Satone ()] 'Design and analysis of multi-storied building with effect of shear wall'. H Rahangdale
- , S R Satone . International journal of engineering research and application 2013. 3 p. . (Global Journal of Researches in Engineering. XVII Issue IV Version I)
- [Gary et al. (2004)] Design drifts requirement for long period structures, R Gary, Sigmund A Scarer, Freeman
 Aug 2004. B.C, Canada. p. 3292.
- [Humar and Yavari (2002)] Design of concrete shear wall buildings for earthquake induced torsion". 4'1" structural
 conference of the Canadian society for civil engineering, J L Humar, S Yavari. June-2002.
- Bureau Of Indian] Ductile detailing of reinforced concrete structures subjected to seismic forces-Code of Practice,
 Bureau Of Indian . Standards: IS 13920: 1993. New Delhi, India.
- 303 [Chandiwala (2008)] 'Earthquake Analysis of Building Configuration with Different Position of Shear Wall'. A
- Chandiwala . International Journal of Emerging Technology and Advanced Engineering 2250-2459. 2008.
 December 2012. 9001 (12) . (Certified Journal)
- 306 [Duggal ()] Earthquake Resistant Design of Structures, S K Duggal . 2010. New Delhi: Oxford University Press.
- [Berkeley (2003)] 'ETABS Integrated Building Design Software'. Berkeley . Computers and Structure, Inc
 February 2003.
- [Plain and Reinforced Concrete-Code of practice IS ()] 'Plain and Reinforced Concrete-Code of practice'. IS
 2000. 456. Bureau of Indian Standars
- [Chandurkar et al. ()] 'Seismic analysis of RCC building with and without shear wall'. P P Chandurkar , Dr , P
 S Pajgade . International Journal of Modern Engineering Research 2013. 3 p. .
- [Anand et al. (2010)] 'Seismic behaviour of RCC shear wall under different soil conditions'. N Anand , C Mightraj
 , G Prince Arulraj . Indian geotechnical conference Dec -2010. p. .
- [Paulay and Priestley ()] Seismic design of reinforced concrete and masonry buildings, T Paulay, M J N Priestley
 . 1992.
- [Anshuman et al. ()] 'Solution of shear wall location in multistory building'. S Anshuman , Bhavin Dipendu
 Bhunia , Ramjiyani . International journal of civil and structural engineering 2011. 4 (5) p. .
- [Mo ()] 'the seismic response of multistory reinforced concrete framed shear walls using a nonlinear model'. Jost
 Mo . Structure Engineering 1993. 15 p. .