

# Source Localization of Low Frequency Oscillations in Power Systems and Methods of Damping

Klimova Tatiana

*Received: 13 December 2016 Accepted: 3 January 2017 Published: 15 January 2017*

---

## Abstract

One of the urgent problems of modern power system are low frequency oscillations (hereinafter LFO) as they reduce the static and dynamic stability of power systems. Today the important task is to detection and localization of sources of LFO and means of effectively damping such vibrations. The basic characteristics of oscillation frequency and amplitude of voltage at station buses obtained using devices phazor measurement units (hereinafter, PMU). In the softwarehardware complex Real-Time Digital Simulation (RTDS) the study method for the determination sources of perturbations that give rise to low-frequency oscillations and suppression of lowfrequency oscillations.

---

**Index terms**— low-frequency oscillations, periodic perturbations, phazor measurement units, automatic regulator of excitation, methods of damping.

Abstract—One of the urgent problems of modern power system are low frequency oscillations (hereinafter LFO) as they reduce the static and dynamic stability of power systems. Today the important task is to detection and localization of sources of LFO and means of effectively damping such vibrations.

The basic characteristics of oscillation frequency and amplitude of voltage at station buses obtained using devices phazor measurement units (hereinafter, PMU). In the softwarehardware complex Real-Time Digital Simulation (RTDS) the study method for the determination sources of perturbations that give rise to low-frequency oscillations and suppression of low-frequency oscillations.

On the basis of measurements obtained using the established in different parts of the power system, PMU for different types of periodic perturbations defined characteristics of oscillations, indicating the location of source of low frequency oscillations. Reviewed and verified way of reducing the influence of LFO on operation of generator. This regularity allows to obtain information about the location of source periodic perturbation, leading to the emergence of LFO on the grid. Further work aimed at creation of algorithm fast detection source LFO based on vector measurements, and research methods reduce the influence of LFO on synchronous generator will help determine the optimal setting of the automatic regulator of excitation for maximum damping occurs in the LFO power system.

## 1 Keywords:

low-frequency oscillations, periodic perturbations, phazor measurement units, automatic regulator of excitation, methods of damping.

## 2 I. INTRODUCTION

urrently, the issue LFO is given attention throughout the progressive world. Already significant progress has been made in identifying the reasons for LFO. The analysis of the influence of periodic disturbances on occurrence of low frequency oscillations in power system, which proves the existence of direct relationship between the periodic variations of load and periodic fluctuations in operating parameters in the power system, as well as strengthening the existing fluctuations in system at resonance with oscillation of load.

Today, an important challenge remains determination location source of the perturbations that give rise to LFO in the power system, and developing effective ways of minimizing the impact of LFO on the work of rotating machines [1].

### 4 III. THE CONSTRUCTION VECTOR DIAGRAMS OF FLUCTUATIONS IN THE OPERATING PARAMETERS WHEN THE EXTERNAL PERIODIC PERTURBATION LOAD

45 Also one of the main causes of low-frequency oscillation is inefficient excitation systems and automatic  
46 regulators of excitation. Therefore, an important task is to study the influence of the structure and parameters  
47 of automatic excitation controllers on oscillatory processes arising due to disturbances of different kinds.

48 In modern conditions in the systems collecting and information transfer widespread digital technology based  
49 on the synchronized vector measurements, which allow to obtain high accuracy and measurement stability, the  
50 lowest latency of the measured variables and increase reliability of the measuring system as a whole [2]. Phasor  
51 measurement unit (hereinafter, PMU) -a device (or software-implemented function) that measures complex values  
52 of current and voltage. Measurement from a PMU is synchronized in time based on the signals of GLONASS  
53 or GPS, which are transmitted to determine the exact location and time synchronization accuracy is  $\pm 0.2$   
54 microseconds. PMU are located in the nodes of the grid form a wide area measurement system (WAMS) [3].

### 3 II. IDENTIFICATION OF DANGEROUS RESONANT FREQUENCIES

57 In the software-hardware complex real-time digital simulator (hereinafter, RTDS) studies have been conducted  
58 method of determining the points application of the perturbations that give rise to LFO. RTDS allows to set  
59 model PMU in any given test points diagrams energy district and to sync them according to signals a single time.

60 As one of the perturbation is used periodically varying load, mounted at various points on the system. This  
61 external perturbation for all synchronous generators of the power system. Another type of perturbation mechanical  
62 moment on a shaft of one of the generators. It will be an internal perturbation for generator, and for the rest-  
63 external [2][3].

64 Disturbance of any kind cause fluctuations in the frequency and amplitude of voltage at all points of the  
65 system. In the network map was implemented the point of application of a periodic load  $P_{n1}$ ,  $P_{n2} = \text{var}$ , and  
66 changes in the moment generator shaft is  $T_m = \text{var}$ . The place of installation, PMU designated in figures 1-13  
67 in Fig. ?? Fig. ??: The test grid and oscilloscope record frequency variations in the place of installation PMU  
68 (the model created in RTDS)

69 By studying the spectral composition and operating parameters have been selected the two most pronounced  
70 dangerous (resonant) frequency of oscillations periodic disturbances [4], which correspond to values of 0.47 Hz  
71 and 0.74 Hz, which is almost the same for all operating parameters.

### 4 III. THE CONSTRUCTION VECTOR DIAGRAMS OF FLUCTUATIONS IN THE OPERATING PARAMETERS WHEN THE EXTERNAL PERIODIC PERTURBATION LOAD

76 Study of the effect periodic load was carried out with the change in oscillation frequency of load in the range  
77 0.4-0.9, is necessarily encompassing both resonant frequencies. For periodic load change  $dP_{n1}$  in the most typical  
78 (close to resonance) frequencies of 0.7 Hz and 0.4 Hz in different parts of the system (for a frequency of 0.7 Hz  
79 the results are shown in Fig. 2) the obtained waveforms show that the phase shift and the amplitude of the  
80 oscillation frequency voltage (Fig. 2, a) and voltage amplitude (Fig. 2, c) depends on the measurement points  
81 the modal parameters (the place of installation, PMU) When using a visual geometric method of representation  
82 harmonic oscillations, namely, their image as vectors in the complex plane [5], are shown the vector fluctuations  
83 of operating parameters at different points installation, PMU. The horizontal axis represents the frequency of  
84 oscillation settings and the vertical attenuation constant (parameters of roots of the equation of free motion).  
85 The length of vector is proportional to amplitude of the corresponding modal parameters, and its phase equal to  
86 the phase oscillations relative to signal sync. Each vector (Fig. 2, b, d) starts at the point of 0.7 Hz, a value of  
87 zero damping constant, since the amplitude of sine wave oscillations operating parameters constant.

88 Device, PMU 3 is set almost at the point of disturbance. In this case, the phase of the oscillation frequency  
89 at point 3 the minimum relative to reference point (1PPS signal), and its amplitude is maximum. The vector  
90 of this oscillation (see Fig. 2, b) -basic, next to it the vectors, shown as a dotted line, is built on the basis of  
91 measurements in area closest to point of application perturbation. Among the vectors oscillation amplitude of  
92 the voltage (see Fig. 2, d), the oscillation amplitude, measured at the point 3, is maximum, but the phase of this  
93 vector is significantly different from minimum.

94 Therefore, only the phase vectors of the oscillation frequency of the voltage measured at different points power  
95 system, uniquely identifies a source location LFO. Phase vectors of the oscillation frequency of voltage measured,  
96 PMU, are minimum where the measurements were performed close to source of perturbation. The module vector  
97 of oscillation frequency depends on the degree of coincidence of frequencies LFO and the resonance frequency in  
98 the considered point of grid and shows the sensitivity of object to fluctuations considered frequency.

---

## 5 IV. STUDY OF THE WAYS TO MINIMIZE IMPACT OF LFO IN POWER SYSTEM ON SYNCHRONOUS GENERATOR

Identified in the previous Chapter the pattern allows through synchronized vector measurements to obtain information about location of source periodic perturbation, leading to the emergence of LFO in grid. Considering all the operating parameters of low-frequency fluctuations and fine tuning of automatic excitation regulators (AEC) generators at stations located near the source of the LFO, which would improve the damping performance of AECs and reduce the probability of violations parallel operation of power plants and grids, the occurrence of asynchronous mode and cascade development process disturbances [6].

In a hardware-software complex of RTDS were studied and proven method of reducing the effects of the various LFO on the performance of synchronous generator.

The first method is the change in the prescribed setpoint voltage of the AEC on the generators of the power plant, located closest to the source of the LFO. To study the simulated real network with multiple parallel links. PMU were placed. Fig. 3 shows part of the studied schemes. Shows diagrams that contain PMU caught in this part, provided their numbers. After an outage of line (X marks in Fig. 3), is an increase in flow in said line, until it exceeds the maximum value.

Using the identified patterns, and analysing data with PMU determined that PMU installed at the point 12 (Fig. 3) shows the minimum phase of the oscillation frequency of the voltage (Fig. 4), which indicates a location closest to the source of the disturbance.

Fig. 4 shows the transition of the local fluctuations (Fig. 4,b) arising out of the disconnection of the line, zonal continuous. Fig. 3 ovals marked stations having the same type of zonal oscillation that is manifested in the waveform in Fig. 4,a. The second way is to change the schema of the AEC. Analysis of oscillation in all nodes of the grid after setting the AEC, the station closest to the source of an LFO will allow for the synchronized vector measurement gauges to assess the impact of the settings of AES on fluctuations in the working parameters of all the given points of the power system Change the structure and parameters of AEC, located near a permanent source of vibrations. The scheme upgraded the device ARV is shown in Fig. 6. Overbuild the part is highlighted and presented on the same figure. 6. The main design feature of this AE? is the summation of the output signal dUp1 with amplitudemodulated and frequency of voltage signal dUp, the main amplitude and frequency of which correspond to parameters of low-frequency oscillations. In addition, the frequency of the b phase modulated oscillations are so chosen that they are the opposite of own oscillations of the generator. It should be noted that implementation's AECs have been used only at node 2 (Fig. ??), the oscillation frequency at this point is a maximum.

When comparing the waveforms of oscillation frequency in Fig. 7 observed in different points, you can see that the modified AE?s has a positive effect on damping of oscillations not only at the station but in whole energy area.

## 6 V. CONCLUSION

This regularity allows to obtain information about location of source periodic perturbation, leading to the emergence of LFO on the grid. Further work are aimed at creation of algorithm of fast detection source of LFO on the basis of vector measurement.

Research methods reduce the influence of LFO on synchronous generator will help determine the optimal setting automatic regulator of excitation for maximum damping LFO has occurring in the power system. Also it is possible to develop adaptivecustomizable automatic excitation regulators depending on the parameters of low frequency oscillations in power system. <sup>1 2 3 4 5</sup>

---

<sup>1</sup>© 2017 Global Journals Inc. (US)Global Journal of Researches in Engineering

<sup>2</sup>Year 2017 F Source Localization of Low Frequency Oscillations in Power Systems and Methods of Damping

<sup>3</sup>© 2017 Global Journals Inc. (US)

<sup>4</sup>Year 2017 F Source Localization of Low Frequency Oscillations in Power Systems and Methods of Damping

<sup>5</sup>Year 2017 F

## 6 V. CONCLUSION

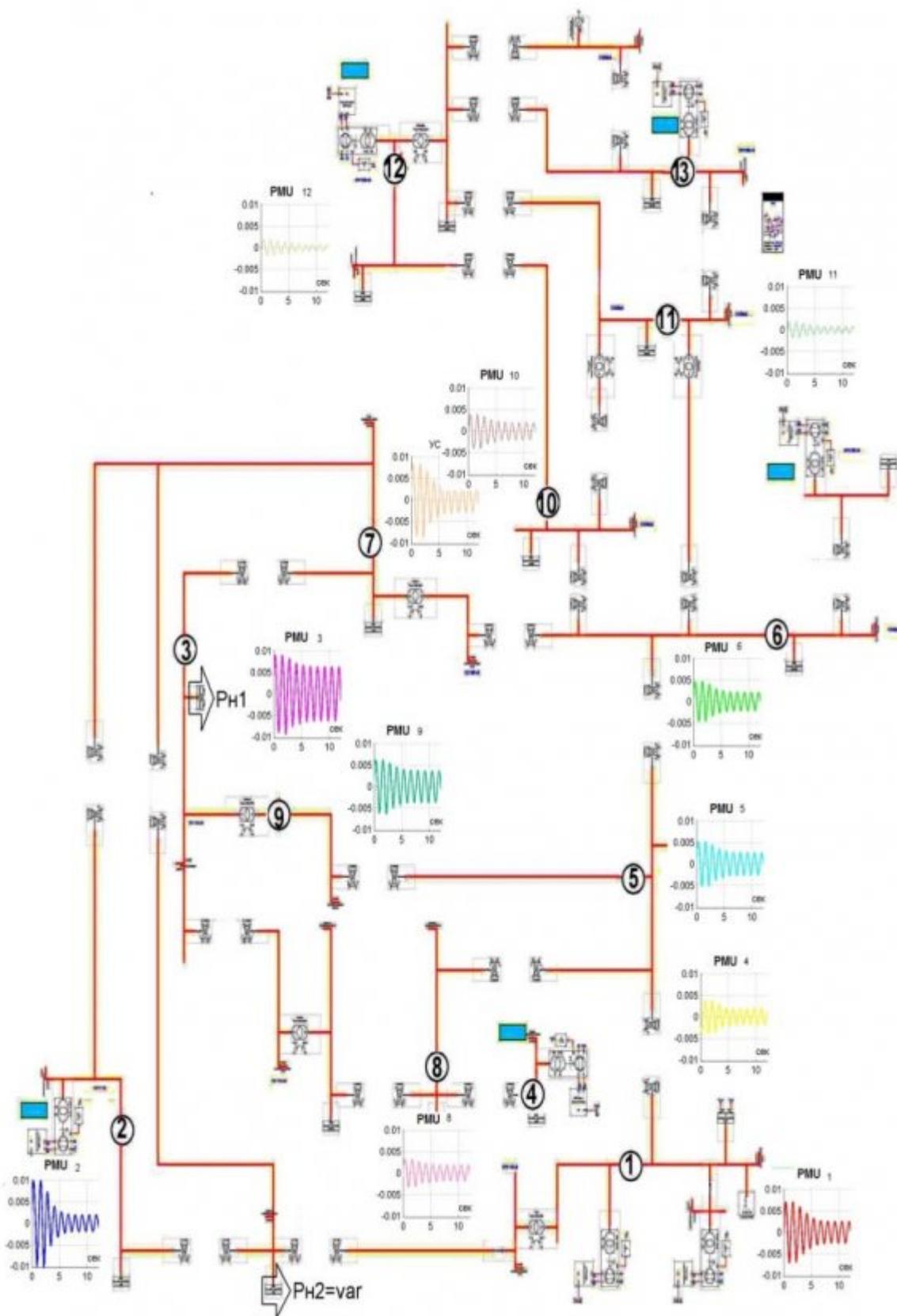
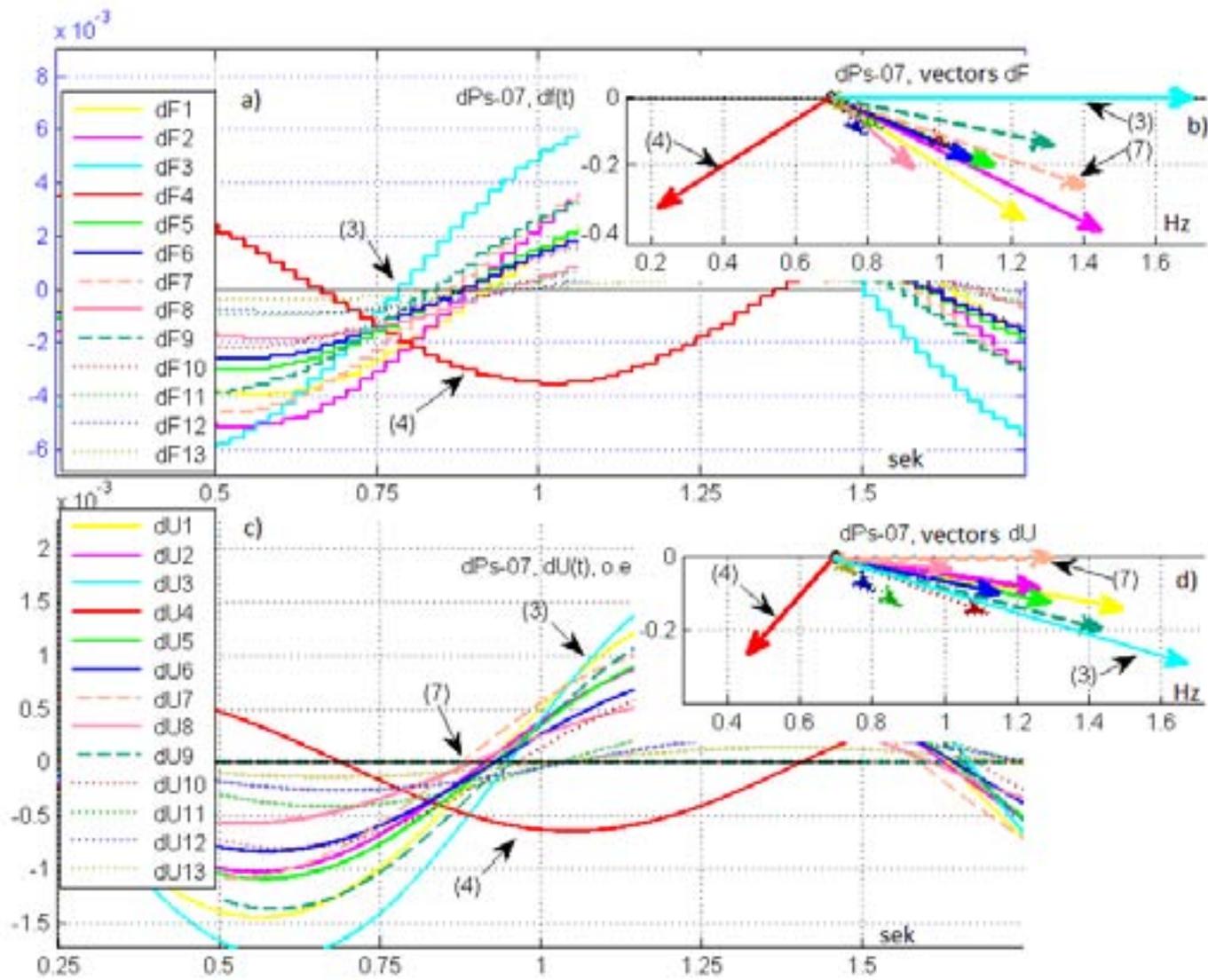


Figure 1: Source



2

Figure 2: Fig. 2 :

## 6 V. CONCLUSION

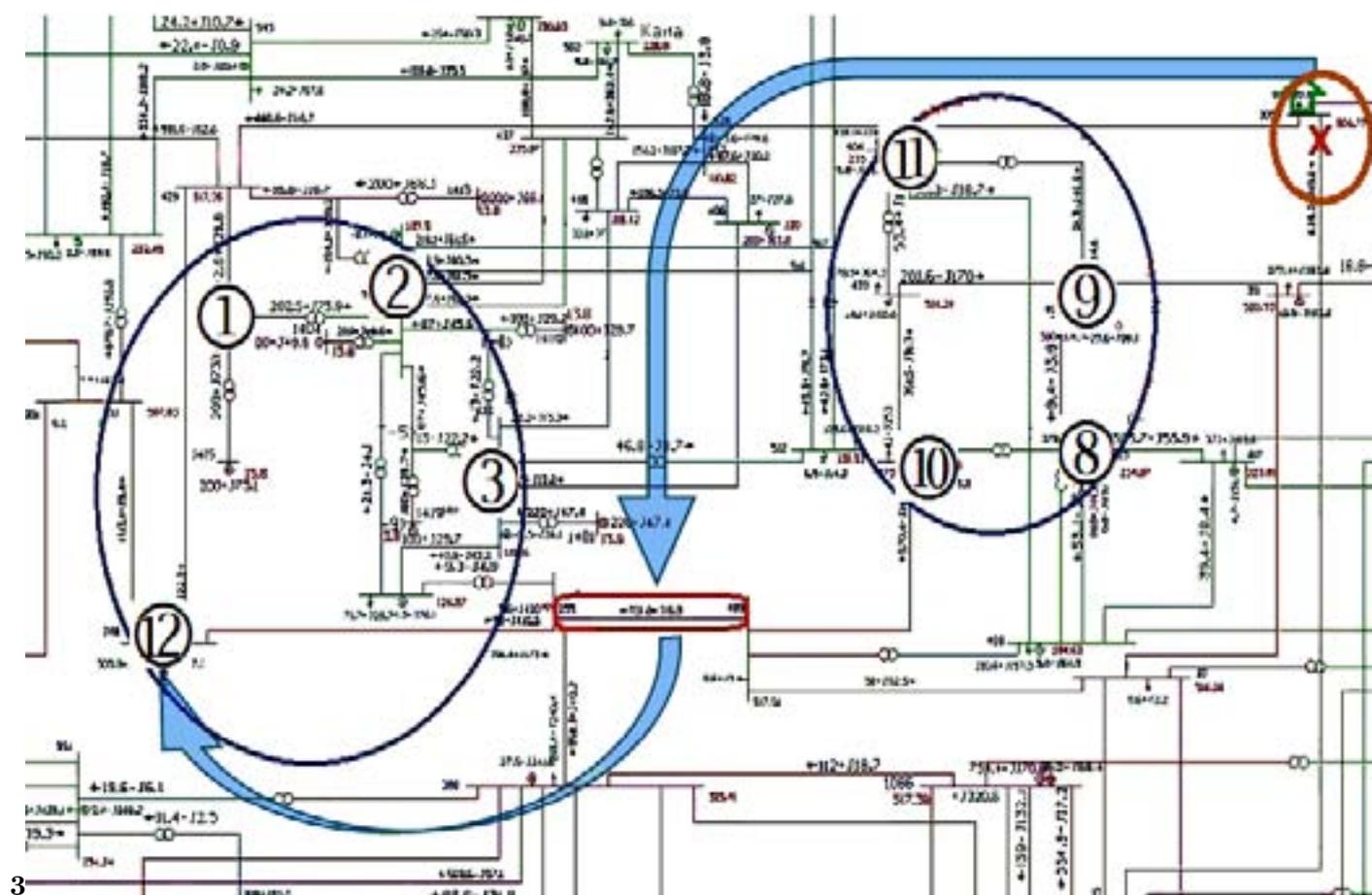
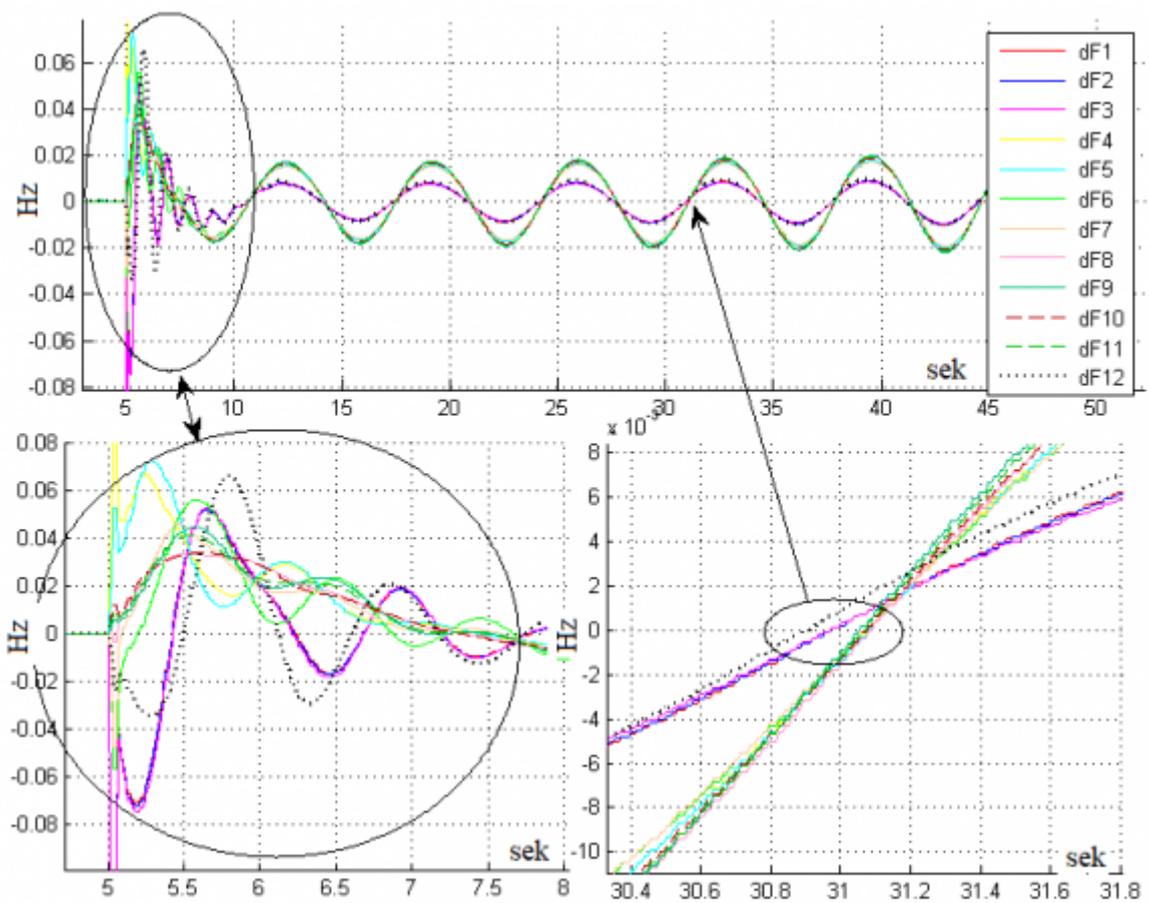


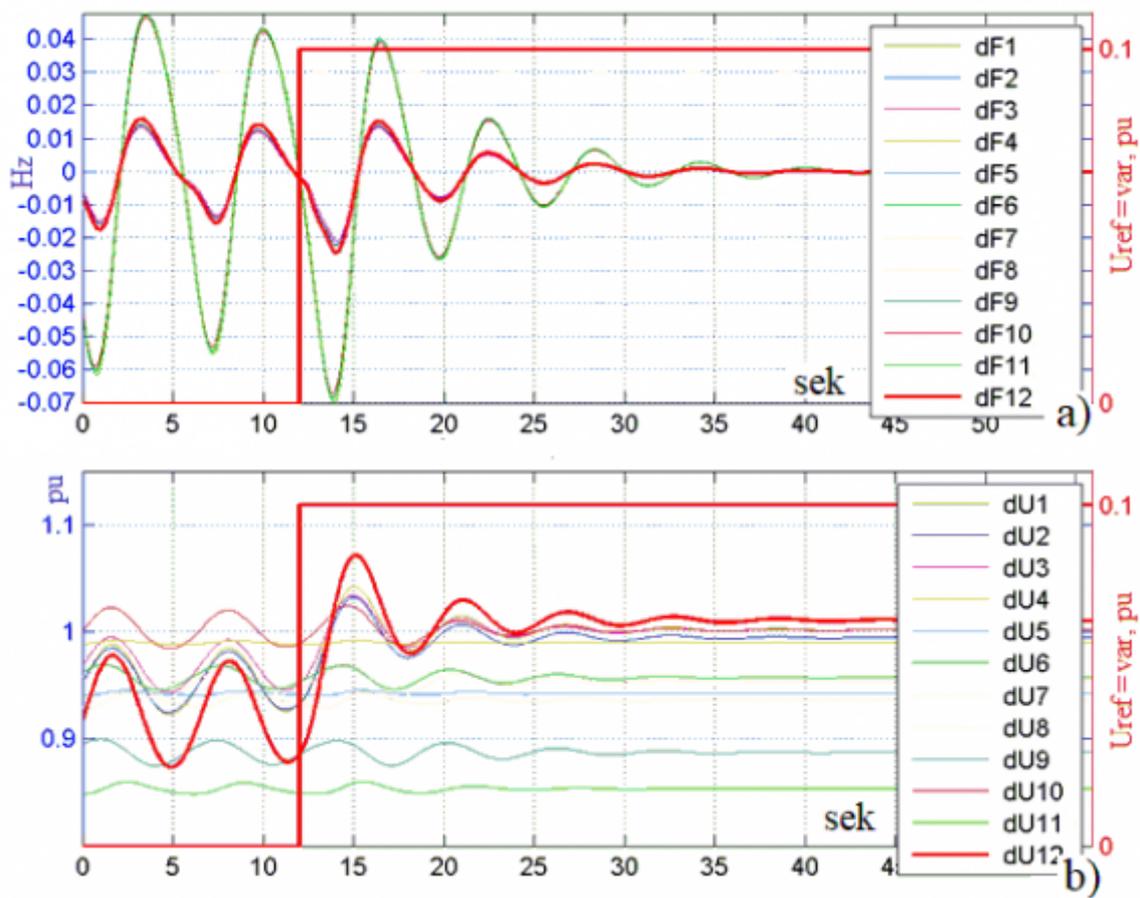
Figure 3: Fig. 3 :



4

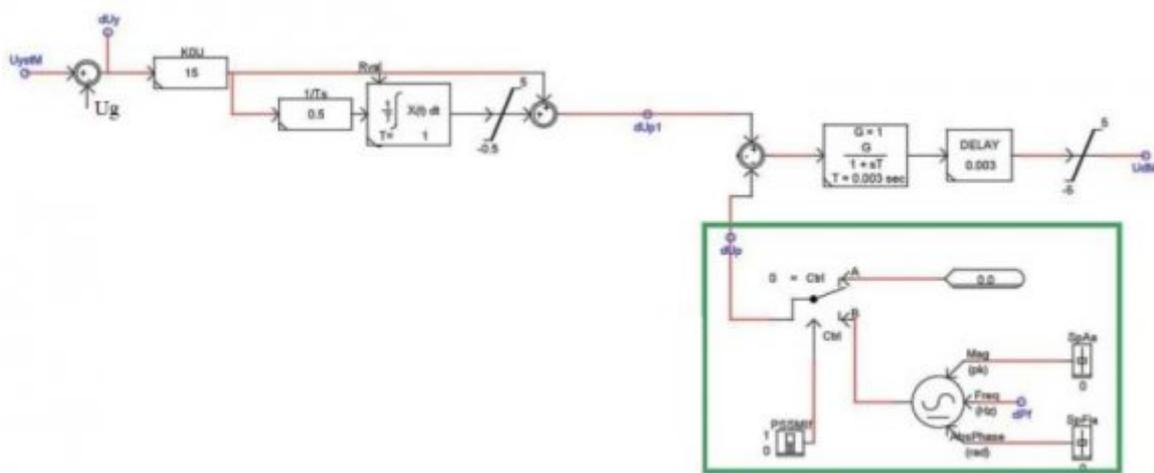
Figure 4: Fig. 4 :

6 V. CONCLUSION



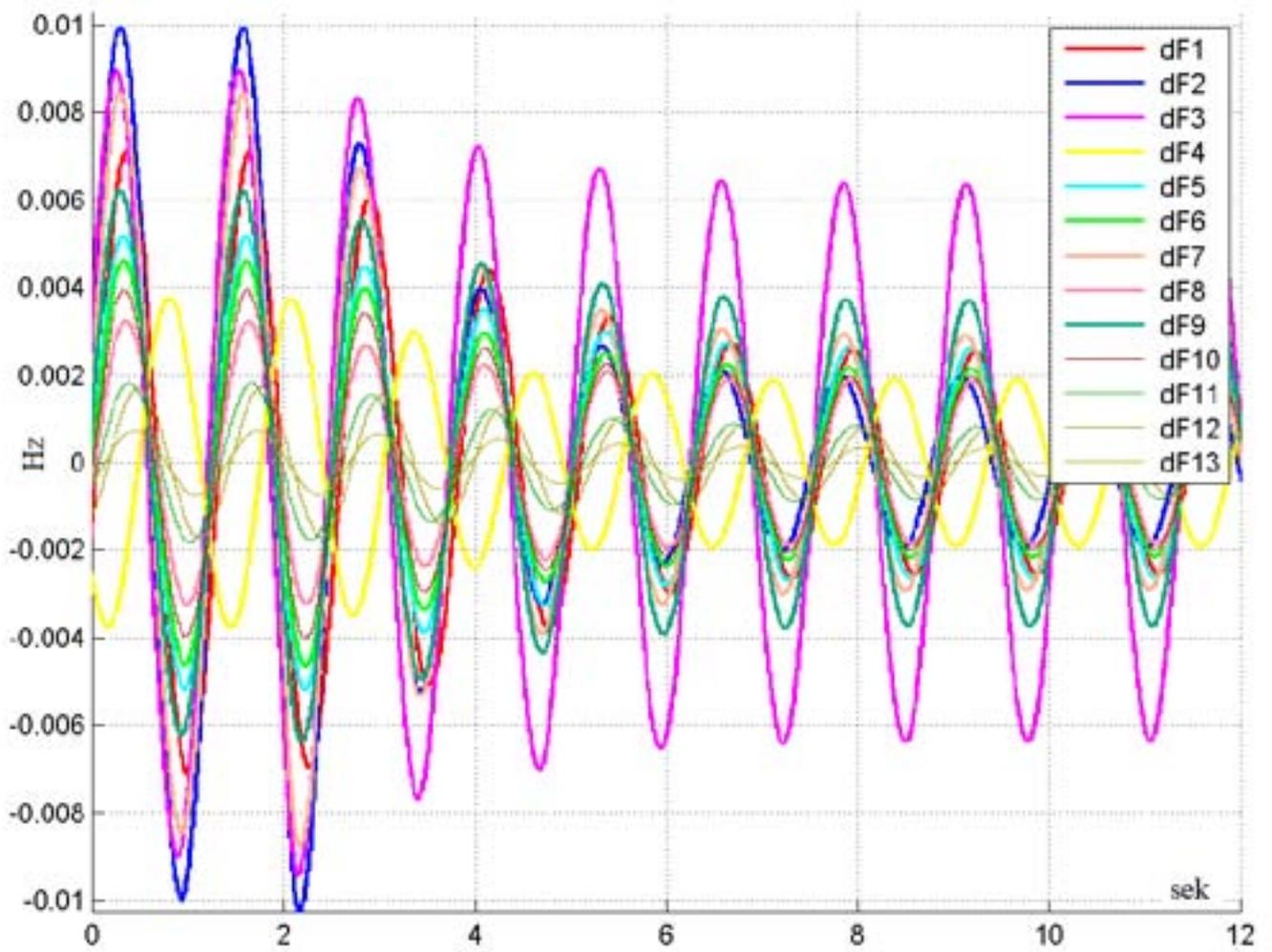
5

Figure 5: Fig. 5 :



6

Figure 6: Fig. 6 :



7

Figure 7: Fig. 7

## 6 V. CONCLUSION

---

- 
- 142 [Klimova and Savvatin ()] ‘Analiz vlijanija periodicheski menjajushhejsja nagruzki na vznikovenie nizkoclas-  
143 totnyh kolebanij [The analysis estimates periodically changing load on the occurrence of low-frequency  
144 oscillations]. T G Klimova , M V Savvatin . *Sbornik dokladov Mezhdunarodnoy nauchno-tehnicheskoy*  
145 *konferencii SIGRE "Sovremennye napravleniya razvitiya system releynoy zashchity i avtomatiki energosistem,*  
146 (Sochi) 2015.
- 147 [Xiao et al. ()] ‘Dynamic Tracking of Lowfrequency Oscillations with Improved Prony Method in Wide-Area  
148 Measurement System’. J Xiao , J Han , J Wu . *IEEE Power Meeting* 2004. Denver.
- 149 [Ja et al. ()] *Predstavlenie perehodnyh processov jelektroenergeticheskikh sistem na giperploskosti s dvumja*  
150 *sistemami koordinat // Jelektrichestvo, Arcishevskij L Ja , T G Klimova , A I Rasshepljaev . 2011. 4.*
- 151 [Task Force on Identification of Electromechanical Modes, Identification of Electromechanical Modes in Power Systems ()]  
152 *Task Force on Identification of Electromechanical Modes, Identification of Electromechanical Modes in Power*  
153 *Systems*, 2012. IEEE Task Force (Report)
- 154 [Sorokin] *Vybor nastroek ARV generatorov slozhnoj jenergosistemy na osnove primenenija geneticheskogo*  
155 *algoritma i metodov modal'nogo analiza, D V Sorokin . (The choice of settings ARV generators of complex*  
156 *energy systems based on the use of genetic algorithm and modal analysis methods. Dis.kand. tehn. nauk:*  
157 *05.14.02.D.V. Sorokin; SPbGPU)*