

Dynamic Fracture Process during Three-Point-Bending Impact on Polymethyl-Methacrylate Beams

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Abstract

Dynamic fracture process in polymethyl-methacrylate (PMMA) beams have been investigated during the three-point- bending impact tests at different impact velocities, conducted in a drop-weight impact tower instrument. The impact-induced crack initiation and propagation have been recorded with a high- speed camera, to determine the instantaneous fracture length and crack velocity during impact process. The beam deformation and displacement fields were extracted and analyzed by using the digital image correlation (DIC) technique during the impact. The impact loading history has been recorded with a load cell attached to the dropping weight. The whole experimental study is a suitable technique to determine the influence of the impact velocities (impact energy) on the dynamic fracture initiation and propagation at different crack speeds.

Index terms— PMMA; three-point-bending impact; dynamic fracture; crack velocity, DIC.

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Abstract-Dynamic fracture process in polymethyl-methacrylate (PMMA) beams have been investigated during the three-point bending impact tests at different impact velocities, conducted in a drop-weight impact tower instrument. The impact-induced crack initiation and propagation have been recorded with a high-speed camera, to determine the instantaneous fracture length and crack velocity during impact process. The beam deformation and displacement fields were extracted and analyzed by using the digital image correlation (DIC) technique during the impact. The impact loading history has been recorded with a load cell attached to the dropping weight. The whole experimental study is a suitable technique to determine the influence of the impact velocities (impact energy) on the dynamic fracture initiation and propagation at different crack speeds.

Fracture in PMMA have also been studied. Takahashi [6] investigated multiple dynamic fracture parameters such as the dynamic stress intensity at the crack tip as well as crack velocity and acceleration. They analyzed the initiation and propagation behavior of the crack of thin PMMA sheet under tensile load. Lataillade [7] studied the mechanical behavior of PMMA under various loading rates as well as the properties of the polymer at high rates of strain. Their research identified the relationship between Young's modulus, yield stress and fracture toughness of PMMA and tensile loading rates. On the other hand, Loya [8] performed quasi-static three-point bending test on PMMA beams and recorded the crack-front propagation process throughout the specimen thickness. The crack length and the average steady crack propagation were extracted and studied. In a more recent study, Huang [9] adopted a different technique, dynamic semicircular bend testing, and performed fracture testing on PMMA specimen with split Hopkinson pressure bar. Their study determined the fracture velocity under different loading rates as well as surface fracture toughness and its relationship with fracture energy.

However, the impact-induced dynamic fracture process in PMMA with precise record of crack propagation and speed has rarely been studied before, especially the fracture caused by impact with different velocities. In the former studies, the recording time step period is relatively long. For example, only the average crack velocity

44 for the whole fracture can be obtained. To better understand more detail dynamic fracture process, including
45 the beam deformation and crack propagation, the more precise experimental investigation in more precise time
46 steps is essential.

47 In this paper, the impact-induced dynamic fracture process in PMMA beams has been investigated. The
48 experiment was conducted with a drop-weight tower instruments. During the impact test, the impact loading
49 history has been recorded by a load cell attached to the bottom of the dropping weight. The impact process was
50 recorded with a high-speed camera at the time resolution of about 15 microseconds. The impact-induced crack
51 initiation and propagation have been extracted from the images recorded with the high-speed camera, to determine
52 the instantaneous fracture length and crack velocity during I. Introduction dynamic fracture in structural materials
53 is a significant issue because it concerns the failure of structural materials in their dynamic service. Impact is one
54 of the most common dynamic loading forms but complicated since the material properties and failure behaviors
55 are complex in dynamic situation. The dynamic fracture problems have been studied experimentally [1][2][3]
56 and numerically [4,5]. Joudon [1] studied the dynamic stress intensity factor by using a strain gauge method
57 associated with high speed cinematography on a three-point-bending test with specimens made of M21 epoxy
58 resins. Cramer [2] conducted dynamic fracture experiments using boron-doped silicon single crystals followed
59 by cleavage fracture with the propagation of a faceted crack front with amorphous materials. Owen [3] studied
60 the critical dynamic stress over a range of loading rates of 2024-T3 aluminum sheets ranging in thickness from
61 1.63-2.54 mm. The dynamic fracture process in three-point-bending beams made with isotropic polymer [4] and
62 orthotropic composite materials [5] have been numerically simulated with peridynamics.

63 2 D Figure 1: Drop weight impact experimental setup

64 The experiment was conducted by performing a three-point-bending impact test on a single-edged notched PMMA
65 specimen by using a drop-weight impact tower as shown in Fig. ?? The dropping weight was located above the
66 PMMA sample and set free to drop onto the sample surface. Three impact velocities (1, 2, and 3 m/s) were
67 achieved by dropping the weight from three different heights. To monitor the force applied during the experiment,
68 a load cell was attached to the bottom of the dropping weight, which is used to record the loading signals during
69 the impact process. The signals from the load cell then can be amplified by an amplifier, then displayed and
70 recorded with an electronic oscilloscope provided by National Instruments. A high-speed camera was placed
71 perpendicular to the vertical surface of the specimen to record the video of the impact process, which can be
72 used to extract the crack propagation details and the corresponding displacement fields at different time steps.

73 The sample beam is made with PMMA (purchased from McMaster-Carr) with the length of 140mm, the width
74 of 38mm, and height of 25.4mm. A notch of 16mm was initially made in the center of the bottom edge of the
75 plate as shown in Fig. 2. The DIC method is an optical method of experimental mechanics that can be used to
76 measure and calculate the displacement, deformation, and strain field of the objective samples during mechanical
77 testing [10][11][12]. White background painting with evenly located black speckles painting was sprayed on the
78 surface of the samples for the DIC testing.

79 3 II. Experimental

80 distances between each speckle can be determined by the suggestions in [13]. A fully prepared specimen surface was
81 shown in Fig. 3. The camera was set to focus on the crack propagation region on the specimen. The resolution of
82 the camera was 256 x 256 pixels, which correlated to the square area at the center of the specimen. A sequence of
83 images were extracted from the video with time incremental of 5 milliseconds. The images were then inputted into
84 software GOM correlate for displacement field and crack propagation analysis. To analyze the images of impact
85 process with GOM correlate software, a surface component was created at first. Emphasizing on the granularity
86 of the sample, a surface component of 37 pixels was chosen, with a point distance of 18 pixels. The area of
87 interest was also selected by using the Select/Deselect Polygon tool to include the crack propagation region. The
88 original notch tip and the crack tip at each time step can be located in the images with GOM, the absolute crack
89 propagation distances can then be directly extracted with GOM

90 4 III. Results and Discussions a) Impact force on PMMA beam

91 The impact loadings were extracted from the signals recorded with the load cell. The loading record resolution
92 was set as 10⁷s. The force histories of impact processes with different impact velocities are presented in Fig. ?? In
93 the figure, the impact force history at different impact velocities as $v=1, 2, 3$ m/s are presented separately with
94 different marked curves. For impact with different velocities, similarly, the force curves initiate from zero once
95 the impactor (load cell) contact the top surface of the sample, and rise till the maximum values. The force then
96 drops suddenly till even negative values, which indicate the load cell recording of the reflection of the impact
97 stress wave. However, the peak values of the impact force at different velocities are different. The peak force for
98 impact at 3 m/s is the largest and 1 m/s the lowest. The crack initiates at the time of the peak impact force and
99 propagates till the fracture, as shown in Fig. 5, Fig. ??, and Fig. ??.

5 Figure 4: Force history of impact processes with different impact velocities b) Impact fracture process

The impact fracture process in PMMA beam with the corresponding displacement fields have been presented in Fig. 5, Fig. ??, and Fig. ??, with the impact velocities at 1 m/s, 2 m/s, and 3 m/s respectively. In Fig. 5, the fracture initiates at 630 μ s after the dropping weight contacts the top surface of the PMMA beam, which means the loading time is 630 μ s till the crack initiate from the tip of the original notch. The crack propagations from the initiation at 630 μ s, to 690 μ s, till 780 μ s are presented in Fig. 5, with the crack tip marked with the white arrows. During the fracture process, as the crack length increases, both the displacements in x and y directions increase correspondingly. The detail displacement field contour can be found in Fig. 5 with the specific color bar. Displacements fields are symmetric to the vertical line of the original notch. The change of the color in the displacement contour indicates the deformation process of the beam during the impact process, which lasts as short as round 150 μ s. Once the dropping weight reaches the top surface of the beam, the beam is subjected to an impact loading and starts to bend due to the simply supported boundary conditions at the bottom surface. During the impact bending process, the tensile stress concentration increases at the tip of the original notch. The crack initiates to propagate once the stress intensity factor reaches the critical value (fracture toughness).

Fig. ?? shows the fracture process in PMMA beam with the impact at a velocity of 2 m/s. The fracture initiates at 285 μ s after the dropping weight contacts the top surface of the PMMA beam. During that time, the dropping weight subject impact loading at the middle of the top surface of the beam, which causes the beam bending with the increase of the stress concentration at the crack top. The crack propagations from the initiation at 285 μ s, to 345 μ s, till 435 μ s, with the crack tip marked with the white arrows in Fig. ?. Similar to the impact at a velocity of 1 m/s, during the fracture process, as the crack length increases, both displacements in x and y directions increase correspondingly. The detail displacement field contour with color bar can be found in Fig. ?. Displacements fields are also symmetric to the vertical line of the original notch. The change of the color in the displacement contour indicates the deformation process of the beam during the impact process, which lasts during the time period as short as about 150 μ s. The crack initiation and propagation length history in PMMA beams subjected to impact at different impact velocities are shown in Fig. 8. During the impact process, the time step when the dropping weight contacts the surface of the beam is set as 0. The crack initiation time for PMMA beam subjected to impact at velocities of 1 m/s, 2 m/s, and 3 m/s are 635 μ s, to 265 μ s, and 110 μ s, respectively. Obviously, the loading time before the crack initiates is much longer for higher impact velocity, shorter for lower impact velocity. The cracks propagate till 20 mm within about 150 μ s, but with a different slope of the length curves, which means the crack velocities are different, as shown in Fig. 8. The crack propagation speeds after crack initiation in PMMA beams subjected to impact with different impact velocities are shown in Fig. 9, in which the time is set as 0 at the crack initiation point. The crack velocities in beams subjected to different impact loading have the similar trend. Crack velocities start from a relatively low value round 100 m/s, then rise to the peak value round 200 m/s, and decrease till the fracture. The peak crack velocities for fracture in beams subjected to different impact are different. For fracture in the beam under the impact of 3 m/s, the peak crack velocity is highest as 212 m/s. The peak crack velocities in the beam under the impact of 2 m/s and 1 m/s are lower as 195 m/s and 189 m/s respectively.

6 IV. Conclusion

The impact-induced dynamic fracture initiation and propagation in single-edge-notched PMMA beams have been analyzed in this paper. Crack initiates later after the contact of impact when it is subjected to smaller impact velocity. During the dynamic fracture process, crack velocities rise from a lower value, then reach the peak value, and then decrease till fracture. Peak velocity of the fracture in beam subjected to bigger impact loading is higher than that in the beam under smaller impact loading.

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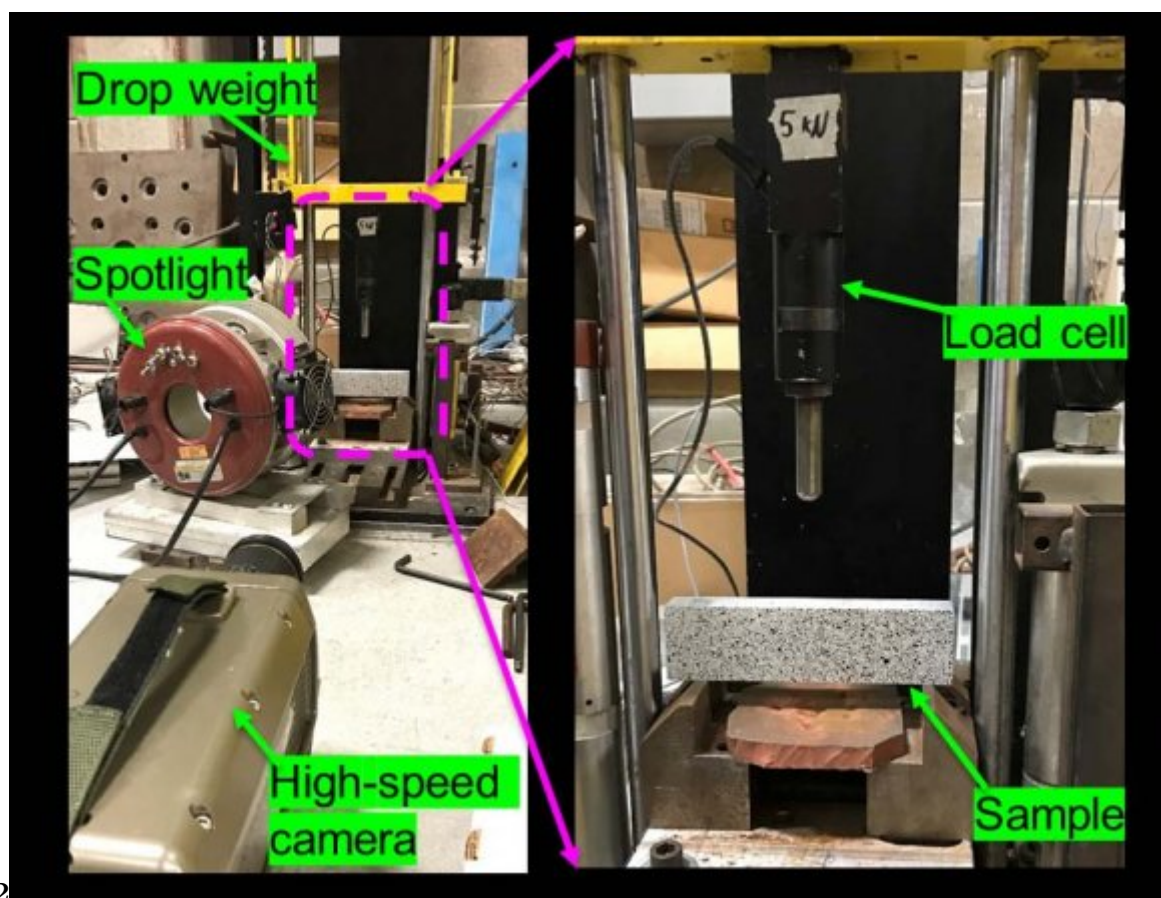


Figure 1: Figure 2 :

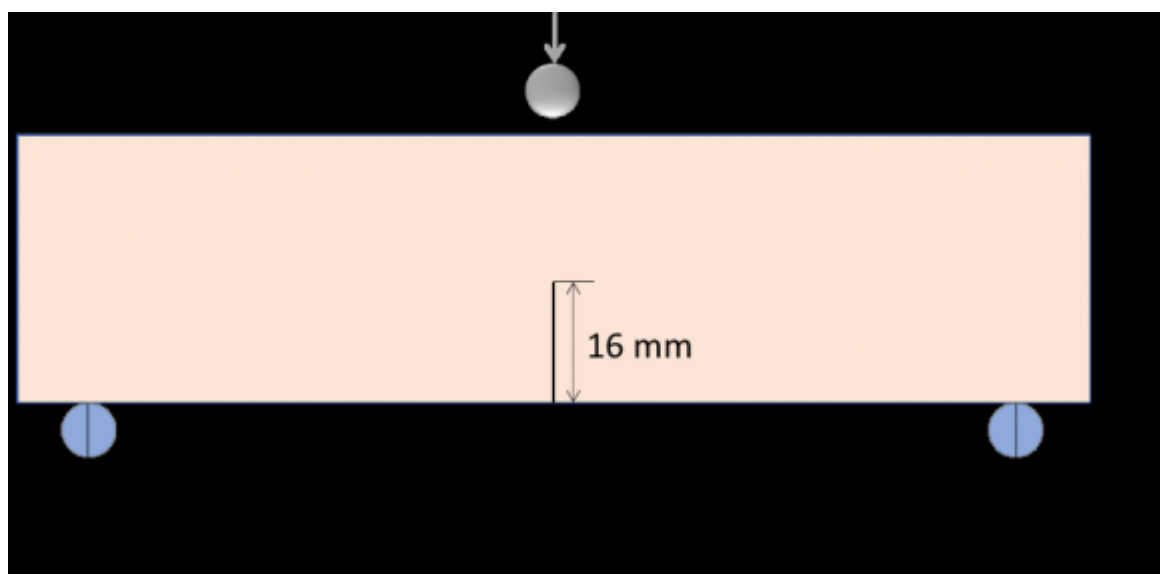
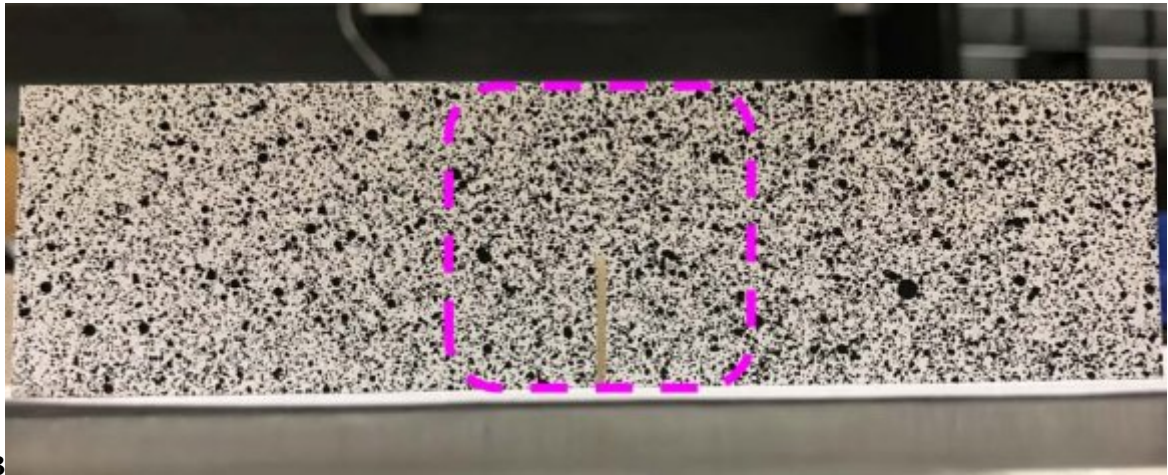
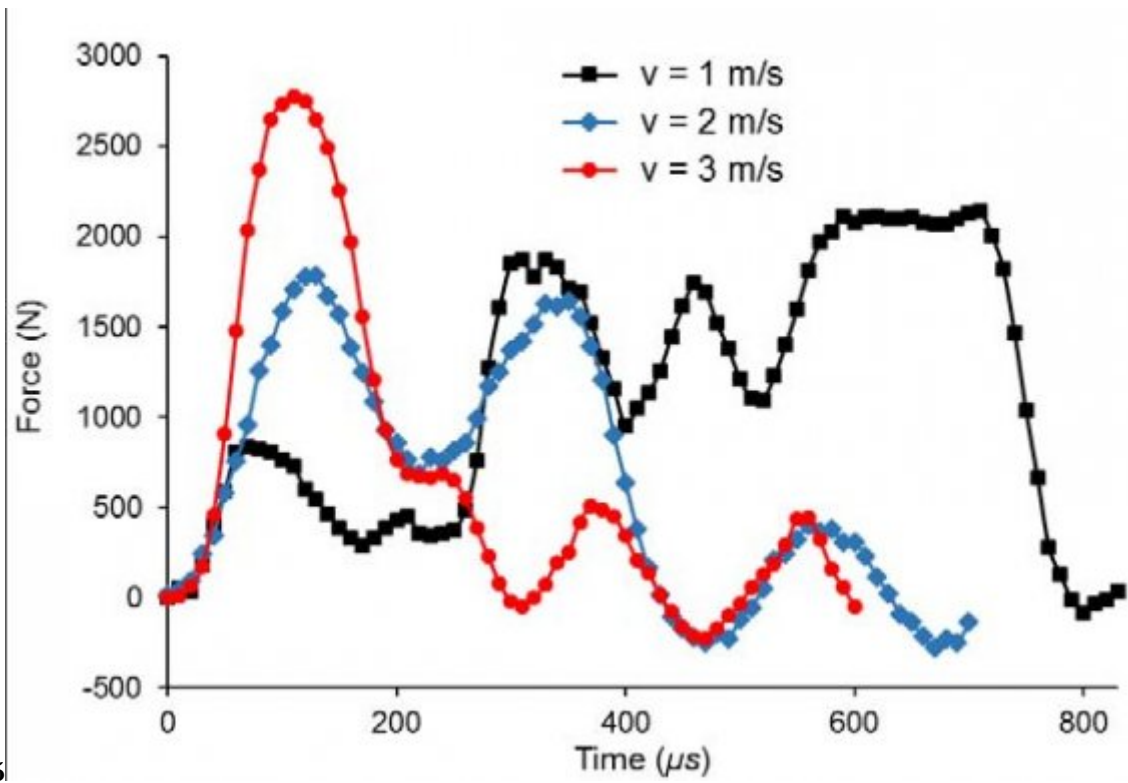


Figure 2:



3

Figure 3: Figure 3 :



5

Figure 4: Figure 5 :A

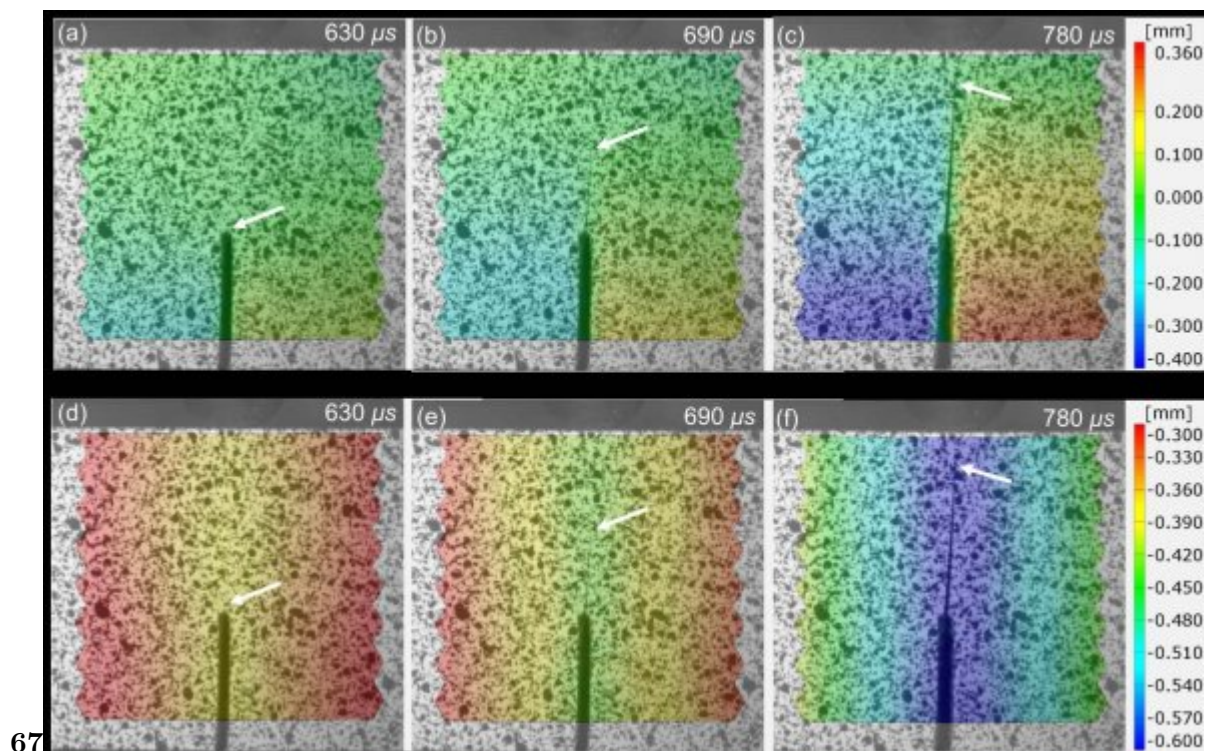


Figure 5: Figure 6 :Figure 7 :

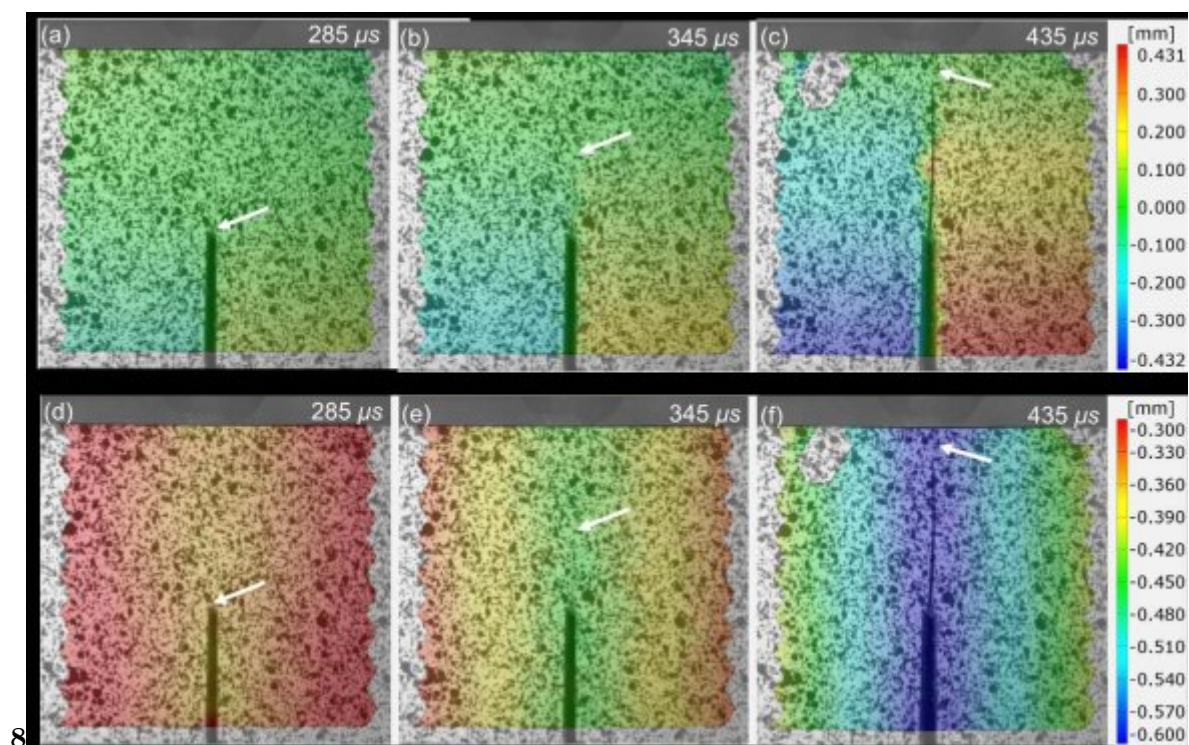
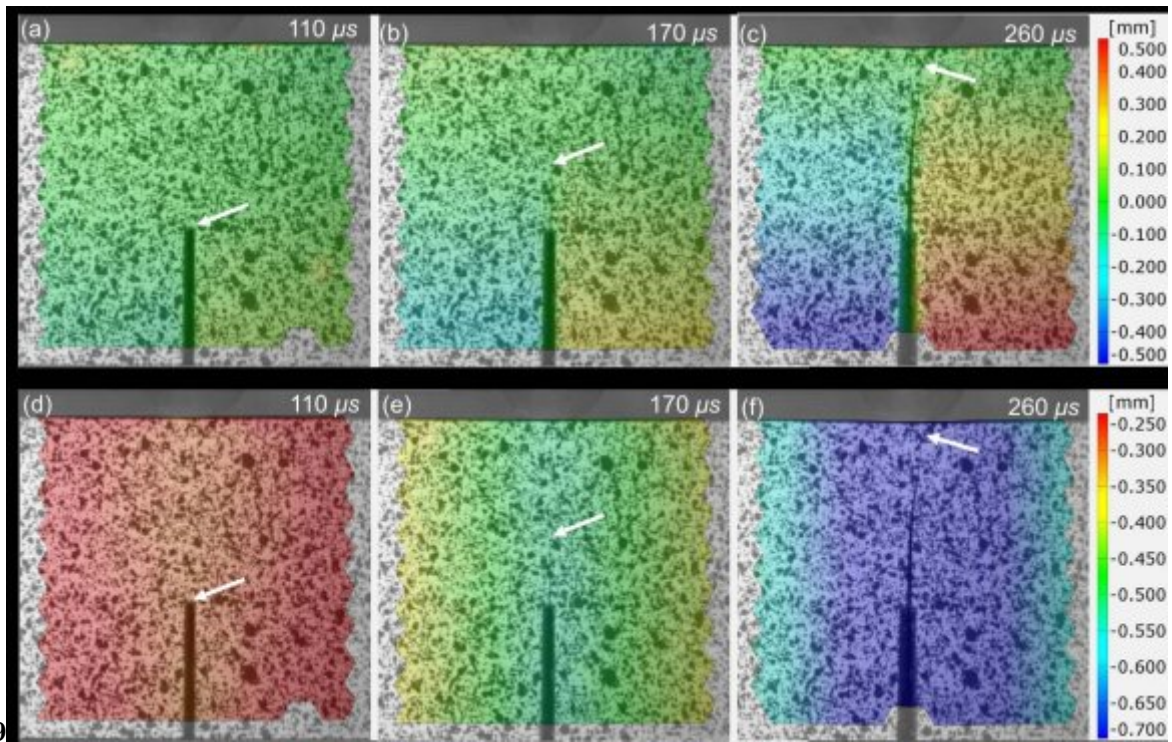


Figure 6: Figure 8 :



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Figure 7: Figure 9 :

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