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### Evaluation the Dissipated Energy by the Automobile Dampers 1

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## Abstract

Simulation of suspension system and evaluation of dissipated energy by the system highlights

- the potential of the car operation mode, where the suspension can provide a significant 8
- amount of power. A roughness road profile and a car with elastic suspension springs and stiff 9
- dampers can provide significant energy. This energy varies between 4 10

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- simulation, suspension, stiffness, damping, road profiles, dissipated energy

*Index terms*— simulation, suspension, stiffness, damping, road profiles, dissipated energy. I. Introduction haracterization of automotive suspensions, in terms of energy dissipated by the suspension 13 dampers while running, is a complex process that takes into account a number of factors, such as road profile, 14 vehicle characteristics, running speed. All these factors contribute to determining the conditions under which 15 the dampers dissipate a large amount of possible energy. In order to simulate the systems suspension operation 16 and to evaluate the dissipated energy by the system, there were considered the following parameters: 17

? road profile; ? mass parameters and general organization of the car; ? operating parameters of the 18 suspension; ? simulation conditions. 19

#### II. Road Profile 1 20

The road profile is comprised of two components: ? the road microstructure; ? the road macrostructure. 21

The road microstructure road represents the uneven humps of tread, felt by the vehicle driver as vibrations or 22 small oscillations. This is divided into four classes, depending on the variation of high road irregularities (Î?"h) 23

in relation with theoretical nominal profile, measured in mm, [1]: Depending on the mentioned macrostructures 24

parameters, there were defined eight road profiles, whose design speeds are in the range 25 km/h -120 km/h, with 25

the following characteristics: Following the conditions from the table 1, it results a sequence of road characteristics 26

used in simulation: ? ISO A-B,  $\hat{I}$ ?"h =  $\pm$ 27

#### 2 Β 28

The road profile sequences with a concave and convex radius, will be repeated until the length of road, in 29 horizontally profile, will have the value of 1 km (distance used in simulation). 30

#### 3 V. Conditions of Simulation 31

The conditions required for vehicle during the simulation are: ? simulation performed in two conditions, the 32 car's unladed weight and with total weight; ? straight displacement at a constant speed; ? all the profiles road 33

used in simulation have a length of 1 km; 34 ? the cross profile of the road is symmetrical. 35

#### 4 VI. Suspension Mathematical Model 36

Each suspension vehicle consists of: ? the suspension itself; ? the tyres. The suspension itself includes the springs, 37 the dampers and the arms of the car body. Here it was defined the suspension mass (m s ), vehicle sprung mass 38 (m 1), the suspension spring rate (k s) and the suspension damping (c s). The tire was defined as an independent 39 suspension with the same elements, spring and damper. It was considered the tire stiffness (k t) and tire damping 40

(c t ). The suspension excitation is characteristic for every road profile (X r ) and is identical between the front 41

### 4 VI. SUSPENSION MATHEMATICAL MODEL



Figure 1:



Figure 2: Figure 1 : Figure 2 :

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Figure 3: Figure 3 :



Figure 4: Figure 4 : Table 3 :



Figure 5: Figure 5 :







Figure 7: (  $2\ \mathrm{B}$ 



Figure 8: Figure 6 :



Figure 9:





1

Road	profile	speed	? [ ° ]	R convex [m]	R concav [m]
$[\mathrm{km/h}]$					
25			8	500	300
30			7,5	800	500
40			7	1000	1000
50			7	1300	1000
60			$6,\!5$	1600	1500
80			6	4500	2200
100			5	10000	3000
120			5	18000	6500

Figure 11: Table 1 :

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	4	,
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Road profile	speed	H [m]	h [m]	D [m]	d [m]
$[\rm km/h]$					
25		1.6	0.9	80	48
30		2.2	1.4	120	75
40		2.4	2.4	140	140
50		3.1	2.4	181	140
60		3.3	3.2	207	196
80		8.1	3.9	538	224
100		7.1	2.1	748	263
120		12.2	4.5	1330	480

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Figure 12: Table 2 :

## $\mathbf{4}$

	ISO A-B	ISO B-C	ISO C-D	ISO D-E
25  km/h	8877	8011	8444	8852
30  km/h	8610	8491	9920	9905
40 km/h	6567	6151	8198	8519
50  km/h	6525	6322	7956	7905
60  km/h	5914	5954	6755	8125
80 km/h	5351	5341	6290	6771
100  km/h	4222	3792	-	-
120  km/h	3062	-	-	-



 $\mathbf{5}$ 

	ISO A-B	ISO B-C	ISO C-D	ISO D-E
25  km/h	13930	12380	14760	13650
30  km/h	13000	12730	15000	15490
40 km/h	9328	9577	12240	12880
50  km/h	9363	9482	11960	11670
60 km/h	8502	8339	9830	11300
80 km/h	7592	7323	8855	9553
100  km/h	5735	5449	-	-
120  km/h	4297	-	-	-

Figure 14: Table 5 :

# <sup>50</sup> .1 VIII. Conclusions

51 The simulation of system suspension shows a relation between the energy dissipated by the damping car and

<sup>52</sup> vehicle and road profile properties. Among the properties of the car, it results that the mass of the car (m), the

suspension spring (k s) and the suspension damping (c s) are the elements that influence the dissipated energy.
An increase of mass vehicle and damping coefficient, corroborated with a decrease of spring rate, will produce a

54 An increase of mass vehicle and damping coefficient, corroborated with a decrease of spring rate, will produce a 55 higher energy dissipation for the dampers. The road profile subcomponent who have the biggest influence on the

<sup>56</sup> suspension excitation is the microstructure. The macrostructure has an important role only if the road profile

<sup>57</sup> speeds is below 60 km/h. Thus, a car loaded, with elastic suspension and stiff dampers, will require to dissipate

 $_{\tt 58}$   $\,$  more energy through the dampers. However, macrostructure profiles of road categories with maximum speeds

- <sup>59</sup> between 25 km/h -60 km/h and microstructures profiles of road categories ISO C-D and ISO D-E contributes to
- 60 increased suspension load.

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