Artificial Intelligence formulated this projection for compatibility purposes from the original article published at Global Journals. However, this technology is currently in beta. *Therefore, kindly ignore odd layouts, missed formulae, text, tables, or figures.*

The Effect of the Eccentric Loading on the Components of the 2 Spine

Samir Zahaf¹, Bensamine Mansouri², Abderrahmane Belarbi³ and Zitouni Azari⁴

¹ University of Sciences and Technology

Received: 11 December 2015 Accepted: 2 January 2016 Published: 15 January 2016

7 Abstract

3

4

5

15

⁸ The objective of this work is to study the effect of the backpack on the components of the ⁹ spine system of a child, know the effect of an eccentric load on the intervertebral discs, the ¹⁰ creating a 3D model of the spine of child of 80 kg overall weight under the effect of three ¹¹ eccentric load (P2, P3, P4) plus P1 compression load and calculated by the element method ¹² ends, For the boundary conditions we fixed the sacrum (Embedding the sacrum). We propose ¹³ in this section to draw up a comprehensive study of the distributions of stresses and normal ¹⁴ elastic strain of Von Mises in the intervertebral discs based on loads supported.

16 Index terms— child; herniated discs; lumbar-thoracic; intervertebral discs; finite element; biomechanics; von 17 mises stress-strain; disc degeneration.

18 1 Introduction

he spine or rachis consists of a movable column of 24 free vertebrae and a fixed column formed of fused vertebrae:
the sacrum and coccyx \"(Fig. 2) \"; it is the fixing strut of many essential muscles in the posture and locomotion
and protects the spinal cord located in the vertebral canal; it supports the head and transmits the weight of the
body to the hip joints; with a length of about 70 cm in men (60 cm in women), its reduction may reach 2 cm
when standing [1].
Intervertebral discs connect the vertebral bodies, provide the mobility of the column and amortize them

25 pressure and shocks. Each consisting of a peripheral annulus (annulus) containing a gelatinous core (nucleus). 26 Disc degeneration begins, after a phase of asymptomatic dehydration, with tears in the fibrous ring. The core can then migrate into the thickness of the ring and cause acute or chronic back pain. If it moves further through 27 the ring, the ring may protrude to the rear side of the disc while forming a HERNIATED DISC this is indicated 28 in \backslash "(Fig. 1) \backslash " and \backslash "(Fig. 2) \backslash ". This hernia can migrate into the spinal canal and even exclur leaving the 29 disc. This disc herniation can come compress or "stuck" in one or more nerve roots located near the drive. It 30 is the cause of symptoms: pain is sciatica when the back of the thigh, cruralgie when the pain is in front of the 31 thigh [2] see Figure 1 and figure 2. shows the gel-filled nucleus escapes through a tear in the disc annulus and 32 compresses the spinal nerve [3]. 33

It is the cause of symptoms when sciatic pain is in back of the thigh, crural when pain is in front of the thigh. It 34 comprises variably pain in the lower limbs, defournillements or tingling sensation (paraesthesia), the sensitivity 35 to disturbance of sensation (dysesthesia) up to a complete loss of feeling (anesthesia), loss muscle strength or 36 37 partial or complete paralysis or sphincter disorders. continuously exerted, the pressure of the herniated disc can 38 cause irreversible damage [2]. Every year it is the same finding, schoolchildren satchels or bags to back are too heavy and can cause long-term back problems and deformities of the spine that is to say students complain of 39 back pain, shoulder pain, muscle pain, knee pain, pain in the neck, numbress pain, bad posture, poor balance 40 and falls due at the port of a backpack overloaded view "(Fig. ??) "[5]. 41

Worse, their weight increases over the years from 6.5 kg in 1997 to 8 kg today in the best case. This would amount to carry to an adult of 80 kg weight 17 kg Yet the official circular of 2008 National Education clearly advocates that the weight of the backpack should not exceed 10% of the weight of the child, ie, primary, about

2 MATERIAL AND METHODS

2.5 kg ... we're off!! It is between 8 and 15 years back is the most fragile, and scientific studies have demonstrated
imaging (MRI), the risk of joint damage and intervertebral disc are real [5].

Yet the official circular of 2008 National Education clearly advocates that the weight of the backpack should not exceed 10% of the weight of the child, either primary, about 2.5 kg ... we're off!! It is between 8 and 15 years back is the most fragile, and scientific studies have demonstrated imaging (MRI), the risk of joint damage and intervertebral disc are real [5].

51 During this period of school age, the spine of children is particularly rough ride. With their school bags too 52 heavy, students are real porter, causing stiffness and pain, which are themselves a source of bad posture on often 53 inadequate seating.

It is in this context daily, as well as family education, the accumulation, repetition of these situations will cause joint damage, common causes such as scoliosis. This explains the fact that 67% of students suffer from muscle tension, 50% of back pain, 24% falling asleep during classes and 15% of pain in the shoulders [5]. The schoolbag defined as an eccentric load $\langle "(Fig. ??) \rangle$ ", the load represented by the mass (P4), in other words, this load created a moment of posterior bending which tends to bend the spine and causes a problem called lumbar disc herniation is the most common cause of low back pain. The MRI study [6], alerts of this overweight effect in the development of degenerative disc disease, back pain and then herniated disc \rangle " (Fig. ??) \backslash ".

We propose in this work to draw up a comprehensive study of stresses and strains in the spinal discs distributions based on supported loads. The results show that the level of degeneration increased in all intervertebral discs but concentrated in the four disks D1, D15, D16 and D17.

Fig. ?? shows two vertebrae of the spinal column with an intervertebral disc under the effect of a compound 64 loading (compression P1+ bending moment P4). The compressive load P1 creates an internal pressure in the 65 nucleus, this pressure will there after generate the disc degeneration or degenerative disc disease \"(Fig. ??)\" and 66 \"(Fig. ??)\", as regards the forward flexion P4, if the load of the schoolbag increases, automatically distance 67 between the point of load application and the axis of the spinal column increases, we see that the posterior 68 portion of the annulus fibrosis is compressed and the other front portion is tensioned, that is to say the nucleus 69 pulposus burst back (posterior compression), this compression produced by disc protrusion comes into contact 70 with a nerve root called herniated disc this mentioned in \langle "(Fig. 2) \rangle ". Fig. ??: The intervertebral disc with 71 (a): compression [7]. In this work, the simulation of the disc degeneration, based on a finite element model of 72 the spine depending on the mechanical properties were established ; the boundary condition has been applied 73 74 in the frontal plane to define restriction on movements of translation and rotation of the spine. Fig. ??: The 75 intervertebral disc with (b): bending [7].

76 II.

77 2 Material and Methods

The objective of this study was to investigate the effects induced by an eccentric load of the backpack on the back of a child, know the effect of an eccentric load on the intervertebral discs, cortical bone, cancellous bone, posterior bone, sacrum, basin, created a 3D model of spine, the total mass of person standing of specific global 80kg under the effect of three eccentric loads (p2, p3, p4) plus a p1 compression load and calculated by the finit element method, the boundary conditions we fixed the sacrum (incorporation of the sacrum) see \"(Fig. ??) \". The analysis of biomechanical problems includes several steps.

The first is to study the form to define the geometrical configuration of the object, which allows the reconstitution of the vertebra, the ligament and bone using CAD programs.

The result is a 3D geometric model including these three components will then be prepared for use in finite element analyzes for the study of stresses and strains distribution in the system.

The steps for the execution of the 3D vertebra model \"(Fig. 8) \" are as follow: a) Draw cortical bone that is 88 the upper hinge and the lower hinge, then make the smoothing process; this gives a solid body called the vertebral 89 body. b) Secondly, draw the posterior arch (blade with the pedicle) with the spinous process. c) Finally we draw 90 the transverse process. The simulation of the disc degeneration is based on a finite element model of the healthy 91 spine. Fig. 9 shows a spine model, this consists of five lumbar vertebrae (L1, L2, L3, L4 and L5) plus the sacrum 92 and the basin, twelve thoracic vertebrae (TH1, TH2, TH3, TH4, TH5, TH6, TH7, TH8, TH9, TH10, TH11, 93 TH12) and 17 inter vertebral discs between (S1-L5, L5-L4, L4-L3, L3-L2, L2-L1, L1-TH12 TH12-TH11, TH11, 94 TH10, TH10-TH9, TH9-TH8, TH8-TH7, TH7-TH6, TH6-TH5, TH5-TH4, TH3-TH4, TH3-TH2 TH2-TH1) and 95 various ligaments thoracic lumbar spine (anterior longitudinal ligament, posterior longitudinal ligament, ligament 96 97 interspinous, ligament supraspinatus, yellow ligament and capsular ligament), ligaments of the basin (sacroiliac 98 posterior ligament, sacrotuberous ligament and interosseous ligament). In static loading conditions, the model 99 of the reconstructed spine is used in an analysis for studying the role of the inter vertebral discs and the stress 100 distribution in these disks as well as its supporting structures. The spine is reconstructed in 3D to study the system dimensions (IVD -ligament-bone) "(Fig. 10)". ? The application of the load on the upper side of the 101 thoracic vertebra TH1. ? The fixed part applied to the body of the basin. 102

? The interfaces between the different components of the system of the spine, the cortical bone, the inter vertebral disk and ligament are treated as perfectly bonded interfaces \"(Fig. 10)\". Fig. 9 shows an isometric view of an explored assembly of the spine and each component of the spine system is denoted by letters.

3 Abbreviations

D4: intervertebral disk upstairs four. N4: nucleus in the intervertebral disc upstairs four. D2: intervertebral 107 disk upstairs two. N2: nucleus in the intervertebral disc upstairs two. L2: lumbar vertebra is on level two. D4: 108 intervertebral disk upstairs four. N4: nucleus in the intervertebral disc upstairs four. AF1: annulus fibrosus one. 109 AF2: annulus fibrosus two. The selection of constitutive equations of the vertebral bone is defined as the part 110 of the bone which carries the inter vertebral disc, composed of cortical bone, cancellous bone, the posterior arch, 111 with a Young's modulus of about 12000 MPa. It is well known that cortical bone has better load capacity than 112 the cancellous bone. Cortical bone is considered as an isotropic material, and homogeneous linear elastic. Table 113 ?? shows the tensile strength of the structure annulus fibrosis according to different authors. These materials are 114 anisotropic and non-linear elastic. 115

The behavior of inter-transverse ligament and inter-spinous ligament is nonlinear viscoelastic as in In order to define the boundary conditions, restriction on movements of translation and rotation of the spine has been applied in the lower plane, and defined as having zero displacements. Several charges in the anterior direction were applied as follows:

previous studies [10]; a linear elastic model is chosen to represent this behavior.

Ansys Workbench software was used for analyzing this geometry and generate the most suitable mesh. For the studied behavior, we used tetrahedral elements, type Solid187 conforming to defined parametric surfaces interfaces \"(Fig. 13) \".

124 It is necessary to mesh the components of the spine with small and confused elements to ensure optimum 125 accuracy of the results of stresses and strains in the inter vertebral discs.

126 The material properties of the spine components were selected after a careful review of the published literature

¹²⁷ "Table 2"; it was considered appropriate to define the cortical and cancellous bone as homogeneous and isotropic.

The magnitudes of 12000 MPa and 100 MPa (cortical and cancellous, respectively) were observed in all studies by various researchers.

130 Table ??: Material Properties Specified in the Model.

Since physiologically the nucleus is fluid filled, the elements were assigned low stiffness values (1MPa) and near incompressibility properties (Poisson's ratio of 0.499). Biologically, the annulus fibrosus is comprised of layers of collagen fibers, which attributes to its nonhomogenous characteristics. However, due to limitations in modeling abilities, the annulus was defined as a homogenous structure with a magnitude of 4.2 MPa.

This was based on the modulus of the ground substance (4.2 MPa) and the collagen fibers reported in the literature, taking into account the volume fraction of each component. The complete model of the spine \"(Fig. 13)\" was realized by the SOLIDWORKS SOFTWARE VERSION 2014 and was then transferred to the software Calculates each element ends ANSYS 16.2 WORKBENCHE generated the default mesh then generated linear global custom mesh tetrahedra 10 nodes conform to surface.

The three views of spine model with condensed mesh are shown in \"(Fig. 13)\". All element and node numbers are specified in " The Effect of the Eccentric Loading on the Components of the Spine

¹⁴² 4 Global Journal of Researches in Engineering () Volume XVI ¹⁴³ Issue IV Version I

The posterior arch was modeled with tetrahedral elements to 10 nodes contains (132464 elements, 226389 nodes), the nucleus pulposus in the annulus fibrosus were modeled with tetrahedral type elements 10 nodes (26112 elements 42449 nodes), the annulus fibrosus were modeled with elements of type tetrahedral to 10 nodes (114036 elements, 244800 nodes).

The gelatinous cartilage modeled with a tetrahedral element to 10 nodes (87710 elements, 160055 nodes). Finally, the different types of ligaments generated by a tetrahedral mesh to 10 nodes "Table 3". The diagram in (Fig. ??) v shows a person standing of specific global 80kg weight, the overall mass (Head, Neck, Arm (left + right), Forearm (left + right), hand (left + right)) is 13,4517kg to divided by the top surface of the thoracic vertebrae Th1 representing the pressure P1, P2 load represents the mass of the body superior Trunk is 12,768kg, the distance between the point of application of the load and axis (yy ') is 200 mm \"(Fig. 14) \".

The total mass of the lower trunk of the human body is equal to 22 kg; represented by P3, the distance between the point of application of the load and the axis (yy ') is 250 mm "(Fig. 14) "P4 represents the maximum mass of the backpack is (20 kg), the distance between the point of load application and the axis (yy ') of the spine is (350 mm) "(Fig. 14) ".

For the boundary conditions we fixed the sacrum (Embedding the sacrum) \"(Fig. 14) \". We propose in this section to draw up a comprehensive study of the distributions of stresses and elastic strain in the intervertebral discs, the cortical bone, cancellous bone, the posterior arch, anterior longitudinal ligament and posterior according to the supported loads. Distributions of global stress state for each component of our model were presented.

A quantitative analysis was performed based on a scale of progressive visual colors predefined by the software used (ANSYS Workbench 16.5), ranging from dark blue to red.

Results 5 165

Fig (15) shows a histogram of stress and maximum strain of Von Mises, we notice that the spine undergoes a 166 concentration of maximum stresses in the thoracic region, in the order word the stresses in the thoracic vertebrae 167 (Th3, Th4, Th5, Th6, Th7) are respectively equal to (995,68MPa, 754.61 MPa, 467.09 MPa, 483.08 MPa, 369.65 168

MPa) as mentioned in "(Fig. 17) ". 169

Fig 16 shows a load applied to the upper surface of the thoracic vertebra TH1 of the spinal column causes a 170 high concentration of maximum Von Mises strains in the anterior part of vertebral bodies (red section) this is 171 mentioned in \backslash "(Fig. 17) \backslash ". 172

On the other hand, Fig 17 shows that the posterior arch of the thoracic vertebrae (Th3, Th4, Th5, Th6, Th7) 173 absorbed the maximum von Mises stresses, these stresses were observed on a posterior side of the spine (red 174 contour) with respect to other components of the system of the spine. Proceeding from the fact that the Fig 175 (??7) and (??6) that watches the posterior load presents greater strains within two thoracic vertebrae (Th3, 176 Th4) which are equal to (0.29194, 0.21867), which means that the so-called vertebrae are the most stressed in 177 the case of posterior bending. 178

Fig (18) shows that the posterior loading presents maximum stresses and strains concentrated in the 179 intervertebral disc D1 that is to say between the sacrum and the lumbar vertebra L5, in the order word the 180 ('(Fig. 19) (clearly shows that the loading posterior with a lever arm equal 350mm presents maximum Von 181 Mises stresses and strains concentrated in the disc D1 and are respectively equal to (6.9797MPa, 1.7347mm / 182 mm). We see in Fig (18) the intervertebral discs (D1, D15, D16, D17) absorbed the maximum stresses that 183 equal (6,9797MPa, 4,4374MPa, 4,7858MPa, 2,7365MPa), On the other hand the posterior loading presents of 184 maximum strains concentrated in the intervertebral discs (D1, D15, D16, D17) which are respectively equal to 185 (1.7347, 1.0586, 1.1463, 0.66065) as mentioned in ("Fig. 19). On the other hand, ("Fig. 22) shows that 186 the maximum von Mises stresses in the cortical bone (S1, Th12, Th5, Th1) are equal to (40,069MPa, 140.15 187 MPa 223.82 MPa 496, 69 MPa) as compared to other components of the system of the spine see \langle "(Fig. 24) 188 ". A loading of the posterior backpack applied on the upper surface of the thoracic vertebra TH1 of the spinal 189 column causes a high concentration of maximum normal strains in the anterior part of the thoracic vertebra Th 190 (red part) this is mentioned in "(Fig. 23) ", with regard to the said vertebra supported Von strain value set 191 which are equal to (0.041791 mm / mm) relative to the other components of the system of the spine. 192

The posterior load \langle "(Fig. ??) \rangle " shows clearly that the stresses and strains of Von Mises are concentrated 193 in the two cancellous bone (Th1, Th5) and are respectively equal to (4.6282Mpa, 5.7386MPa) and (0.049594, 194 0.057685) this is mentioned in the (Fig 26) The posterior loading of the backpack with a 350mm lever shown that 195 increased stresses and strains of Von Mises illustrated in the face of upper and lower articulation of the posterior 196 197 arch of the thoracic vertebrae (Th3, Th4, Th5, Th6, Th7) (red outline) \"(Fig. 27) \", on the other hand \"(Fig. 198 28) \"shows clearly legend stress and strain of Von Mises put in the thoracic region (Th3, Th4, Th5, Th6, Th7) are respectively equal to (995,68MPa, 754,61MPa, 467,09MPa, 483,08MPa, 369,65MPa) and (0.29194, 0.21719, 199 0.16183, 0.21867, IV. 200

Discussion 6 201

202 In sum, we concluded that the posterior loading is certainly an aggravating factor, and may cause long term back 203 problems and strains of the spine, the 3D model of the spine of a child under the effect of an eccentric load and calculate by the FEM provokes stress and strains maximum of Von Mises concentrated in the intervertebral disc 204 (D1) and are equal to (6,9797MPa, 1,7347mm / mm) as noted in the "(Fig. 18) ", with regard to "(Fig. 19, 19, 19)205 20, 21) $\$ show that the intervertebral disc (D1) is the most damaged which is disc degeneration often occurs 206 after a phase asymptomatic dehydration cracks, tearing of annulus fibrosus (D1), the nucleus (N1) can then 207 along these cracks migrate into the ring thickness (D1), and cause acute or chronic back pain, If the core (N1) 208 move around more through the ring (D1), the core can project to the posterior surface of the disc while forming 209 a lumbar disc herniation, this hernia can complete rupture of the ring, migrate laterally into the vertebral canal, 210 or up or down, and even exclude leaving the disk, herniated disc that can come be compressed one or more nerve 211 roots "stuck" near the disc, causing the symptoms of pain "sciatica" when the rear seat of the thigh or "cruralgie" 212 when the seat of pain in the front of the thigh. This justifies that the distance between the load which is the 213 point of application of the load and the axis of the spine plays an important role in increasing stresses at the 214 intervertebral discs. 215 V.

216

7 Conclusion 217

In sum, we concluded the case of posterior loading 350mm lever arm with a load 200N posterior indicate normal 218 maximum Von Mises stresses in four intervertebral discs (D1, D15, D16, D17) and are equal to (6,9797MPa, 219 4,4374MPa, 4,7858MPa, 2,7365MPa) these mentioned in "(Fig. 18)", on the other hand "(Fig. 19)"clearly 220 shows the elastic strain is higher in the four intervertebral discs (D1, D15, D16, D17) that are equal (1.7347, 221 1.0586, 1.1463, 0 66065), which justifies that the distance between the load which is the point of application of 222 the load and the axis of the spine plays a very important role in increasing the solitation of the latter. 223

- 224 **8 VI.**
- 225 9 Global



Figure 1: Fig. 1 :



 $1 \ 2$



¹The Effect of the Eccentric Loading on the Components of the Spine © 2016 Global Journals Inc. (US) 2 © 2016 Global Journals Inc. (US)



Figure 3: Fig. 2:







Figure 5: Fig. 6 :The



Figure 6: Fig. 8 :



Figure 7: Fig. 9:



Figure 8: AFig. 10:



Figure 9: Fig. 11 :



Figure 10: Fig 12:



Figure 11: Table 1 :



Figure 12:

 14 1420 mm

Figure 13: Fig. 14 :



Figure 14:



Figure 15: Fig. 15 : Fig. 16 : Fig. 17 :



Figure 16: Fig. 18:



Figure 17: AFig. 20 :



Figure 18: Fig (20) Fig. 19 :



Figure 19: Fig. 21 : Fig. 22 : AFig. 23 :



Figure 20: Fig. 24 :



Figure 21: Fig (25)



 $\mathbf{25}$







Figure 23: Fig. 26 :



Figure 24: Fig. 27:

".

[Note: \bigcirc 2016 Global Journals Inc. (US)]

Figure 25: Table 3

3

COMPONENT	NODES	ELEMENTS	Thickness
Cortical Bone	961810	644683	$3\mathrm{mm}$
Cancellous Bone	244460	164441	$3\mathrm{mm}$
Posterior Bone	226389	132464	$3 \mathrm{mm}$
Cartilage endplates	160055	87710	$3\mathrm{mm}$
Annulus Ground Substance	244800	114036	$3\mathrm{mm}$
Nucleus Pulposus	42449	26112	$3 \mathrm{mm}$
Anterior Longitudinal Ligament	45798	24467	$3 \mathrm{mm}$
Posterior Longitudinal Ligament	14414	6607	$3 \mathrm{mm}$
Ligamentum Flavum	30226	13447	$3 \mathrm{mm}$
Transverse Ligament	285328	131648	$3 \mathrm{mm}$
Inter-Spinous Ligament	28968	13158	$3\mathrm{mm}$
Supra-Spinous Ligament	17833	8279	$3\mathrm{mm}$
Capsular ligament	51816	24072	$3\mathrm{mm}$
Sacrotuberous Ligament	20878	10128	$3\mathrm{mm}$
Sacroiliac posterior Ligament	5876	3280	$3\mathrm{mm}$
Interosseouse Ligament	13756	8306	$3 \mathrm{mm}$
TOTAL	2005025	1178694	$3\mathrm{mm}$

[Note: Fig. 13: Spine 3D finite element modeling (ANSYS 16.2 software).]

Figure 26: Table 3 :

Acknowledgements .1 227

- The authors extend their appreciation to the Director of Scientific Research at LaBPS for funding the work 228 through the Biomechanics Research Group. 229
- 0.21867) compared to other components of the system spine. We see in Figure ??8 the role of the basin to 230
- transmit the load to the lower part of the human body and absorbation stresses and strain Von bets (red outline), 231
- we note that the two bodies (basin, sacrum) supported stresses and normal elastic deformations which are equal 232
- 233 to (46,069MPa, 28,201MPa) and (0.012947, 0.0187) relative to the other components of the system of the spine. Fig. ??9: Distributions of stresses and strains in the basin and sacrum for a load of 20kg. 234
- [Masc et al.], Claire B-R Masc, Pierre-Jean A Phd, B Rohan-Jean, Yves G-R Phd, L F Meng, Carl-Éric 235 A-P Phd.
- [White Iii and Panjabi ()], A A White Iii, And Panjabi, MM. Clinical Biomechanics Of The Spine 1990. 237
- [Zheng et al. ()], S N Zheng, Q Q Yao, L M Wang, W H Hu, B Wei, Y Xu, D G Zhang. Biomechanical Effects 238
- Of Semi Constrained Integrated Artificial Discs On Zygapophysial Joints Of Implanted Lumbar Segments. 239 Experimental and Therapeutic Medicine 2013. 6 p. . 240
- [Karine ()], L Karine . 2014. (Institut Français D'étiopathie (IFE) Paris, le 16 Septembre) 241
- [Kassab et al. ()], Dr Kassab, M Centre Avicenne, Médical. Av Tahar Sfar 2092. 2. (El Manar) 242
- [Kiapour et al. ()] 'A Biomechanical Finite Element Study of Subsidence and Migration Tendencies in Stand-243 Alone Fusion Procedures. Comparison of an In Situ Expandable Device with a Rigid Device'. A Kiapour, A 244
- M Kiapour, M Kodigudla, G M Hill, S Mishra, V K Goel. J Spine 2012. 1 p. . 245
- [Starmans et al. ()] 'A Three-Dimensional, Finite-Element Analysis Of Bone Around Dental Implants In An 246 Edentulous Human Mandible'. F J Starmans, W H Steen, F Bosman. Arch Oral Biol 1993. 38 p. . 247
- [Rohlmann et al. ()] 'Analysis of the influence of disc degeneration on the mechanical behaviour of a lumbar 248
- motion segment using the finite element method'. A Rohlmann, T Zander, H Schmidt, Wilke Hj, G 249 Bergmann . J Biomech 2006. 39 p. . 250
- [Phd et al. ()] 'Anatomic facet replacement system (AFRS) restoration of lumbar segment mechanics to intact. 251
- 252 a finite element study and in vitro cadaver investigation'. G , Vijay K Phd , Ankit , J Bs , Jayant , Bs , A Faizan, K Bs, Ali Ms, R W Hoy, Meng Fauth, AR, Phd. SAS Journal 2007. 1 p. . 253
- [Kim et al. ()] 'Biomechanical Analysis of Fusion Segment Rigidity Upon Stress at Both the Fusion and Adjacent 254 Segments-A Comparison between Unilateral and Bilateral Pedicle Screw Fixation'. H J Kim, Tak Kang, K 255 Chang, BS, Lee Chk, JW Kim, And Yeom, JS. Yonsei Med J 2014. 55 (5) p. . 256
- [Steven et al. ()] Biomechanical Evaluation Of A Spherical Lumbar Interbody Device At Varying Levels Of 257 Subsidence. Exponent, inc, philadelphia, pa, sas journal, A Steven, M S Rundell, Jorge E Isaza, M D 258 Steven, M, Kurtz Phd. 2011. 5 p. . 259
- [Rohlmann et al. ()] 'Comparison of the effects of bilateral posterior dynamic and rigid fixation devices on the 260 loads in the lumbar spine'. A Rohlmann , Burra Nk , T Zander , G Bergmann . Eur Spine J 2007. 16 p. . 261
- [Thomas ()] 'Contribution A L'analyse Biomécanique Et A L'évaluation Des Implants Rachidiens, L'école 262 Nationale Supérieure D'arts Et Métiers Spécialité'. M Thomas . Biomécanique 2008. 263
- [Lee and Teo ()] 'Effects of laminectomy and facetectomy on the stability of the lumbar motion segment'. K Lee 264 , E Teo . Med Eng Phys 2004. 26 p. . 265
- [Gong et al. ()] 'Finite Element Analysis of 3 Posterior Fixation Techniques in The Lumbar Spine'. Z Gong , Mm 266 , Z Chen , Md , Z Feng , Md , Y Cao , Jiang Mm , M D Ch , X Jiang , Md . Feature Article 2014. 37 p. . 267
- [Chch et al. ()] 'Finite element analysis of biomechanical behavior of whole thoraco-lumbar spine with ligamen-268 tous effect'. Lan Chch, Kuo Chs, Chen Chh, H T Hu. The Changhua Journal of Medicine 2013. 11 p. 269 270
- [Finite Element Analysis of Sacroiliac Joint Fixation under Compression Loads International Journal of Spine Surgery ()] 271
- 'Finite Element Analysis of Sacroiliac Joint Fixation under Compression Loads'. 10.14444/3016. International 272 Journal of Spine Surgery 2016. 273
- [Byun et al. ()] 'Finite Element Analysis of the Biomechanical Effect of CoflexTM on the Lumbar Spine. 274 laboratory investigation'. D H Byun , Ah Shin , D Kim , J M Kim , S H Kim , HI . Korean J Spine 275 2012. 9 (3) p. . 276
- [Polikeit ()] Finite element analysis of the lumbar spine: Clinical application. Inaugural dissertation, A Polikeit 277 . 2002. University of Bern 278
- [Mingzhi et al.] Four Lateral Mass Screw Fixation Techniques In Lower Cervical Spine Following Laminectomy. 279
- A finite Element Analysis Study Of Stress Distribution, S Mingzhi, Z Zhen, L Ming, Z Junwei, D Chao, 280 Kai M Shouyu, W. 281
- [Dr and Kilcup (2011)] Herniated disk fixed without harmful, Addictive Drugs and Surgery, Dr, Kilcup. 20 282 October 2011. 283

9 GLOBAL

- [Bohinski ()] Herniated Lumbar Disc. Mayfield Clinic, university of cincinnati department of neurosurgery,
 cincinnati, Ohio, mayfieled brain and spine, Robert Bohinski, MD. 1998-2016.
- [Hernie Discale Lombaire] Hernie Discale Lombaire . Service de Chirurgie orthopédique et Traumatologique,
 Hôpital Beaujon,
- [Ng et al. ()] 'Influence Of Laminotomies And Laminectomies On Cervical Spine Biomechanics Under Combined
 Flexion-Extension'. H W Ng , Teo Ech , Q H Zhang . Journal Of Applied Biomechanics 2004. 20 p. .
- [Ibarz et al. ()] 'Instability Of The Lumbar Spine Due To Disc Degeneration. A Finite Element Simulation'. E
- Ibarz, Y Más, J Mateo, A Lobo-Escolar, A Herrera, L Gracia. Advances In Bioscience And Biotechnology
 2013. 4 p. .
- [Marcovschi Champain ()] S Marcovschi Champain . Corrélations Entre Les Paramètres Biomécaniques Du
 Rachis Et Les Indices Cliniques Pour L'analyse Quantitative Des Pathologies Du Rachis Lombaire Et De
 Leur Traitement Chirurgical, (Enam, Paris) 2008.
- [Natarajan and Andersson ()] 'Modeling the annular incision in a herniated lumbar intervertebral disc to study
 its effect on disc stability'. R N Natarajan , Gbj Andersson . Comput Struct 1997. 64 p. .
- [Hj et al. ()] 'New intradiscal pressure measurements in vivo during daily activities'. Wilke Hj , P Neef , M Caimi
 T Hoogland , Claes Le . Spine 1999. 24 p. .
- [Hw and Ec ()] 'Nonlinear finite-element analysis of the lower cervical spine (C4-C6) under axial loading'. Ng
 Hw , Teo Ec . J Spine Disord 2001. 14 p. .
- ³⁰² [Denozi´ere ()] Numerical modeling of a ligamentous lumber motion segment, G Denozi´ere . 2004. Department
 ³⁰³ of Mechanical Engineering. Georgia Institute of Technology. Georgia. USA (M.S. thesis)
- [Holekamp et al. ()] 'Optimal Intervertebral Sealant Properties for the Lumbar Spinal Disc. A Finite-Element
- Study'. S Holekamp , V Goel , K Phd , M D Hiroshi , Janet Ms , E Nabil , MD . SAS Journal. Spring 2007.
 1 p. .
- [López et al. ()] 'Probability Of Osteoporotic Vertebral Fractures Assessment Based On DXA Measurements
 And Finite Element Simulation'. E López , I Elena , A Herrera , J Mateo , A Lobo-Escolar , S Puértolas , L
 Gracia . Advances in Bioscience and Biotechnology 2014. 5 p. .
- $\frac{1}{2}$
- 310 [References Références Referencias] References Références Referencias,
- Sharma et al. ()] 'Role of ligaments and facets in lumbar spinal stability'. M Sharma , Langrana Na , J Rodriguez
 Spine 1995. 20 p. .
- Stress Reduction in Adjacent Level Discs Via Dynamic Instrumentation. A Finite Element
 Analysis'. M D Cae , H Huang , Vestgaarden Phd , Tov , Phd , S Saigal , Phd , D H Clabeaux , R N
 Pienkowski , D , Phd . SAS Journal. Spring 2007. 1 p. .
- [Smit et al. ()] 'Structure and function of vertebral trabecular bone'. T Smit , A Odgaard , E Schneider . Spine
 1997. 22 p. .
- Pitzen et al. ()] 'The influence of cancellous bone density on load sharing in human lumbar spine: a comparison
 between an intact and a surgically altered motion segment'. T Pitzen , F H Geisler , D Matthis , H M Storz
 , K Pedersen , W I Steudel . *Eur Spine J* 2001. 10 p. .
- 321 [Sairyo et al. ()] 'Three-dimensional finite element analysis of the pediatric lumbar spine'. K Sairyo, V K Goel
- , A Masuda , S Vishnubhotla , A Faizan , A Biyani , N Ebraheim , D Yonekura , R I Murakami , T Terai . *Eur Spine J* 2006. 15 p. .
- Shin ()] Viscoelastic responses of the lumbar spine during prolonged stooping, Gwanseob Shin . 2005. NCSU,
 USA. (Ph.D. dissertation)