

# Simulation and Analysis of Power Quality Improvement using Multilevel Unified Power Quality Conditioner

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## Abstract

Unified Power Quality Conditioner (UPQC) is an effective device to solve the power quality problems. The UPQC is a combination of series and shunt filters which simultaneously compensate load voltage and source current imperfections. This paper presents harmonic mitigation using three level Neutral Point Clamped inverter based Unified Power Quality Conditioner. The use of three level Neutral Point Clamped converters allows a better performance of equipment by reducing harmonics and the ripple of the generated voltages and currents. The performance of UPQC in the reduction of harmonics is evaluated when employed with Multi carrier based SPWM and three level novel SVPWM techniques. Simulation results based on MATLAB/SIMULINK are presented to verify the effective compensation of harmonics using the two different modulation techniques.

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**Index terms**— active filters, neutral point clamped converters, total harmonic distortion, power quality, SVPWM.

## 1 I. Introduction

The increased use of non-linear loads deteriorate power system voltage and current waveforms as they inject harmonics into the system. This results in increased losses, lower efficiency, failure of equipment etc. in the power system. Apart from voltage and current harmonics, voltage sag, voltage swell, voltage outage also can lead to poor quality of power [1]. Harmonic compensation and voltage regulation have become more important as imbalance in the voltage and presence of harmonics have been serious issues. Hence, there is a great need to mitigate these power quality issues.

The introduction of advanced power electronics technology has led to the development of active power filters which are viable solution to these power quality problems [1,2].

The general arrangement of Unified power quality conditioner is shown in Fig. ???. The main function of a UPQC is to compensate voltage and current harmonics.

The UPQC combines series and shunt active filters with a common dc link. The series active filter suppresses voltage distortions while the shunt filter Author ??: e-mail: gootyanu@gmail.com cancels current distortions such that this combination allows simultaneous compensation of voltages and currents supplied to the sensitive load to see that they are sinusoidal and balanced. Fig. ??? : General configuration of UPQC Multilevel inverters play an important role in the reduction of harmonic content in the voltages and currents. The multilevel inverters can synthesize high output voltage from smaller voltage levels and thus the current ripples and voltage harmonics are reduced. The UPQC presented in this work consists of three level converter topology [3,4]. The performance of UPQC can be optimized because of reduction in the size of passive components and transformers [4].

## 2 II. The Upqc Controller

The UPQC controller is composed of PLL circuit, Reference Voltage Algorithm and Reference Current Algorithm [4,5, ???].

43 The PLL circuit has the system voltages  $V_{ab}$  and  $V_{cb}$  i.e ( $V_{ab} = V_{as} - V_{bs}$ ,  $V_{cb} = V_{cs} - V_{bs}$ ) as inputs and  
 44 the outputs are the signals  $PLL\_a$ ,  $PLL\_b$  and  $PLL\_c$  as shown in Fig. ??.

45 **3 Fig. 2 : The synchronizing circuit**

46 The PLL circuit guarantees the load voltages and source currents to be balanced sinusoidal waveforms at  
 47 fundamental frequency.

48 The reference current control strategy is shown in Fig. 3. The reference currents algorithm control block  
 49 determines six reference currents ( $i_{aref1}$ ,  $i_{bref1}$ ,  $i_{cref1}$ ) and ( $i_{aref2}$ ,  $i_{bref2}$ ,  $i_{cref2}$ ) by using the outputs of  
 50 PLL ( $PLL\_a, PLL\_b, PLL\_c$ ), the DC link voltages ( $V_{dc1}$ ,  $V_{dc2}$ ) and the load currents ( $I_{al}$ ,  $I_{bl}$ ,  $I_{cl}$ ) as inputs. The  
 51 shunt active power filter will then synthesize the reference currents. The "reference voltage algorithm" shown in  
 52 Fig. 4 calculates, the reference voltages ( $V_{aref}$ ,  $V_{bref}$ ,  $V_{cref}$ ) by using system input voltages ( $V_{as}$ ,  $V_{bs}$ ,  
 53  $V_{cs}$ ) and PLL outputs( $pll\_a$ ,  $pll\_b$ ,  $pll\_c$ ) that will be synthesized by the series power converter.

54 .

55 **4 III. Switching Strategy of Three Level Converters**

56 In order to illustrate the switching control technique applied to the series and shunt active power converters, a  
 57 basic three level NPC (Neutral Point Clamped) topology as shown in Fig. ?? is used [7,8].

58 **5 Fig. 5 : Three level Neutral point clamped converter**

59 Each leg has four switching devices connected in series. As an example, phase "a" is considered to explain the  
 60 behavior of the circuit.

61 The output of the inverter can take three voltage levels based on the switching states of the devices. The  
 62 output  $V_a$  is positive when switches  $S_{1a}$  and  $S_{2a}$  are ON, it is negative when  $S_{3a}$  and  $S_{4a}$  are turned ON, and  
 63 it is '0' when switches  $S_{2a}$  and  $S_{3a}$  are ON. The switching states of the devices and the corresponding output  
 64 voltages with respect to the dc mid-point are indicated in the following Table ??.

65 The switching strategy of the series active filter is shown in Fig 6 ?? In this technique, the reference signal is  
 66 compared with measured signal, the error is amplified and processed by PWM generator to obtain  $V_a\_PWM$ .  
 67 This signal is compared with two triangular waves of different limits having unit magnitude. The switching  
 68 control strategy of the shunt active converter is shown in In this work, Phase Disposition multicarrier scheme  
 69 is applied to Sinusoidal PWM. In this modulation, the reference sine wave is compared with the level shifted  
 70 carrier triangular waves for producing the pulses. For a three level inverter, two triangular carrier waves of same  
 71 frequency and amplitude are compared with the reference wave. The plane is divided into 6 triangular major  
 72 sectors numbered I to VI each of 60° of fundamental cycle. There are 4 minor sectors within each major sector  
 73 such that 24 minor sectors are there in the plane.

74 The vertices of these minor sectors represent the voltage vectors. In the above plane,  $V_0$  is the zero voltage  
 75 vector, large voltage vectors are represented by  $V_{13}, V_{14}, V_{15}, V_{16}, V_{17}, V_{18}$  and  $V_7, V_8, V_9, V_{10}, V_{11}, V_{12}$   
 76 are the medium voltage vectors. To determine the location of the command vector  $V^*$  in a given major sector,  
 77 first space vector phase angle  $\theta^*$  is calculated and then sector is determined. The determination of major sector  
 78 is done as follows:

79 Table I : Determination of major sector

80 **6 Range of  $\theta^*$**

81 Major sector number 0  $0^\circ < \theta^* < 60^\circ$  I  $60^\circ < \theta^* < 120^\circ$  II  $120^\circ < \theta^* < 180^\circ$  III  $180^\circ < \theta^* < 240^\circ$  IV  $240^\circ < \theta^* < 300^\circ$   
 82 V  $300^\circ < \theta^* < 360^\circ$  VI

83 Let us consider space vector diagram of sector I as shown in Fig. ?. It contains 4 minor triangles  $D_1, D_7,$   
 84  $D_{13}$  and  $D_{14}$ . The reference vector can be located in any of these 4 regions, where each region is limited by three  
 85 adjacent vectors.

86 If the triangular sector where the command vector lies is defined by vectors  $V_x, V_y,$  and  $V_z$  assuming their  
 87 durations  $T_x, T_y,$  and  $T_z$  respectively and  $T_x + T_y + T_z = T_s$ , then  $V^* = V_{ref}$  can be synthesized by  $V_x, V_y,$   
 88 and  $V_z$  as follows : ( $0 < \theta^* < 60^\circ$ ),  $V^*$  lies in sector  $D_{14}$  and can be synthesized by Vectors  $V_2, V_7,$  and  $V_{14}$ .  $X,$   
 89  $Y,$  and  $Z$  can be determined as follows:  $X = 2m [\cos(\theta^*) - \frac{1}{2}]$   $Y = -1 + m \frac{2}{\sqrt{3}}$   $Z = 2-2m [\cos$   
 90  $(\theta^*) + \frac{1}{2}]$

91 Similar argument can be applied, when the reference vector lies in the others major sectors. The above  
 92 calculations for the entire coordinate plane can be obtained by replacing  $\theta^*$  by  $\theta^* - 60^\circ, \theta^* - 120^\circ, \theta^* - 180^\circ, \theta^* -$   
 93  $240^\circ,$  and  $\theta^* - 300^\circ$  respectively.

94 **7 V.**

95 **8 Simulation Results**

96 Simulations were carried out in MATLAB/ SIMULINK on three-level Neutral Point Clamped Unified Power  
 97 Quality Conditioner connected to a non-linear load employing Sinusoidal Pulse Width Modulation and Space

98 Vector Pulse Width Modulation techniques and the results are presented below. FFT analysis is carried out in  
99 order to measure %THD in the load voltage and source current.

100 To study the performance of the UPQC, 5 th and 7 th harmonics are deliberately injected into the system  
101 and simulations were carried out to show the response of the UPQC. The series inverter is put into operation  
102 at 0.2sec and shunt inverter at 0.5sec. FFT analysis is carried out on the load voltage at 0.1sec and the THD  
103 is found to be 12.32%. In the second analysis, FFT is done at 0.8sec i.e. after connecting UPQC and THD is  
104 reduced to 2.01% FFT analysis of source current FFT analysis of source current before connecting UPQC FFT  
105 analysis of source current after connecting UPQC FFT analysis is carried out on the source current at 0.1sec  
106 before connecting UPQC and the THD is found to be 33.97%. In the second analysis, FFT is done at 0.6sec  
107 after connecting UPQC and THD is 2.01% b) Simulation results of 3level UPQC with SVPWM 19, it is clear  
108 that the harmonics are reduced to some extent after 0.1 sec where series filter is switched ON and from 0.25sec  
109 onwards there is a considerable reduction in the harmonics as both filters are in operation.

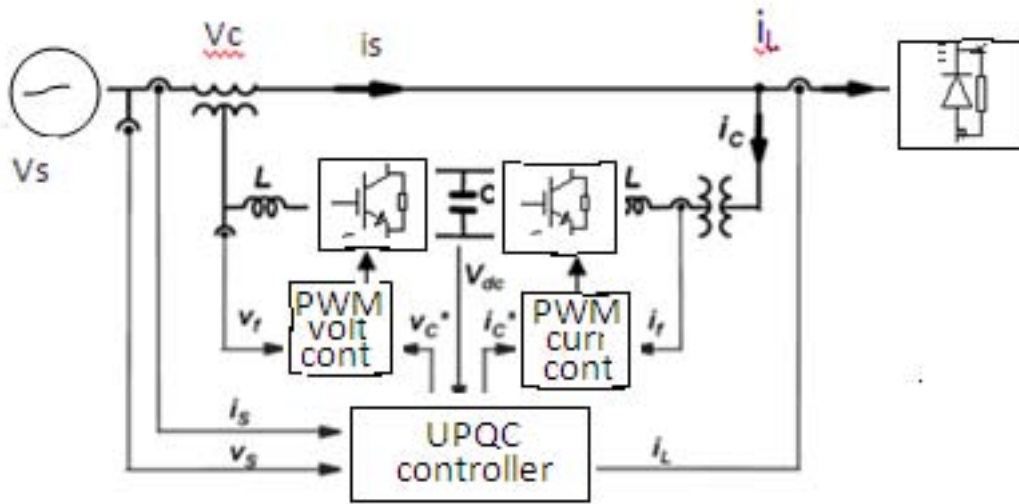
## 110 9 FFT analysis of load voltage

111 FFT analysis of load voltage before connecting UPQC FFT analysis of load voltage after connecting UPQC FFT  
112 analysis is carried out on the load voltage at 0.05sec before switching ON series and shunt inverters and the THD  
113 is found to be 12.32%. FFT analysis of load voltage again carried out at 0.3sec after connecting both series and  
shunt filters and THD is found to be 1.27%.<sup>1</sup>



Figure 1: Fig. 3 :

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Figure 2: Fig. 4 :

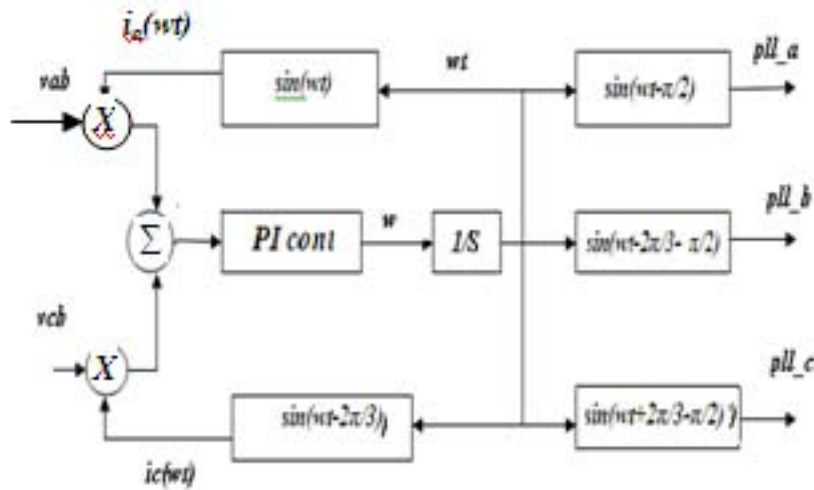
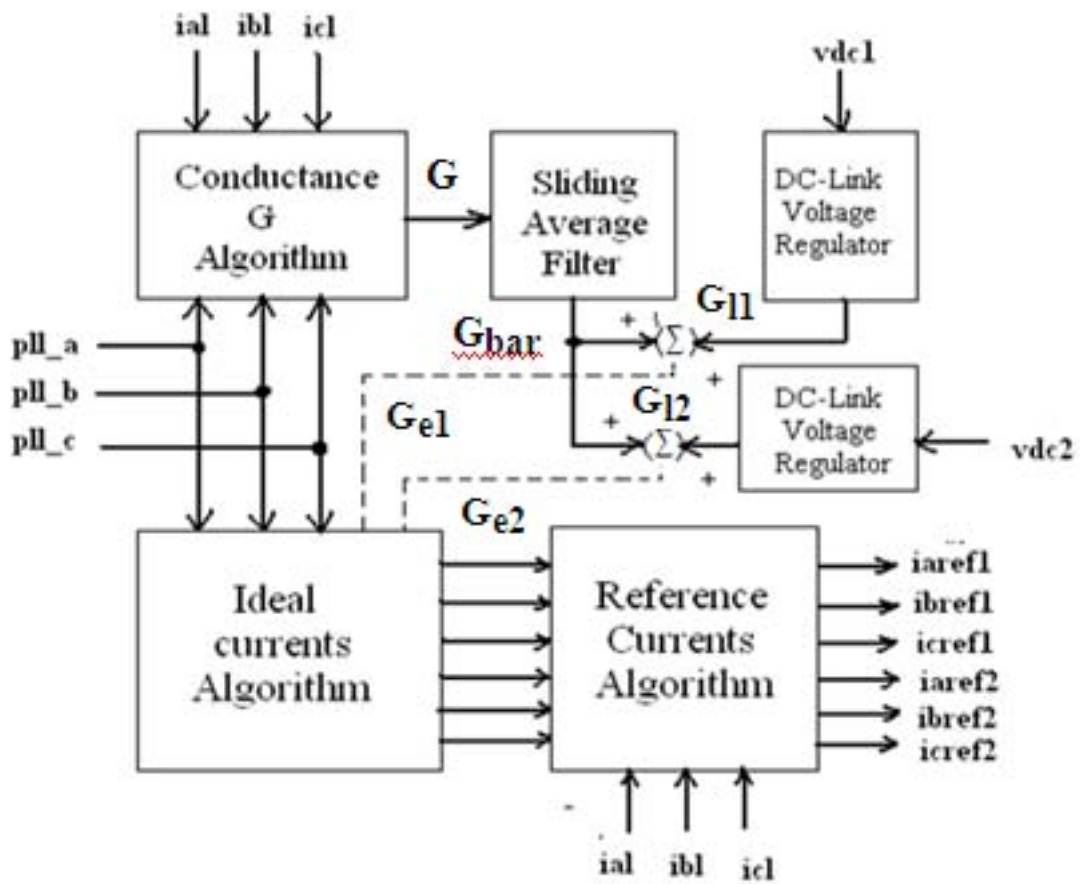


Figure 3:



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Figure 4: Fig. 6 :

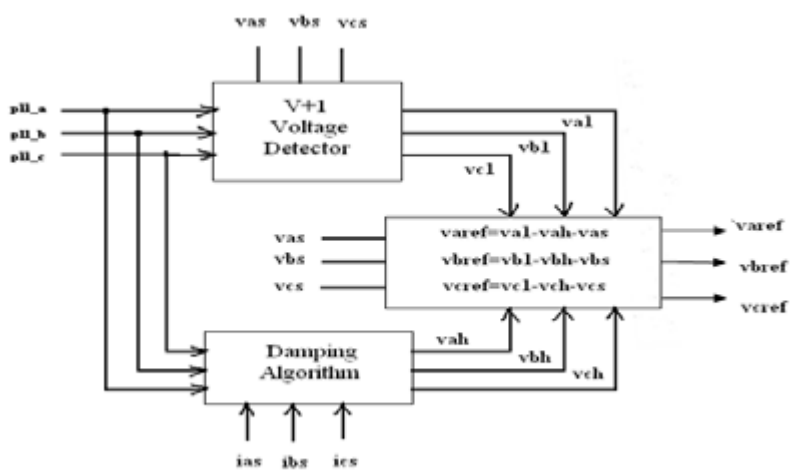
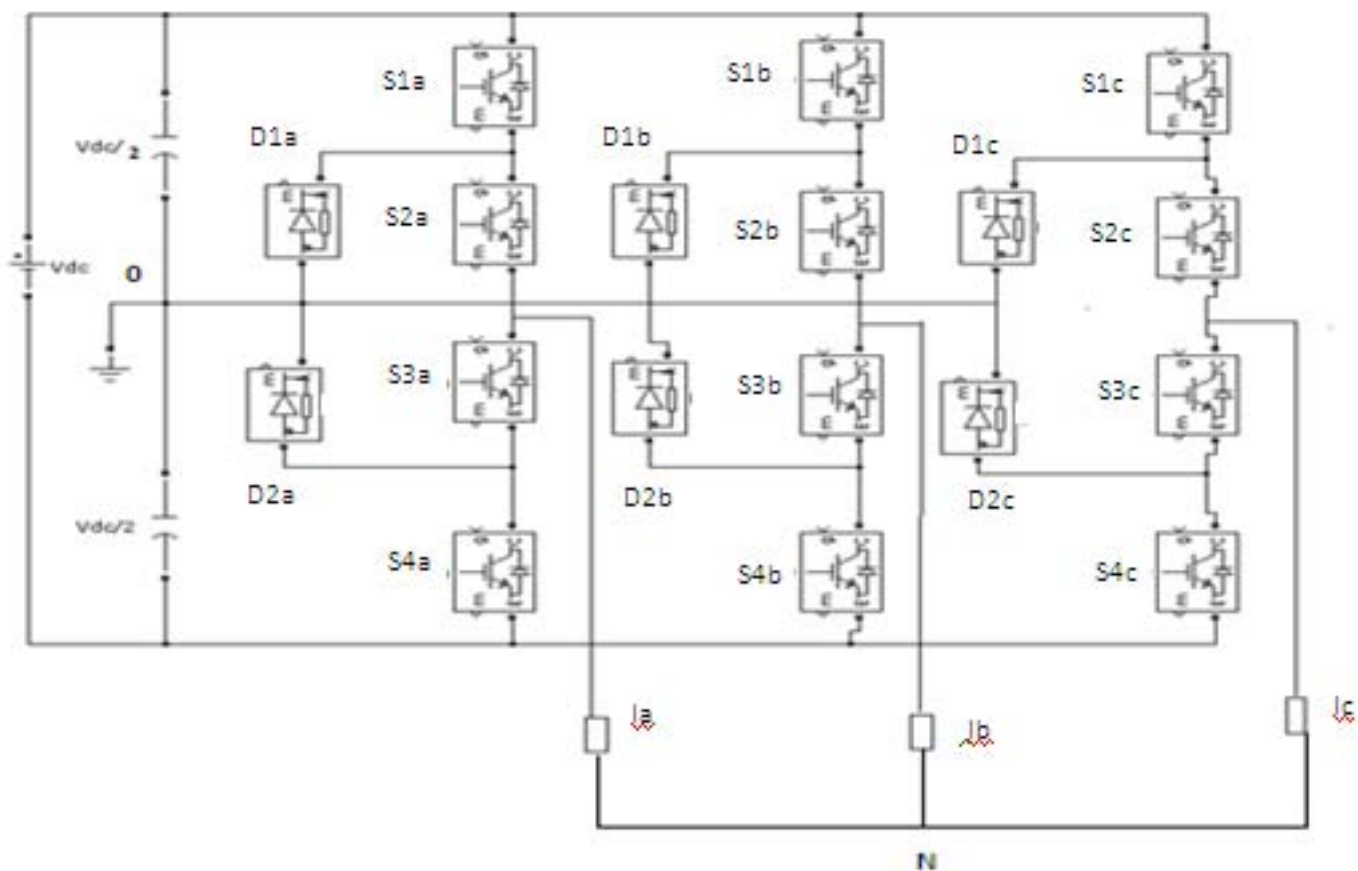
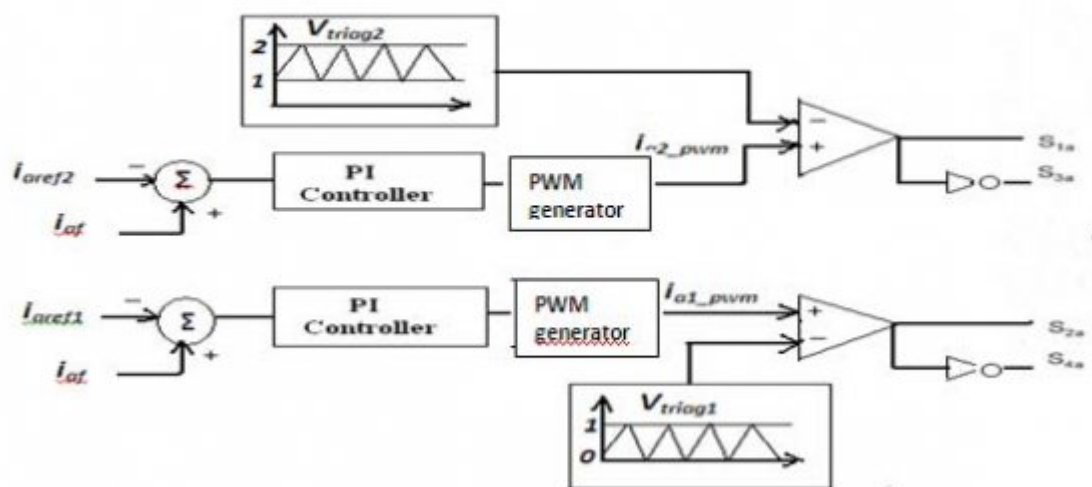


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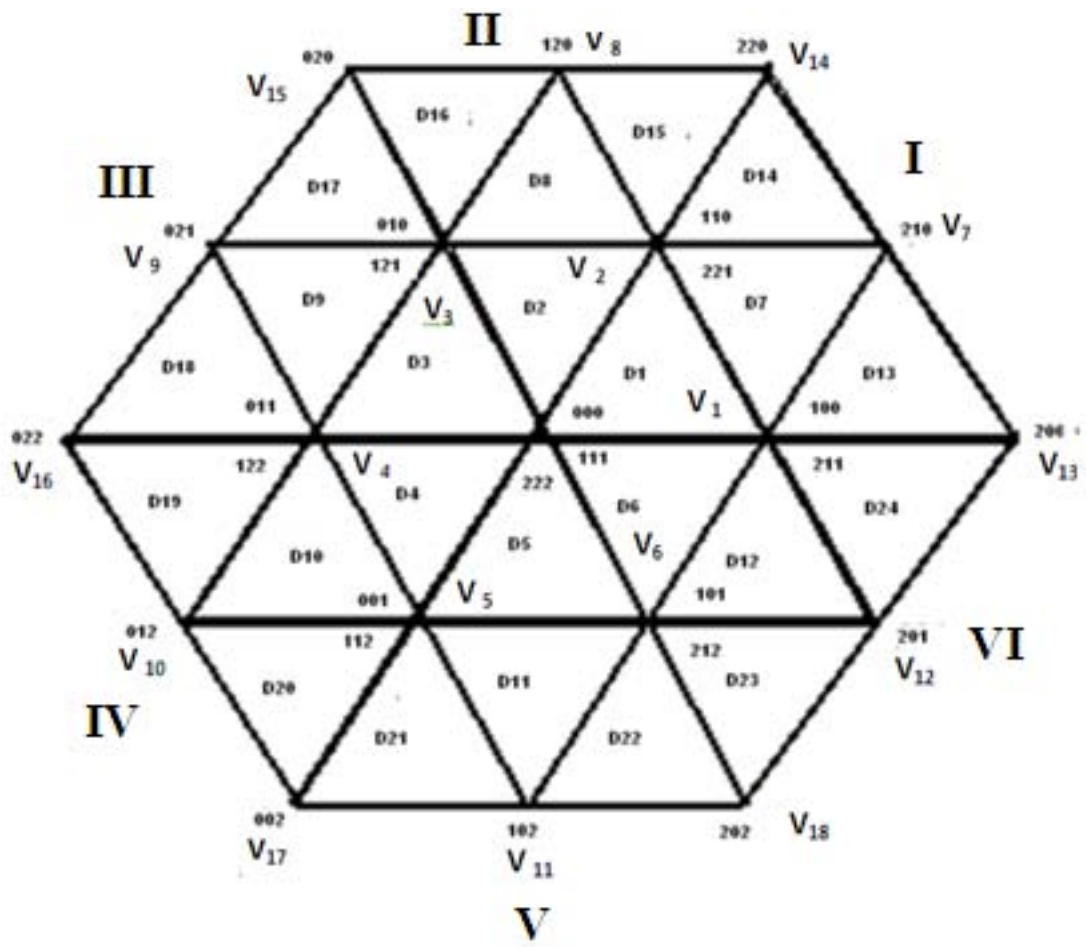
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Figure 6: Fig. 8 :



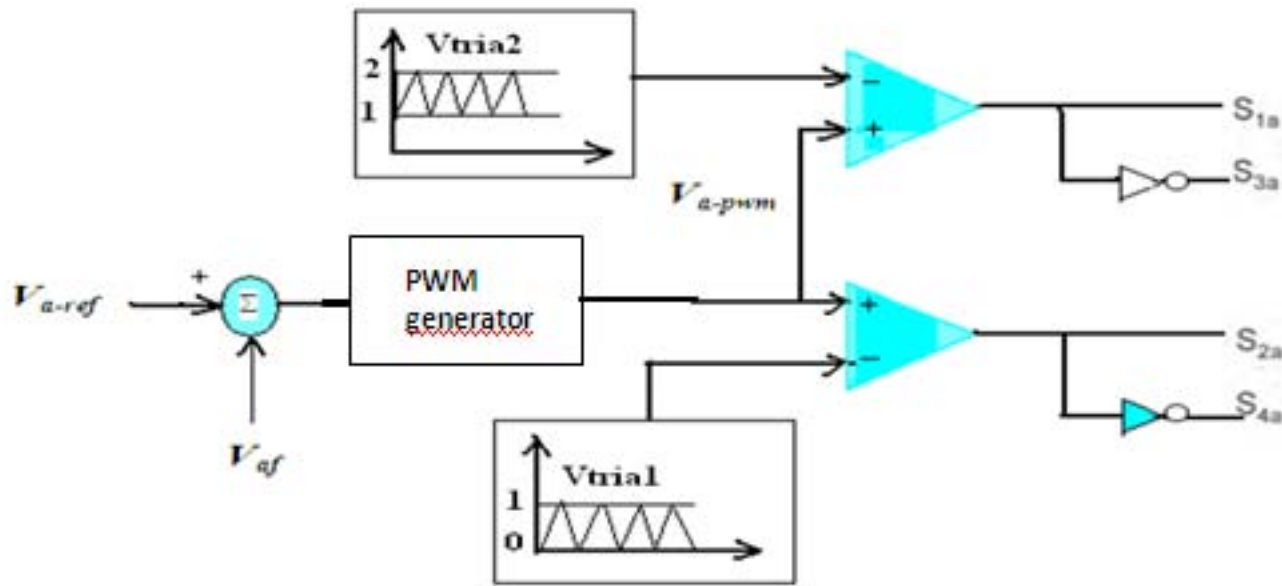
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Figure 7: Fig. 9 :Case 1 : 2 X + 1 2 (



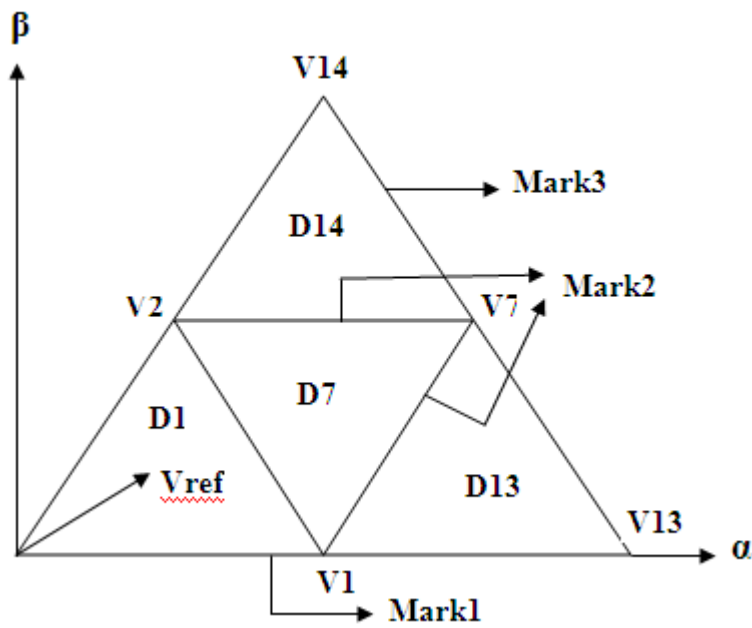
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Figure 8: Fig. 11 :



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Figure 9: Fig. 13 :



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Figure 10: Fig. 15 :

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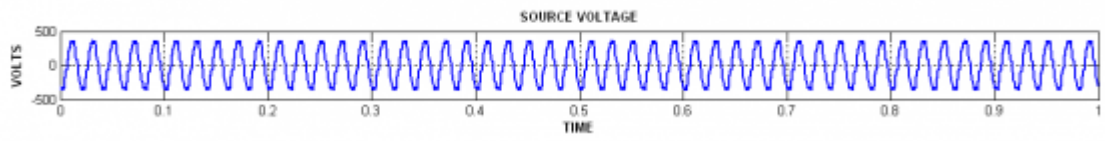


Figure 11: Fig. 17 :

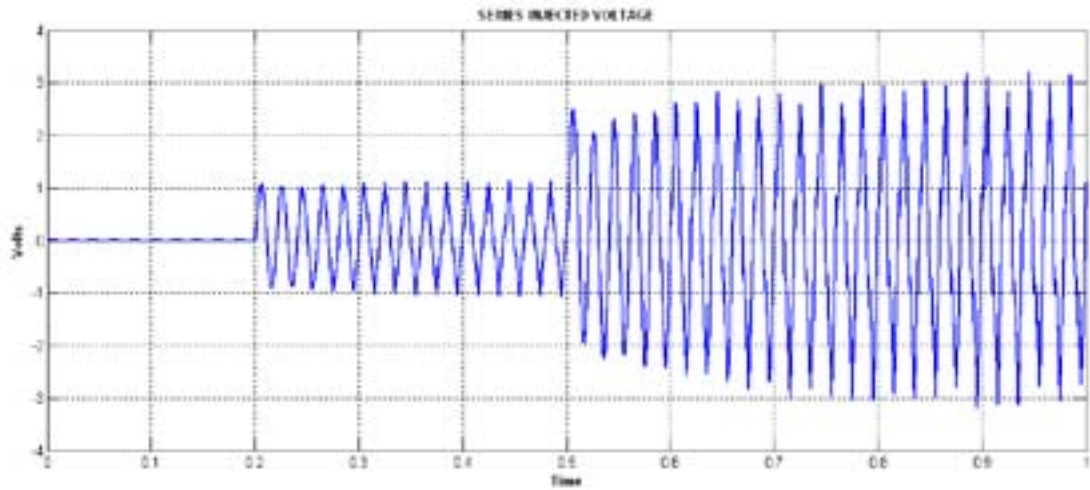


Figure 12:

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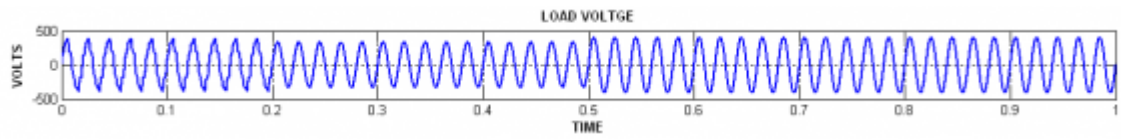


Figure 13: Fig. 18 :

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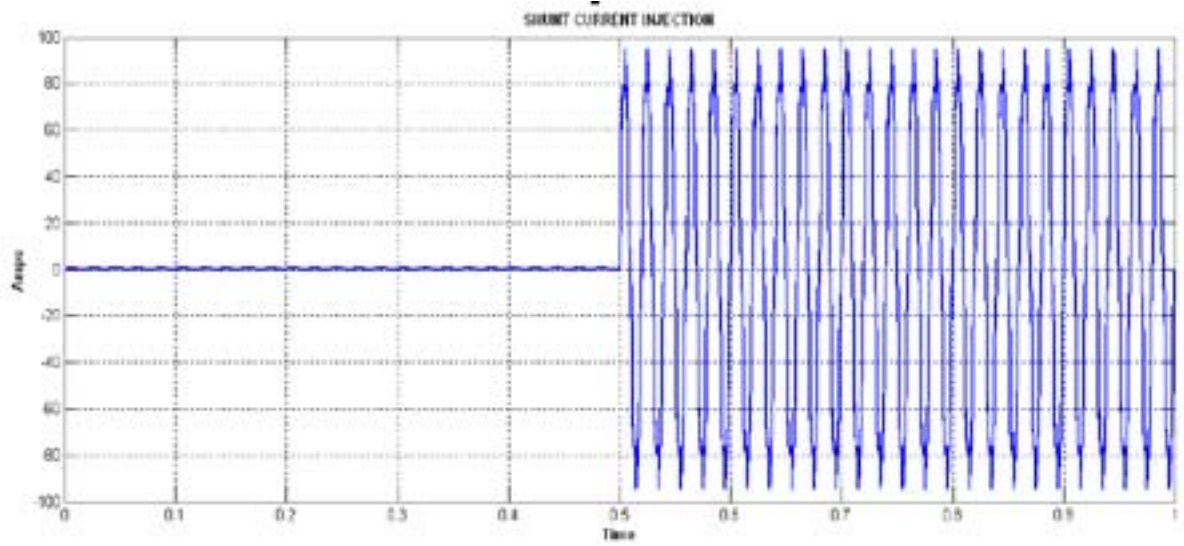


Figure 14: Fig. 19 :

SWITCHING STATES				OUTPUT VOLTAGE
S1a	S2a	S3a	S4a	Va
ON	ON	OFF	OFF	+Vdc/2
OFF	OFF	ON	ON	-Vdc/2
OFF	ON	ON	OFF	0

Figure 15: Table . I

115 FFT analysis of source current after connecting UPQC FFT analysis is carried out on the source current at  
 116 0.07sec before connecting UPQC and the THD is found to be 33.97%. In the second analysis, FFT is done at  
 117 0.6sec after connecting UPQC and measured THD is 0.61% The above results are shown in the form of graphs  
 118 for better understanding

119 The above table and graphs clearly show that the % THD of both load voltage and source current is less with  
 120 SVPWM when compared to SPWM and within the prescribed limits of IEEE -519.

## 121 .1 VI. Conclusion

122 The performance of three level UPQC has been evaluated using Sinusoidal Pulse Width Modulation and Space  
 123 Vector Pulse Width Modulation techniques. To prove the effective compensation by UPQC, harmonics are  
 124 deliberately injected into the source voltage and the UPQC has successfully reduced harmonics from load voltage  
 125 and source current. The %THD content in the load voltage and source current after compensation is very less  
 126 and comply with IEEE-519. The simulation results show that the Total Harmonic Distortion of the load voltage  
 127 after UPQC is put into operation is less in case of SVPWM compared to SPWM.

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