

Evaluation of Parametric Control for Machining with WEDM and Machinability Index

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Abstract

The present research work is intended to optimize the machining parameters for achieving high dimensional accuracy in wire electric discharge machining (WEDM). Experiments were designed and carried out to evaluate the best parametric setting which gives parameters like power, spark gap and corner radius using Inconel X-750 as workpiece material. These parameters are determined for a wide range of job thickness and mathematical correlations were developed for the parameters such as power and spark gap. Analysis of variance (ANOVA) is also performed to study the fitness. This procedure eliminates the need for repeated experiments which saves time and material unlike conventional machining process. The primary objective of the study is to find out the important and combination of one or more factors that influence the machining process in order to achieve the best power setting in turn machining current. Also, Machinability index of various materials which can be machined by WEDM is evaluated by referring to the present research work and literature review.

Index terms— wire electrical discharge machining, ferrous and non-ferrous materials, aviation materials, parameters, machinability index.

1 Introduction

Worldwide industry acceptance has brought revolutionary changes in bringing the Wire electrical discharge machines (WEDM) into the shop floors which is an unconventional production process thus manufacturing the components with a complex geometry.

The material is removed from a workpiece by creating a series of rapidly recurring electric current discharge (thousands of sparks) between the cutting tool and workpiece, immersed in a non-conductive fluid called dielectric.

The wire used for machining is also called as a tool/electrode and is made of copper, brass, tungsten or brass coated of diameter varying from 0.03 to 0.30mm.

A constantly moving wire fed from a spool is subjected to a high tension with the help of an advanced tension servo control mechanism shall results in producing precision components of extremely complex shape and desired profile.

The WEDM can be deployed to machine the materials that are hard to machine such as high strength and temperature resistive materials (HSTR). Also, the components manufactured out of Wire EDM would be free from the geometrical changes as there won't be any mechanical stresses developed during the machining. The dimensional accuracy can be achieved even in the case of machining the heat treated materials regardless of the hardness. Hard or difficult to machine materials are also can be machined using the WEDM.

The mechanical stresses that are developed during the machining process would be eliminated as there would not be any direct contact between workpiece and the tool. It may be observed that the material is eroded ahead of the wire travel.

The first commercially NC machine was built and introduced to the manufacturing industry in the late 1960s. The WEDM process was developed as a result of quest of a technique to replace the machined EDM electrode.

3 A) EXPERIMENTAL SET-UP

44 D.H. Dulebohn has automated the WEDM process and controlled the shape of the machined components with
45 the help of optical-line follower technique in 1974. The process has become very popular by the year 1975 and
46 by then the industry has good understanding and knowledge about various capabilities of WEDM. Later, it was
47 observed that there was rapid growth in deploying the WEDM machines in the manufacturing segment.

48 The first CNC EDM was fabricated in late 1970s which has brought a major evaluation of the machining
49 processes.

50 2 A

51 As a result, the wide range of capabilities of the WEDM process were significantly implemented for any
52 through hole machining owing to the wire, which has to pass through the component to be machined. The
53 WEDM applications includes Prototype production, die making, closed loop manufacturing, metal disintegration
54 machining, Extrusion Dies, Fixtures and Gauges, Form tools and inserts, Bio-Medical applications, Aerospace,
55 defense and electronic parts. Limited varieties of composites and ceramics also can be machined using WEDM.
56 Fig. ?? shows the schematic view of the process.

57 Figure1 : Wire electrical discharge machining Process WEDM removes material with the help of a storage
58 capacitor by releasing a series of discrete electrical discharges (transient sparks over a shorter duration). The
59 erosion takes place when the capacitor starts discharging an electrical current through an accurately positioned
60 and constantly moving wire (tool/electrode) and the workpiece (anode). A narrow gap is maintained between the
61 tool and cathode through an insulated medium (dielectric fluid). A microprocessor embedded with the WEDM
62 machine maintains a constant narrow gap varying from 25 to 50 microns between the electrode and workpiece.

63 When the wire approaches close to the workpiece, the controlled electrical discharges creates a concentrated
64 spark that helps melting down the required portion of material into vaporized tiny particles during the erosion
65 process.

66 The workpiece is totally submerged in dielectric fluid which would help in maintaining constant temperature
67 and also flushes away the debris after erosion. Flushing mechanism plays a vital role when there is a change in
68 thickness of the workpiece.

69 The flushing mechanism even aids in cooling down the workpiece after erosion and surrounding environment
70 handling huge temperature range of 10000°C. The volume of the material removed per spark may be 10-6 mm³
71 approximately.

72 WEDM does not require customized form or a shaped electrode as there is only a wire used as a tool which saves
73 investment of resources like cost, time and money. Unlike traditional machining, the WEDM process eliminates
74 use of different electrodes for rough and finish operations. Sometimes, the finish operation may demand multiple
75 passes along the profile/shape to be created.

76 WEDM can achieve exceptionally high dimensional accuracy as it uses a thin and continuous wire feeding
77 through the workpiece and enables the production of parts particularly a complex shape.

78 Surface finish quality depends on the amount of electrical discharge energy and also relates to the intensity
79 and duration of the spark plasma. Decrease in both pulse duration and discharge current may influence Surface
80 finish, cutting speed and MRR.

81 Machining Parameters influencing the WEDM process Discharge Current, Gap Voltage, Pulse parameters like
82 pulse frequency and duration, Conductivity, flow rate and flushing pressure of dielectric fluid, dielectric flushing
83 pressure, wire size, material, speed and tension, thickness, melting point, material of workpiece etc.,

84 3 a) Experimental Set-Up

85 The experimental studies were performed on a Wire EDM machine of make ULTRACUT 334.

86 A brass wire of 250 microns diameter is used as a tool-electrode with a wire tension of 70N at a velocity of
87 3.4 m/min. Inconel X-750 is used as a workpiece material for conducting the experimentation. As per DIN
88 160 standards, the preferred mechanical strength of the brass alloy wire opted for the experimentation is of 900
89 N/mm² with a composition of CuZn36.

90 Deionized water with a dielectric conductivity of a value of 38 mhos is used as a Dielectric medium for the
91 present study. A range of 30 to 90 Volts has been set as a gap voltage. The optimum values were obtained at 80
92 Volts.

93 Experimental investigation was done to find out the influence of the current with respect to the parameters
94 like varying workpiece thickness, spark gap and the geometry. Workpiece thickness of Inconel X-750 material
95 used was varying from 5 to 80mm material.

96 As shown in Fig. 2, an "L" shaped cut was performed to measure the corner radius with respect to the current
97 value and also another slot of 30mm length has been cut to measure the slot width. Series of experiments were
98 carried out varying the workpiece thickness starting from 5 to 80 mm with an increment of 2.5mm or 5mm as
99 convenient. A total of 20 experiments were conducted in the present research work.

100 Necessary care was taken to achieve high cutting speed with respect to varying current with a least wire
101 breakage. The variation of power, spark gap and corner radius with respect to change in thickness of workpiece
102 is discussed in this article to derive the best fit curve. Origin 8.0 software tool is being used for the study. The

103 mathematical equations are derived and statistical analysis ANOVA is also performed to calculate the coefficient
104 of variance, R2 and standard deviation in order to determine the fitness of the curve.

105 4 b) Results and Discussions

106 Fig. 3. describes the effect of variation in thickness with respect to the power. The increase in workpiece
107 thickness causes variation in power. It is also observed that the increase in workpiece thickness causes increase in
108 machining current for a specific set of machining conditions. This phenomenon reveals that the high amount of
109 energy required to machine higher workpiece thickness, the machining can be performed only when the current
110 is increased which involves high amount of power. However, the rate of power change is found decreasing with
111 increasing thickness. This may be due to the limitation of current carrying capacity of the wire electrode.

112 The plot is useful to determine suitable values like the minimum power required for machining the INCONEL
113 X-750 workpiece at given thickness with in working range of the select machine. Eqn. (1) Fig. 4 depicts the trend
114 of variation in spark gap with the increase in workpiece thickness. The plot shows that the spark gap increases
115 with increment in workpiece thickness. The increase in gap may be due to the spark jumping longer because
116 of high energy generated at high current values, is required to machine the job of higher thickness, though the
117 rate of change is proportionate with respect to the job thickness. The best fit curve is plotted and is carried out
118 the statistical analysis (ANOVA). The outcome of statistical analysis gives the value of R-Squared and standard
119 deviation as 0.9657 spark gap i.e., the cutting width to compute the MRR and determine the wire offset used
120 while generating a CNC part program and hence high accuracy can be achieved.

121 Figure ?? : Effect of workpiece thickness on corner radius Fig. ?? shows the variation in corner radius with
122 the increase in thickness of workpiece. The curve shows an increasing trend in corner radius with increase in
123 thickness of the workpiece. The plot shows that the spark gap increases with increment in workpiece thickness.
124 The increase in gap may be due to the spark jumping longer because of high energy generated at high current
125 values, is required to machine the job of higher thickness causing deeper cutting, though the rate of change is
126 proportionate with respect to the job thickness. The profile geometry/contour of the corner radius generated
127 can be similar to that of cross-section of the wire used for machining. From the plot, corner radius that can be
128 achieved can be predicted while machining a particular workpiece thickness at optimum cutting parameters. The
129 parameters can be set even for the required corner radius on a given job thickness from the database built while
130 optimizing the parameters.

131 5 c) Machinability Index

132 The data for machining 5mm thick workpieces of Mild steel, HSS, HC-HCr steel, En24 steel, Stainless steel,
133 Copper, Brass, Graphite, Tungsten-carbide and Titanium are adopted from the literature [4,5,[10][11][12], and
134 Inconel X-750 are considered from the present research work. The machinability index is calculated for all these
135 materials and tabulated as below.

136 6 CONCLUSION

137 The influence of machining parameters like Current and Workpiece thickness with respect to the accuracy criterion
138 such as cutting speed and spark gap are determined. A better control on machining accuracy can be achieved in
139 comparison with earlier researchers by controlling the primary parameter "current" in turn Power. The results
140 are useful in setting up the parameters required for accurate cuts on Inconel X-750 workpieces of any size ranging
141 between 5 and 80mm. The appropriate machining parameters can be chosen depends on the availability of wire-
142 electrodes. The mathematical relation developed and the plots are much more beneficial in estimating the spark
143 gap and also to achieve high cutting accuracy for any given workpiece thickness within the working range of the
144 select machine. The modern industrial applications like tool and die manufacturing units may make use of these
145 results in order to optimize the use of Wire EDM resources in more efficient manner than the past.

146 Student fraternity, Researchers, Manufacturing industry can refer the machinability index developed out of
147 this research to have an overall understanding about various challenges like the degree of difficulty or ease while
148 dealing with the machining of different materials.

149 The findings of the present work will open up new insights into the fundamental and applied researchers in
150 the WEDM area for better understanding of the technology, and also useful to the manufacturing industry and
151 tool rooms for taking up a quantum leap from the present day needs of machining of the

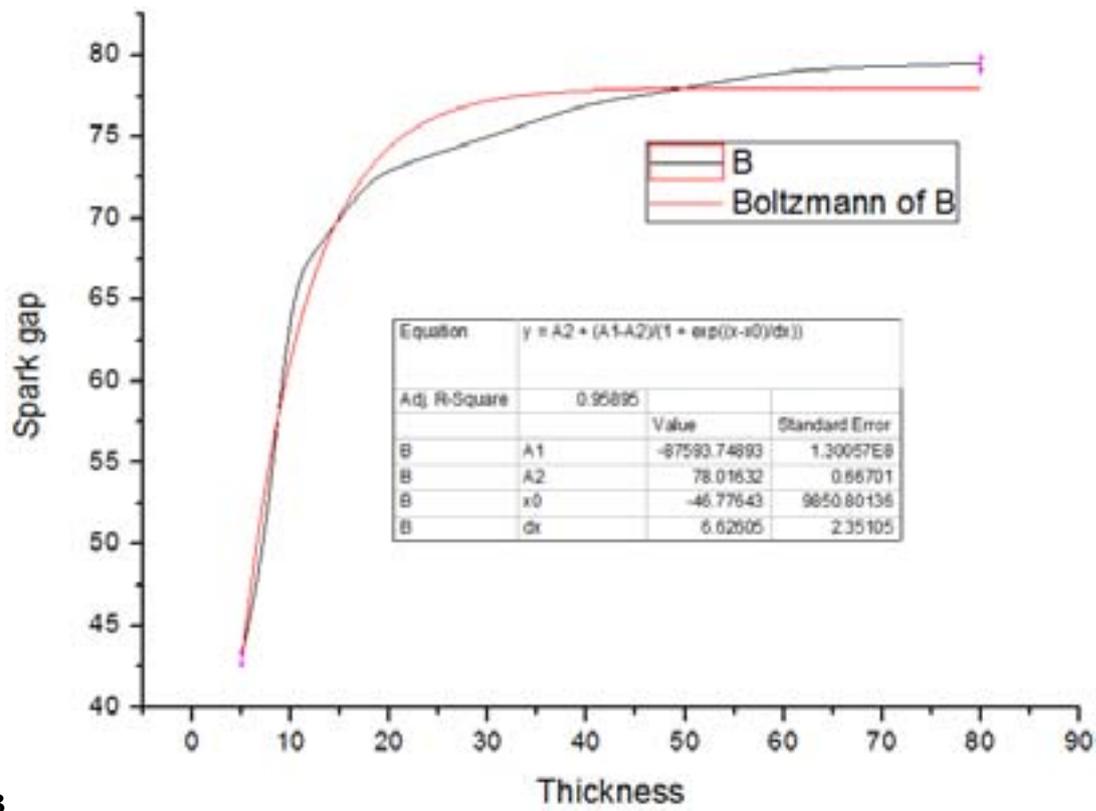


Figure 1:



2

Figure 2: Figure 2 :



3

Figure 3: Figure 3 :

1

S.No.	Material, (5mm thickness)	Cutting speed, (mm/min)	Machinability Index
1	Mild steel	3.10	1.000
2	HSS	3.44	1.207
3	HC-HCr steel	2.20	0.752
4	EN24 steel	2.67	0.827
5	Stainless steel	3.00	0.985
6	Copper	2.80	1.253
7	Brass	7.80	2.560
8	Graphite	1.60	0.616
9	Tungsten carbide	1.40	0.474
10	Titanium	4.11	1.412
11	Inconel X-750	3.84	1.324

II.

Figure 4: Table 1 :

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[Amitesh and Jatinder (2012)] ‘An investigation into the machining characteristics of Nimonic 80A using CNC WIRE-EDM’. Goswami Amitesh , Kumar Jatinder . *International Journal of Advanced Engineering Technology* 0976-3945 IJAET. January-March, 2012. p. .

[Kamal Jangra Sandeep Grover Felix T. S. Chan Aman Aggarwal. (2011)] ‘Digraph and matrix method to evaluate the machinability of tungsten carbide composite with wire EDM’. 10.1007/s00170-011-3234-5. *Int J Adv Manuf Technol* Kamal Jangra & Sandeep Grover & Felix T. S. Chan & Aman Aggarwal. (ed.) February 2011. Springer-Verlag London Limited.

[EDM machinability and frictional behavior of ZrO₂-WC composites International Journal of Advances Manufacturing Technology ‘EDM machinability and frictional behavior of ZrO₂-WC composites’. *International Journal of Advances Manufacturing Technology* Springer. 41 p. .

[Ch et al. (2009)] ‘Evaluation of Optimal Parameters for machining Brass with Wire-cut EDM’. V S Ch , Mmm Parameswara Rao , Sarcar . *Journal of Scientific and Industrial Research* 0022-4456. Jan-2009. 68 (1) p. .

[S V Subrahmanyam and Sarcar (2013)] ‘Evaluation of Optimal Parameters for machining with Wire-cut EDM Using Grey-Taguchi Method’. M M M S V Subrahmanyam , Sarcar . *International Journal of Scientific and Research Publications* 2250-3153. March 2013. 3 (3) .

[Sanchez et al. ()] ‘On the influence of cutting speed limitation on the accuracy of wire-EDM corner-cutting’. J A Sanchez , J L Rodil , A Herrero , L N Lopez De Lacalle , A Lamikiz . *Journal of material processing technology* 2007. Elsevier. 182 p. .

[Kousoulidou and Dimaratos ()] ‘Optimizing the machining characteristics of Nimonic 80A using wire-cut EDM’. Marina Kousoulidou , Athanasios Dimaratos . *Rev. Téc. Ing. Univ. Zulia* 2014. 37 p. .

[Sivanaga Malleswara Rao and Parameswara Rao (2013)] ‘Parametric analysis for machining HSS by WEDM-development of Mathematical Correlations and statistical analysis’. S Sivanaga Malleswara Rao , Ch V S Parameswara Rao . *IJ-ETA-ETS* Feb 2013. p. .

[Sivanaga Malleswara Rao and Parameswara Rao (2013)] ‘Parametric Evaluation for Machining Die-Steel with WEDM’. S Sivanaga Malleswara Rao , Ch V S Parameswara Rao . *International Journal of Scientific and Research Publications* 2250-3153. April 2013. 3 (4) p. .

[Rao et al. (2014)] P Rao , Dr Chvs Parameshwara Rao , Dr K Ravindra . *Experimental studies on parametric influence on machining of Titanium with WEDM*, May-2014. 2 p. . (IJETR edition)

[Levy (1990)] ‘WEDM Machinability Comparison of Different steel grades’. Maggi G N F Levy . *Annals of CIRP* January 1990.

[Aspinwall et al. ()] ‘Workpiece surface roughness and integrity after WEDM of Ti-6Al-4V and Inconel 718 using minimum damage generator technology’. D K Aspinwall , S L Soo , A E Berrisford , G Walder . *CIRP Annals-Manufacturing Technology* 2008. Elsevier. 57 p. .