

# Optimal Power Flow using a hybrid Particle Swarm Optimizer with Moth Flame Optimizer

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## Abstract

At present, power system operation, control, Management becomes very complex due to continuously increasing demand. Flexible AC Transmission System (FACTS) controllers are used to increase power transfer capability of the transmission lines closer to their limits. This paper proposed a methodology to solve Optimal Power Flow (OPF) problem in the presence of Thyristor Controlled Series Capacitor (TCSC) while satisfying system operating and practical constraints. A novel cost objective function is formulated by combining investment cost of the TCSC with the conventional fuel cost function. The proposed methodology is tested on standard IEEE-14 bus test system with supporting results.

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*Index terms*— economic dispatch, ramp-rate limit, prohibited operating zones, TCSC, investment cost.

## 1 Introduction

At the present time, The Optimal power flow (OPF) is a very significant problem and most focused objective for power system planning and operation [1]. The OPF is the elementary tool which permits the utilities to identify the economic operational and secure states in the system [2]. The OPF problem is one of the utmost operating desires of the electrical power system [3]. The prior function of OPF problem is to evaluate the optimum operational state for Bus system by minimizing each objective function within the limits of the operational constraints like equality constraints and inequality constraints [4]. Hence, the optimal power flow problem can be defined as an extremely non-linear and non-convex multimodal optimization problem [5].

From the past few years too many optimization techniques were used for the solution of the Optimal Power Flow (OPF) problem. Some traditional methods used to solve the proposed problem have some limitations like converging at local optima and so they are not suitable for binary or integer problems or to deal with the lack of convexity, differentiability, and continuity [6]. Hence, these techniques are not suitable for the actual OPF situation. All these limitations are overcome by metaheuristic optimization methods. Some of these methods are [7][8][9][10]: genetic algorithm (GA) [11], hybrid genetic algorithm (HGA) [12], enhanced genetic algorithm (EGA) [13][14], differential evolution algorithm (DEA) [15][16], artificial neural network (ANN) [17], particle swarm optimization algorithm (PSO) [18], tabu search algorithm (TSA) [19], gravitational search algorithm (GSA) [20], biogeography based optimization (BBO) [21], harmony search algorithm (HSA) [22], krill herd algorithm (KHA) [23], cuckoo search algorithm (CSA) [24], ant colony algorithm (ACO) [25], bat optimization algorithm (BOA) [26], Ant-lion optimizer (ALO) [27][28] and Multi-Verse optimizer (MVO) [29].

In the present work, a newly introduced hybrid meta-heuristic optimization technique named Hybrid Particle Swarm Optimization-Moth Flame Optimizer (HPSO-MFO) is applied to solve the Optimal Power Flow problem. HPSO-MFO comprises of best characteristic of both Particle Swarm Optimization [30] and Moth-Flame Optimizer [31][32] algorithm. The capabilities of HPSO-MFO are finding the global solution, fast convergence rate due to the use of roulette wheel selection, can handle continuous and discrete optimization problems.

According to No Free Lunch Theorem [27,29,30], particular meta-heuristic algorithm is not best for every problem. So, we considered HPSO-MFO for continuous optimal power flow problem based on No Free Lunch Theorem. In this work, the HPSO-MFO is presented to standard IEEE-30 bus test system [33] to solve the OPF

[34-37] problem. There are five objective cases considered in this paper that have to be optimize using HPSO-MFO technique are Fuel Cost Reduction, Voltage Stability Improvement, Voltage Deviation Minimization, Active Power Loss Minimization and Reactive Power Loss Minimization. The results show the optimal adjustments of control variables in accordance with their limits. The results obtained using HPSO-MFO technique has been compared with Particle Swarm Optimisation (PSO) and Moth Flame Optimizer (MFO) techniques. The results show that HPSO-MFO gives better optimization values as compared to other methods which prove the effectiveness of the proposed algorithm.

This paper is summarized as follow: After the first section of the introduction, the second section concentrates on concepts and key steps of standard PSO and MFO techniques and the proposed Hybrid PSO-MFO technique. The third section presents the formulation of Optimal Power Flow problem. Next, we apply HPSO-MFO to solve OPF problem on IEEE-30 bus system in order to optimize the operating conditions of the power system. Finally, the results and conclusion are drawn in the last section.

## 2 II. Standard PSO and Standard MFO a) Particle Swarm Optimization

The particle swarm optimization algorithm (PSO) was discovered by James Kennedy and Russell C. Eberhart in 1995 [30]. This algorithm is inspired by the simulation of social psychological expression of birds and fishes. PSO includes two terms  $v_{ij}(t+1)$  and  $x_{ij}(t+1)$ . Position and velocity are updated over the course of iteration from these mathematical equations:

$$v_{ij}(t+1) = w \cdot v_{ij}(t) + c_1 \cdot r_1 \cdot (p_{best} - x_{ij}(t)) + c_2 \cdot r_2 \cdot (g_{best} - x_{ij}(t))$$

$$x_{ij}(t+1) = x_{ij}(t) + v_{ij}(t+1)$$

Where  $w$  is the inertia weight,  $c_1$  and  $c_2$  are the cognitive and social coefficients respectively,  $r_1$  and  $r_2$  are random numbers between 0 and 1.  $p_{best}$  and  $g_{best}$  are the personal and global best positions.

### 3 b) Moth-Flame Optimizer

A novel nature-inspired Moth-Flame optimization algorithm [31] based on the transverse orientation of Moths in space. Transverse orientation for navigation uses a constant angle by Moths with respect to Moon to fly in straight direction in night. In MFO algorithm that Moths fly around flames in a Logarithmic spiral way and finally converges towards the flame. Spiral way expresses the exploration area and it guarantees to exploit the optimum solution [31]:

Moth-Flame optimizer is first introduced by Seyedali Mirjalili in 2015 [31]. MFO is a populationbased algorithm; we represent the set of moths in a matrix:  $M$  of size  $n \times d$ .

Where  $n$  represents a number of moths and  $d$  represents a number of variables (dimension). For all the moths, we also assume that there is an array for storing the corresponding fitness values as follows:

Where  $n$  is the number of moths. Note that the fitness value is the return value of the fitness (objective) function for each moth. The position vector (first row in the matrix  $M$  for instance) of each moth is passed to the fitness function and the output of the fitness function is assigned to the corresponding moth as its fitness function (OM 1 in the matrix  $OM$  for instance).

Other key components in the proposed algorithm are flames. We consider a matrix similar to the moth matrix [31]:  $F$  of size  $n \times d$ .

Where  $n$  shows a number of moths and  $d$  represents a number of variables (dimension). We know that the dimension of  $M$  and  $F$  arrays are equal. For the flames, we also assume that there is an array for storing the corresponding fitness values [31]:  $OF$  of size  $n \times 1$ .

Here, it must be noted that moths and flames both are solutions. The variance among them is the manner we treat and update them, in the iteration. The moths are genuine search agents that move all over the search space while flames are the finest location of moths that achieves so far. Therefore, every moth searches around a flame and updates it in the case of discovering an enhanced solution. With this mechanism, a moth never loses its best solution.

The MFO algorithm is three rows that approximate the global solution of the problems defined like as follows [31]:

$I$  is the function that yields an uncertain population of moths and corresponding fitness values. The methodical model of this function is as follows:

The  $P$  function, which is the main function, expresses the moths all over the search space. This function receives the matrix of  $M$  and takes back its updated one at every time with each iteration.

The  $T$  returns true and false according to the termination Criterion satisfaction.

104 In order to mathematical model this behavior, we change the location of each Moth regarding a flame with  
 105 the following equation:

$$106 \quad (i, j) M S M F = (12)$$

107 Where  $i$  indicate the moth,  $j$  indicates the flame and  $S$  is the spiral function.

108 In this equation flame  $FL_n, d$  (search agent \* dimension) of equation (6) modifies the moth matrix of equation  
 109 (12).

110 Considering these points, we define a log (logarithmic scale) spiral for the MFO algorithm as follows [31]:  
 111  $(i, j) * \cos(2\pi b t) i j j S M F D e t F = + (13)$

112 Where:  $i D$  expresses the distance of the moth for the  $j$  th flame,  $b$  is a constant for expressing the shape of  
 113 the log (logarithmic) spiral, and  $t$  is a random value in  $[-1, 1]$ .  $i j i D F M = ? (14)$

114 Where:  $i M$  represent the  $i$  th moth,  $F j$  represents the  $j$  th flame, and where  $i D$  expresses the path length  
 115 of the  $i$  th moth for the  $j$  th flame. The no. of flames are adaptively reduced with the iterations. We use the  
 116 following formulation:  $l * N \text{ flame no round } N l T ? ? ? = ? ? ? ? (15)$

117 Where  $l$  is the present number of iteration,  $N$  is the maximum number of flames, and  $T$  shows the maximum  
 118 number of iterations.  $O M F O O t O \text{ Quick sort } O \text{ position update} = + 2 2 ( ) ( ( * ) ) ( ) O M F O O t n n d O$   
 119  $t n t n d = + = + ( ) ( ) ( ) ( )$

120 Where  $n$  shows a number of moths,  $t$  represents maximum no. of iterations, and  $d$  represents no. of variables.

## 121 4 c) The Hybrid PSO-MFO Algorithm

122 The drawback of PSO is the limitation to cover small search space while solving higher order or complex design  
 123 problem due to constant inertia weight. This problem can be tackled with Hybrid PSO-MFO as it extracts the  
 124 quality characteristics of both PSO and MFO. Moth-Flame Optimizer is used for exploration phase as it uses  
 125 logarithmic spiral function so it covers a broader area in uncertain search space. Because both of the algorithms  
 126 are randomization techniques so we use term uncertain search space during the computation over the course of  
 127 iteration from starting to maximum iteration limit. Exploration phase means the capability of an algorithm to  
 128 try out a large number of possible solutions. The position of particle that is responsible for finding the optimum  
 129 solution to the complex non-linear problem is replaced with the position of Moths that is equivalent to the  
 130 position of the particle but highly efficient to move solution towards optimal one. MFO directs the particles  
 131 faster towards optimal value, reduces computational time. As we know that that PSO is a well-known algorithm  
 132 that exploits the best possible solution for its unknown search space. So the combination of best characteristic  
 133 (exploration with MFO and exploitation with PSO) guarantees to obtain the best possible optimal solution of  
 134 the problem that also avoids local stagnation or local optima of the problem.

135 A set of Hybrid PSO-MFO is the combination of separate PSO and MFO. Hybrid PSO-MFO merges the best  
 136 strength of both PSO in exploitation and MFO in exploration phase towards the targeted optimum solution.  $1 1$   
 137  $1 2 2 ( ) ( ) t t t t t t i j v w v c R \text{ Moth Pos } X c R \text{ Gbest } X + = + ? + (17)$

138 III.

## 139 5 Optimal Power Flow Problem Formulation

140 As specified before, OPF is the optimized problem of power flow that provides the optimum values of independent  
 141 variables by optimizing a predefined objective function with respect to the operating bounds of the system [1].  
 142 The OPF problem can be mathematically expressed as a non-linear constrained optimization problem as follows  
 143 [1]: Minimize  $f(a,b)$  (18) Subject to  $s(a,b)=0$  (19)

## 144 6 i. Control variables

145 The control variables should be adjusted to fulfill the power flow equations. For the OPF problem, the set for  
 146 control variables can be formulated as [1], [4]:  $2 1 1 1 [ ] ,$   
 147  $, NTr NGen NGen NCom T G G G G C C P P V V Q b Q T T = ? ? ? ? (21)$

148 Where,  $G P$  = Real power output at the PV(Generator) buses excluding at the slack (Reference) bus.  $G V$  =  
 149 Magnitude of Voltage at PV (Generator) buses.  $C Q$  = shunt VAR compensation.

150  $T$  = tap settings of the transformer.

151  $NGen, NTr, NCom$  = No. of generator units, No. of tap changing transformers and No. of shunt VAR  
 152 compensation devices, respectively. The control variables are the decision variables of the power system which  
 153 could be adjusted as per the requirement.

## 154 7 ii. State variables

155 There is a need of variables for all OPF formulations for the characterization of the Electrical Power Engineering  
 156 state of the system. So, the state variables can be formulated as [1], [4]:  $1 1 1 1 [ ] [ , , , NLB NGen T 1 1 L L G G$   
 157  $G Nline P V V Q Q S S a = ? ? ? (22)$

158 Where,

## 8 b) Constraints

There are two OPF constraints named inequality and equality constraints. These constraints are explained in the sections given below.

### 9 i. Equality constraints

The physical condition of the power system is described by the equality constraints of the system. These equality constraints are basically the power flow equations which can be explained as follows [1], [4].

### 10 a. Real power constraints

The real power constraints can be formulated as follows: 
$$P_i = \sum_{j \in N} G_{ij} V_i V_j \cos(\theta_{ij} - \theta_i) - \sum_{j \in N} B_{ij} V_i V_j \sin(\theta_{ij} - \theta_i) + P_{gi} - P_{li} \quad (23)$$

Where,  $\theta_{ij}$  is the phase angle of voltage between buses  $i$  and  $j$ .  $NB$  = total No. of buses,  $G P$  = real power output,  $G Q$  = reactive power output,  $ij Y G jB = +$  shows the susceptance and conductance between bus  $i$  and  $j$ , respectively,  $ij Y$  is the mutual admittance between buses  $I$  and  $j$ .

### 11 ii. Inequality constraints

The boundaries of power system devices together with the bounds created to surety system security are given by inequality constraints of the OPF [4], [5].

### 12 a. Generator constraints

For all generating units including the reference bus: voltage magnitude, real power and reactive power outputs should be constrained within its minimum and maximum bounds as given below [27]: 
$$V_{min} \leq V_i \leq V_{max} \quad (25)$$
 
$$P_{min} \leq P_i \leq P_{max} \quad (26)$$
 
$$Q_{min} \leq Q_i \leq Q_{max} \quad (27)$$

b. Transformer constraints Tap settings of transformer should be constrained inside their stated minimum and maximum bounds as follows [27]: 
$$T_{min} \leq T_i \leq T_{max} \quad (28)$$

c. Shunt VAR compensator constraints Shunt VAR compensation devices need to be constrained within its minimum and maximum bounds as given below [27]: 
$$C_{min} \leq C_i \leq C_{max} \quad (29)$$

d. Security constraints These comprise the limits of a magnitude of the voltage at PQ buses and loadings on the transmission line. Voltage for every PQ bus should be limited by their minimum and maximum operational bounds. Line flow over each line should not exceed its maximum loading limit. So, these limitations can be mathematically expressed as follows [27]: 
$$L_{min} \leq L_i \leq L_{max} \quad (30)$$
 
$$i = 1, \dots, N_{line} \quad (31)$$

The control variables are self-constraint. The inequality constrained of state variables comprises the magnitude of PQ bus voltage, active power production at reference bus, reactive power production and loadings on line may be encompassed into an objective function in terms of quadratic penalty terms. In which, the penalty factor is multiplied by the square of the indifference value of state variables and is included in the objective function and any impractical result achieved is declined [27].

Penalty function may be mathematically formulated as follows: 
$$P = \sum_{i=1}^N \lambda_i (V_i - V_{lim})^2 + \sum_{i=1}^N \mu_i (P_i - P_{lim})^2 + \sum_{i=1}^N \nu_i (Q_i - Q_{lim})^2 + \sum_{i=1}^N \rho_i (T_i - T_{lim})^2 + \sum_{i=1}^N \sigma_i (C_i - C_{lim})^2 + \sum_{i=1}^N \tau_i (L_i - L_{lim})^2 \quad (32)$$

Where,  $\lambda, \mu, \nu, \rho, \sigma, \tau$ , The reactive power constraints can be formulated as follows: 
$$-U \leq S_i \leq U \quad (33)$$

; upper upper lim lower lower  $U U U U U U = ? > ? < ?$  (33)  
IV.

## 13 Application and Results

The PSO-MFO technique has been implemented for the OPF solution for standard IEEE 30bus test system and for a number of cases with dissimilar objective functions. The used software program is written in MATLAB R2014b computing surroundings and used on a 2.60 GHz i5 PC with 4 GB RAM. In this work the HPSO-MFO population size is selected to be 40.

## 14 a) IEEE 30-bus test system

With the purpose of elucidating the strength of the suggested HPSO-MFO technique, it has been verified on the standard IEEE 30-bus test system as displays in fig. 2. The standard IEEE 30-bus test system selected in this work has the following features [6] In addition, generator cost coefficient data, the line data, bus data, and the upper and lower bounds for the control variables are specified in [33].

213 In given test system, five diverse cases have been considered for various purposes and all the acquired outcomes  
 214 are given in Tables 3, 5, 7, 9, 11. The very first column of this tables denotes the optimal values of control variables  
 215 found where:

216 -P G1 through P G6 and V G1 through V G6 signifies the power and voltages of generator 1 to generator 6.  
 217 -T 4-12 , T 6-9 , T 6-10 and T 28-27 are the transformer tap settings comprised between buses 4-12, 6-9, 6-10  
 218 and 28-27.-Q C10 , Q C12 , Q C15 , Q C17 , Q C20 , Q C21 , Q C23 , Q C24 and Q C29

219 denote the shunt VAR compensators coupled at buses 10, 12, 15, 17, 20, 21, 23, 24 and 29. Further, fuel cost  
 220 (\$/hr), real power losses (MW), reactive power losses (MVAR), voltage deviation and Lmax represent the total  
 221 generation fuel cost of the system, the total real power losses, the total reactive power losses, the load voltages  
 222 deviation from 1 and the stability index, respectively. Other particulars for these outcomes will be specified in  
 223 the next sections.

224 The control parameters for HPSO-MFO, MFO, PSO used in this problem are given in table 1.

225 In table 1, no. of variables (dim) shows the six no. of generators used in the 30 bus system. It gives the  
 226 optimization values for different cases as they depends on the decision variables. In all 5 cases, results are the  
 227 average value obtained after 10 number of runs. The very common OPF objective that is generation fuel cost  
 228 reduction is considered in the case 1. Therefore, the objective function Y indicates the complete fuel cost of total  
 229 generating units and it is calculated by following equation [1]:1 (\$ / ) NGen i i Y f hr = = ? (34)

230 Where, i f is the total fuel cost of th i generator.

231 i f , may be formulated as follow: 2 which displays that the results obtained by PSO-MFO are better than the  
 232 other methods. The optimal values of control variables obtained by different algorithms for case 1 are specified  
 233 in Table 3. By means of the same settings i.e. control variables boundaries, initial conditions and system data,  
 234 the results achieved in case 1 with the PSO-MFO technique are compared to some other methods and it display  
 235 that the total fuel cost is greatly reduced compared to the initial case [6]. Quantitatively, it is reduced from  
 236 901.951\$/hr to 799.056\$/hr. Case 2: Voltage profile improvement Bus voltage is considered as most essential and  
 237 important security and service excellence indices [6]. Here the goal is to reduce the fuel cost and increase voltage  
 238 profile simultaneously by reducing the voltage deviation of PQ (load) buses from the unity 1.0 p.u.

## 239 15 Fig. 3: Fuel cost variations with different algorithms

240 Hence, the objective function may be formulated by following equation [4]:cost voltage deviation Y Y wY ? = +  
 241 (36)

242 Where, w is an appropriate weighting factor, to be chosen by the user to offer a weight or importance to each  
 243 one of the two terms of the objective function. cos 1 NGen t i i Y f = = ? (37) \_1 | 1.0 | NGen voltage deviation  
 244 i i Y V = = ? ? (38)

245 The variation of voltage deviation with different algorithms over iterations is sketched in fig. ?? . It  
 246 demonstrates that the suggested method has good convergence characteristics. The statistical values of voltage  
 247 deviation obtained with different methods are shown in table 4 which display that the results obtained by PSO-  
 248 MFO are better than the other methods excluding GSA method. The optimal values of control variables obtained  
 249 by different algorithms for case 2 are specified in Table 5. By means of the same settings the results achieved  
 250 in case 2 with the PSO-MFO technique are compared to some other methods and it display that the voltage  
 251 deviation is greatly reduced compared to the initial case [6]. It has been made known that the voltage deviation  
 252 is reduced from 1.1496 p.u. to 0.1056p.u. using PSO-MFO technique.GSA [2] gives better result than the HPSO-  
 253 MFO method only in case of voltage deviation among five cases. Due to No Free Lunch (NFL) theorem proves  
 254 that no one can propose an algorithm for solving all optimization problems. This means that the success of an  
 255 algorithm in solving a specific set of problems does not guarantee solving all optimization problems with different  
 256 type and nature. NFL makes this field of study highly active which results in enhancing current approaches  
 257 and proposing new meta-heuristics every year. This also motivates our attempts to develop a new Hybrid meta-  
 258 heuristic for solving OPF Problem. Case 3: Voltage stability enhancement Presently, the transmission systems  
 259 are enforced to work nearby their safety bounds, because of cost-effective and environmental causes. One of the  
 260 significant characteristics of the system is its capability to retain continuously tolerable bus voltages to each node  
 261 beneath standard operational environments, next to the rise in load, as soon as the system is being affected by  
 262 disturbance. The unoptimized control variables may cause increasing and unmanageable voltage drop causing  
 263 a tremendous voltage collapse [6]. Hence, voltage stability is inviting ever more attention. By using various  
 264 techniques to evaluate the margin of voltage stability, Glavitch and Kessel have introduced a voltage stability  
 265 index called L-index depends on the viability of load flow equations for every node ??[34]. The L-index of a  
 266 bus shows the probability of voltage collapse circumstance for that particular bus. It differs between 0 and 1  
 267 equivalent to zero load and voltage collapse, respectively.

268 For the given system with NB, N Gen and NLB buses signifying the total no. of buses, the total no. of  
 269 generator buses and the total no. of load buses, respectively. The buses can be distinct as PV (generator) buses  
 270 at the head and PQ (load) buses at the tail as follows [4]:[ ] L L LL LG L bus G G GL GG G I V Y Y V Y I V  
 271 Y Y V = = ? (39)

272 Where, LL Y , LG Y , GL Y and GG Y are co-matrix of bus Y . The subsequent hybrid system of equations  
 273 can be expressed as:[ ] L L LL LG L G G GL GG G H I V V V I H H I H H = = ? ? ? ? ? ? ? ? ? ? ? ? ? ? ? ?  
 274 ? ? ? ? ? ? ? ? ? (40)

275 Where matrix H is produced by the partially inverting of bus The matrix H is given by: [ ]1 LL LL LG LL  
 276 LL GL LL GG GL LL LG Z Z Y H Z Y Y Z Y Y Z Y ? ? ? ? = = ? ? ? ? (41)

277 Hence, the L-index denoted by j L of bus j is represented as follows:1 1 i j LG i j ji NGen v L H v = = ? ?  
 278 j=1,2?,NL(42)

279 Hence, the stability of the whole system is described by a global indicator max L which is given by [6], max  
 280 max( )j L L = j=1,2?,NL(43)

281 The system is more stable as the value of max L is lower.

282 The voltage stability can be enhanced by reducing the value of voltage stability indicator L-index at every bus  
 283 of the system. [6]. Thus, the objective function may be given as follows:cos \_\_\_t voltage Stability Enhancement  
 284 Y Y wY = +(44)

285 Where,cos 1 NGen t i i Y f = = ? (45) max \_\_\_voltage stability enhancement Y L = (46)

286 The variation of the Lmax index with different algorithms over iterations is presented in fig. 4. The statistical  
 287 results obtained with different methods are shown in table 6 which display that PSO-MFO method gives better  
 288 results than the other methods. The optimal values of control variables obtained by different algorithms for case  
 289 3 are given in Table 7. After applying the PSO-MFO technique, it appears from Table 7 that the value of Lmax  
 290 is considerably decreased in this case compared to initial [6] from 0.1723 to 0.1126. Thus, the distance from  
 291 breakdown point is improved.

## 292 16 Case 4: Minimization of active power transmission losses

293 In the case 4 the Optimal Power Flow objective is to reduce the active power transmission losses, which can be  
 294 represented by power balance equation as follows [6]: 9. By means of the same settings the results achieved in  
 295 case 4 with the PSO-MFO technique are compared to some other methods and it display that the real power  
 296 transmission losses are greatly reduced compared to the initial case [6]

## 297 17 Case 5: Minimization of reactive power transmission losses

298 The accessibility of reactive power is the main point for static system voltage stability margin to support the  
 299 transmission of active power from the source to sinks [6].

300 Thus, the minimization of VAR losses are given by the following expression:1 1 i i Gi Di NGen NGen NGen i  
 301 i i J Q Q Q = = = = ? ? ? ? (48)

302 It is notable that the reactive power losses are not essentially positive. The variation of reactive power losses  
 303 with different methods shown in fig. 6. It demonstrates that the suggested method has good convergence  
 304 characteristics. The statistical values of reactive power losses obtained with different methods are shown in table  
 305 10 which display that the results obtained by hybrid PSO-MFO method are better than the other methods.  
 306 The optimal values of control variables obtained by different algorithms for case 5 are given in Table 11. It is  
 307 shown that the reactive power losses are greatly reduced compared to the initial case [6] from -4.6066 MVAR  
 308 to -25.335MVAR using hybrid PSO-MFO method. Table 12 show the comparison of elapsed time taken by the  
 309 different methods to optimize the different objective cases. The comparison shows that the time taken by all  
 310 three algorithms is not same which indicates the different evaluation strategy of different methods. V.

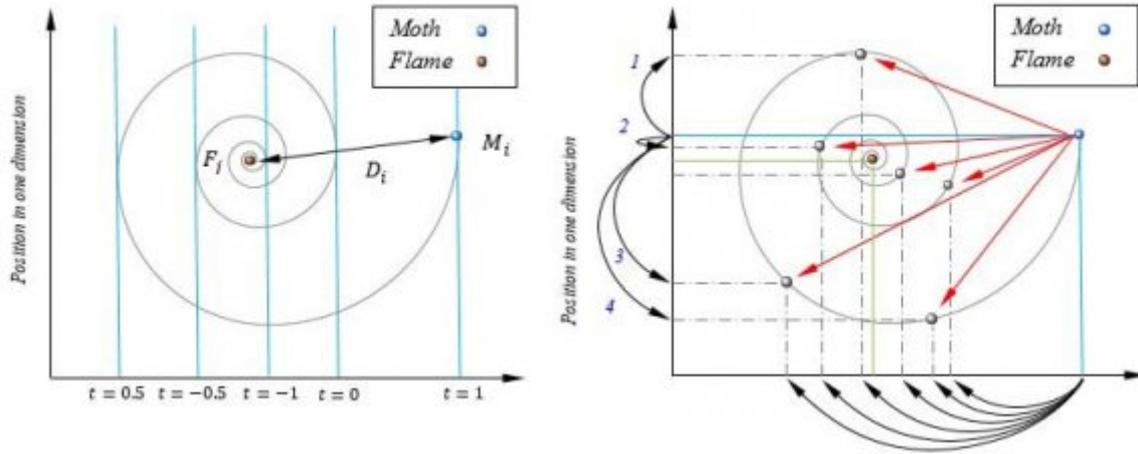
## 311 18 Robustness Test

312 In order to check the robustness of the HPSO-MFO for solving continues Optimal Power Flow problems, 10 times  
 313 trials with various search agents for cases Case 1, Case 2, Case 3, Case 4 and Case 5. Table 2, Table 3, Table 4,  
 314 Table 5, Table 6, Table 7, Table 8, Table 9, Table 10 and Table 11 presents the statistical results achieved by the  
 315 HPSO-MFO, MFO and PSO algorithms for OPF problems for various cases. From these tables, it is clear that  
 316 the optimum objective function values obtained by HPSO-MFO are near to every trial and minimum compare  
 317 to MFO and PSO algorithms. It proves the robustness of hybrid PSO-MFO algorithm (HPSO-MFO) to solve  
 318 OPF problem.

## 319 19 VI.

## 320 20 Conclusion

321 Particle Swarm Optimization-Moth Flame Optimizer (PSO-MFO), Moth Flame Optimizer and Particle Swarm  
 322 Optimization Algorithm are successfully applied to standard IEEE 30-bus test systems to solve the optimal power  
 323 flow problem for the various types of cases. The results give the optimal settings of control variables with different  
 324 methods which demonstrate the effectiveness of the different techniques. The solutions obtained from the hybrid  
 325 PSO-MFO method approach has good convergence characteristics and gives the better results compared to MFO  
 326 and PSO methods which confirm the effectiveness of proposed algorithm.



1

Figure 1: Fig. 1 :

327

VII.

1 2 3 4 5 6 7 8 9 10

<sup>1</sup>Year 2017 F Optimal Power Flow using a hybrid Particle Swarm Optimizer with Moth Flame Optimizer  
<sup>2</sup>G P = Real power generation at reference bus.© 2017 Global Journals Inc. (US)Global Journal of Researches in Engineering  
<sup>3</sup>© 2017 Global Journals Inc. (US)  
<sup>4</sup>weighting function (w) 0.65© 2017 Global Journals Inc. (US)Global Journal of Researches in Engineering  
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<sup>9</sup>Year 2017 F Optimal Power Flow using a hybrid Particle Swarm Optimizer with Moth Flame Optimizer  
<sup>10</sup>Year 2017 F Optimal Power Flow using a hybrid Particle Swarm Optimizer with Moth Flame Optimizer



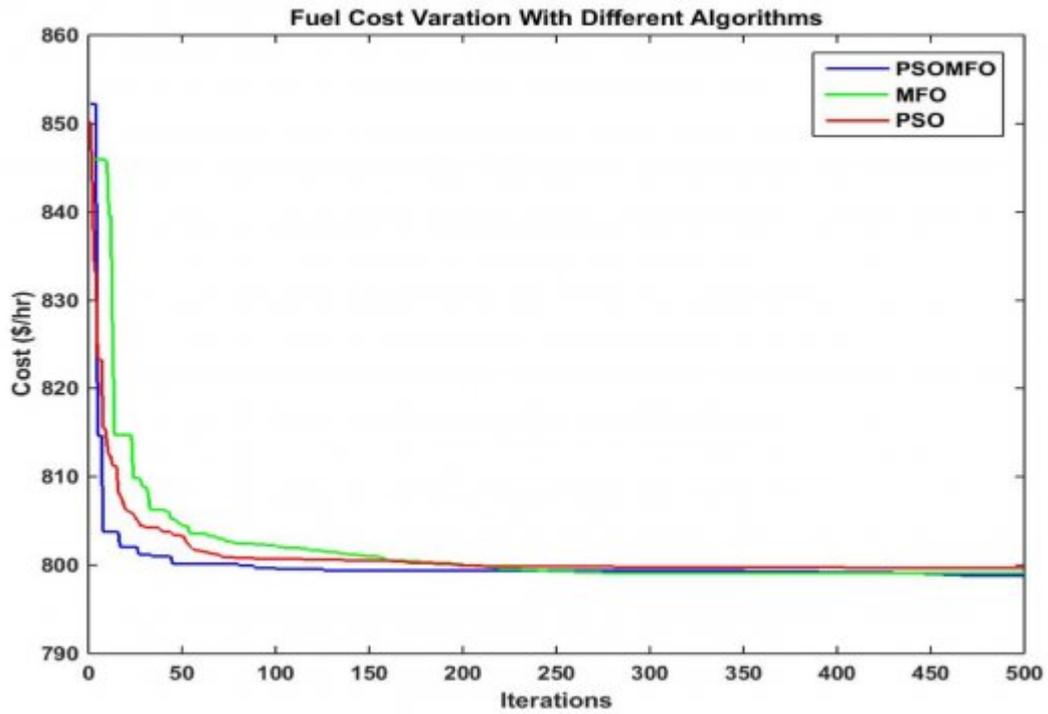


Figure 3: LV=

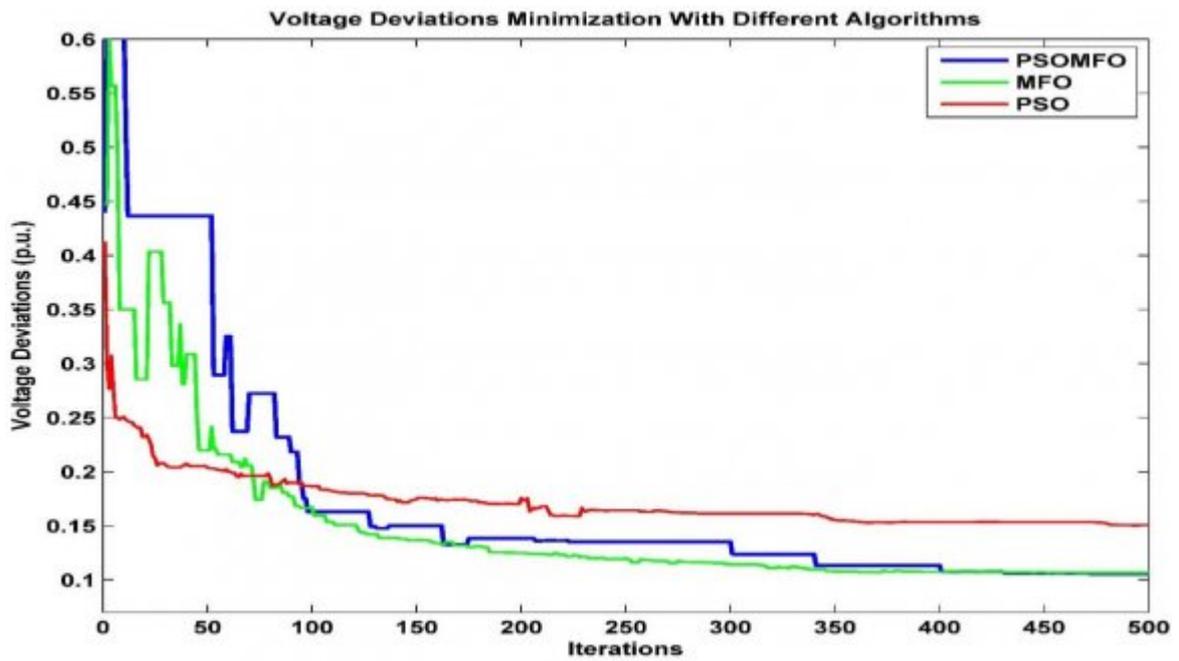


Figure 4: DP

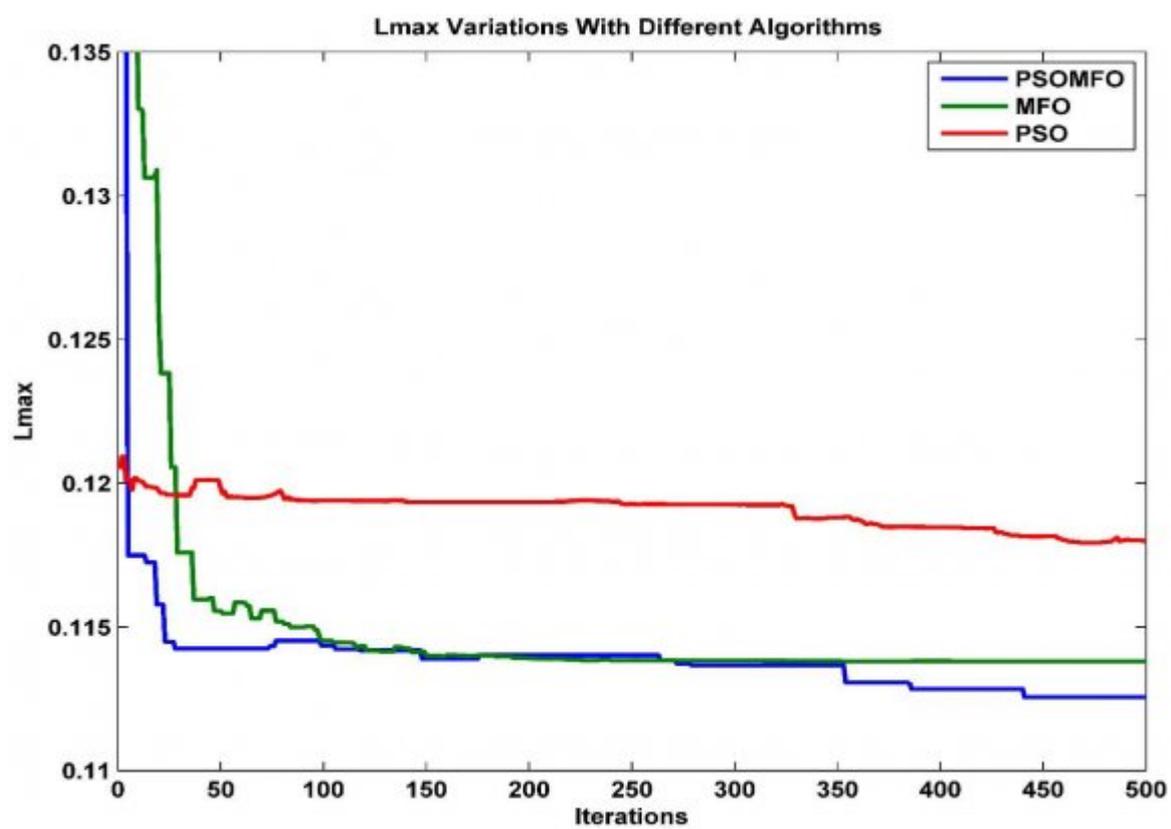
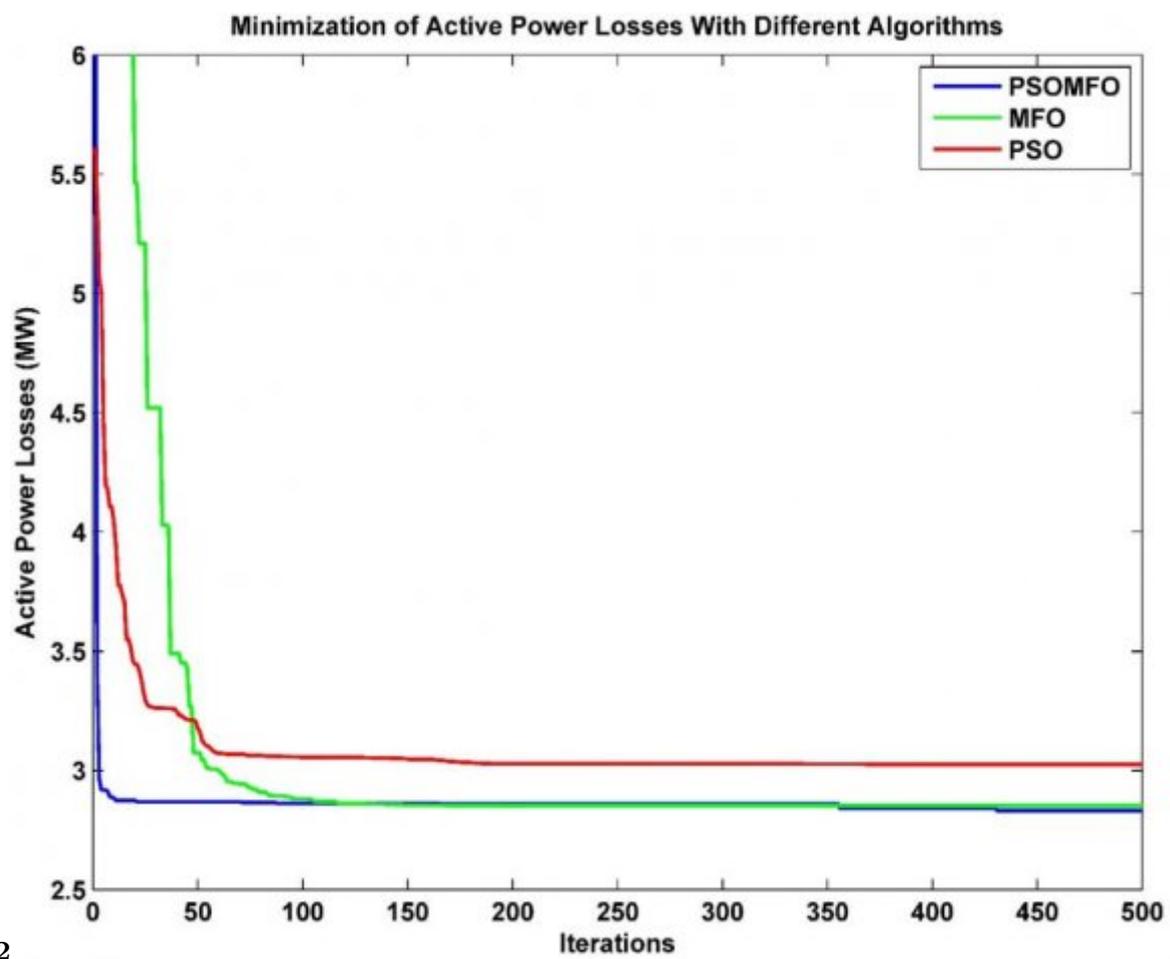


Figure 5:



2

Figure 6: Fig. 2 :

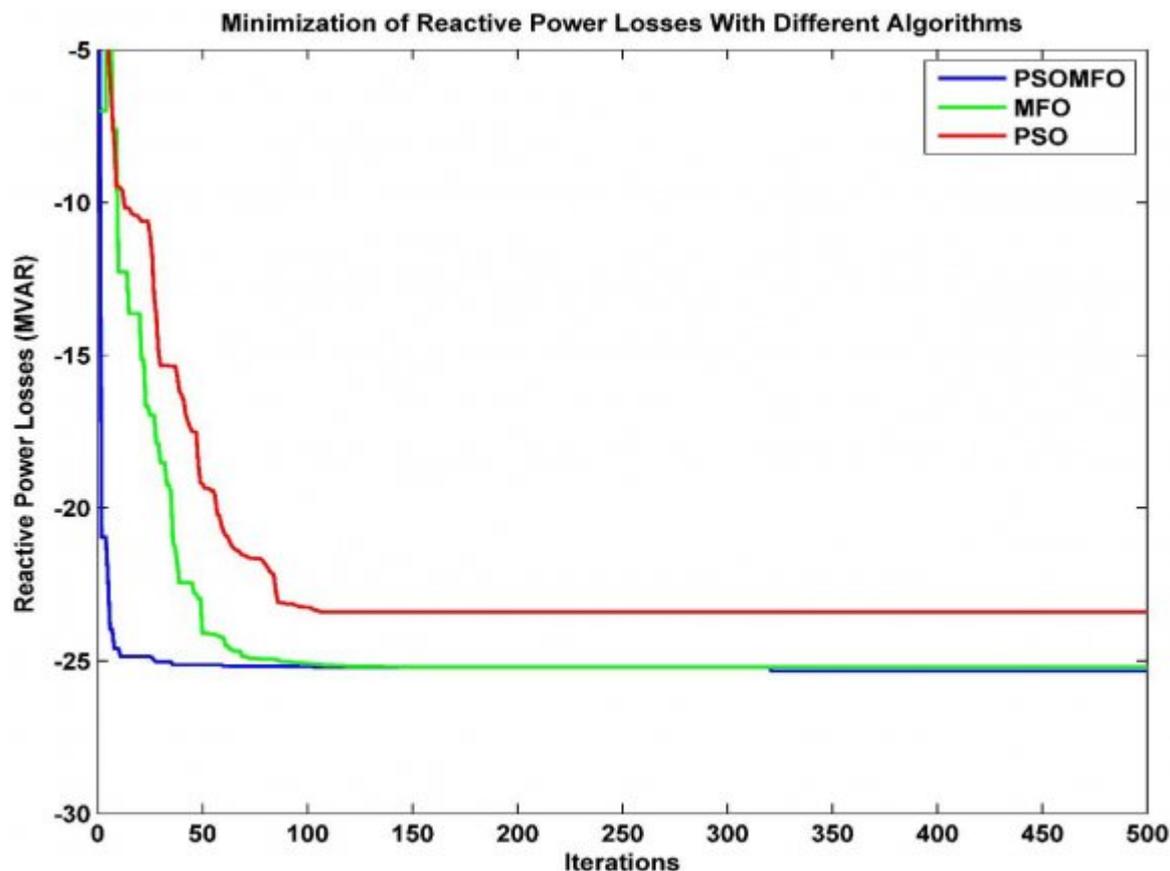


Figure 7: costY

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[Note: penalty factors  $\lim U =$  Boundary value of the state variable  $U$ . If  $U$  is greater than the maximum limit,  $\lim U$  takes the value of this one, if  $U$  is lesser than the]

Figure 8:

1

Sr. No.	Parameters	Value
1	Population (No. of Search agents) (N)	40
2	Maximum iterations count (t)	500
3	No. of Variables (dim)	25
4	Random Number	[0,1]
5	source acceleration coefficient (??_1, ??_2)	2

Figure 9: Table 1 :

2

Method	Fuel Cost (\$/hr)	Method Description
HPSO-MFO	799.056	Hybrid Particle Swarm Optimization-Moth Flame Optimizer
MFO	799.072	Moth Flame Optimizer
PSO	799.704	Particle Swarm Optimization
DE	799.289	Differential Evolution [15]
BHBO	799.921	Black Hole-Based Optimization [6]

Figure 10: Table 2 :

3

Control Variable	Min	Max	Initial	HPSO-MFO	MFO	PSO
P G1	50	200	99.2230	178.133	177.055	177.105
P G2	20	80	80	48.956	48.698	48.748
P G5	15	50	50	21.385	21.304	21.318
P G8	10	35	20	21.706	21.084	20.986
P G11	10	30	20	10.000	11.883	12.049
P G13	12	40	20	12.000	12.000	12.000
V G1	0.95	1.1	1.05	1.100	1.100	1.100
V G2	0.95	1.1	1.04	1.088	1.088	1.088
V G5	0.95	1.1	1.01	1.062	1.062	1.061
V G8	0.95	1.1	1.01	1.070	1.069	1.070
V G11	0.95	1.1	1.05	1.100	1.100	1.100
V G13	0.95	1.1	1.05	1.100	1.100	1.100
T 4-12	0	1.1	1.078	0.939	1.044	0.976
T 6-9	0	1.1	1.069	1.100	0.900	0.975

Figure 11: Table 3 :

4

Method	Voltage Deviation (p.u)	Method Description
HPSO-MFO	0.1056	Hybrid Particle Swarm Optimization-Moth Flame Optimizer
MFO	0.1065	Moth Flame Optimizer
PSO	0.1506	Particle Swarm Optimization
GSA	0.0932	Gravitational Search Algorithm [2]
DE	0.1357	Differential Evolution [15]
BHBO	0.1262	Black Hole-Based Optimization [6]

Figure 12: Table 4 :

5

Control Variable	Min	Max	Initial	HPSO-MFO	MFO	PSO
P G1	50	200	99.2230	177.650	180.212	175.922
P G2	20	80	80	49.092	49.584	46.389
P G5	15	50	50	15.000	15.000	21.597
P G8	10	35	20	10.000	24.349	19.396
P G11	10	30	20	30.000	12.657	17.656
P G13	12	40	20	12.000	12.000	12.000
V G1	0.95	1.1	1.05	1.033	1.033	1.047
V G2	0.95	1.1	1.04	1.017	1.017	1.034
V G5	0.95	1.1	1.01	1.015	1.005	0.999
V G8	0.95	1.1	1.01	0.997	0.999	1.005
V G11	0.95	1.1	1.05	1.047	1.071	0.999
V G13	0.95	1.1	1.05	1.016	1.052	1.018
T 4-12	0	1.1	1.078	1.065	1.100	0.954
T 6-9	0	1.1	1.069	0.914	0.900	0.969
T 6-10	0	1.1	1.032	0.973	1.072	0.989

Figure 13: Table 5 :

6

Method	L max	Method Description
HPSO-MFO	0.1126	Hybrid Particle Swarm Optimization-Moth Flame Optimizer
MFO	0.1138	Moth Flame Optimizer
PSO	0.1180	Particle Swarm Optimization
GSA	0.1162	Gravitational Search Algorithm [2]
DE	0.1219	Differential Evolution [15]
BHBO	0.1167	Black Hole-Based Optimization [6]

Figure 14: Table 6 :

7

Control Variable	Min	Max	Initial	HPSO-MFO	MFO	PSO
P G1	50	200	99.2230	182.308	177.299	158.331
P G2	20	80	80	45.360	48.792	49.050
P G5	15	50	50	21.109	21.316	18.956
P G8	10	35	20	21.557	20.351	31.224
P G11	10	30	20	10.000	12.370	15.906
P G13	12	40	20	12.000	12.012	17.801
V G1	0.95	1.1	1.05	1.100	1.100	1.098

Figure 15: Table 7 :

8

Method	Active Power Loss (MW)	Method Description
HPSO-MFO	2.831	Hybrid Particle Swarm Optimization-Moth Flame Optimizer
MFO	2.853	Moth Flame Optimizer
PSO	3.026	Particle Swarm Optimization
BHBO	3.503	Black Hole-Based Optimization [6]

Figure 16: Table 8 :

9

Control Variable	Min	Max	Initial	HPSO-MFO	MFO	PSO
P G1	50	200	99.2230	51.269	51.253	51.427
P G2	20	80	80	80.000	80.000	80.000
P G5	15	50	50	50.000	50.000	50.000
P G8	10	35	20	35.000	35.000	35.000
P G11	10	30	20	30.000	30.000	30.000
P G13	12	40	20	40.000	40.000	40.000
V G1	0.95	1.1	1.05	1.100	1.100	1.100
V G2	0.95	1.1	1.04	1.100	1.098	1.100
V G5	0.95	1.1	1.01	1.082	1.080	1.083
V G8	0.95	1.1	1.01	1.086	1.087	1.090
V G11	0.95	1.1	1.05	1.100	1.100	1.100
V G13	0.95	1.1	1.05	1.100	1.100	1.100
T 4-12	0	1.1	1.078	1.044	1.056	0.977
T 6-9	0	1.1	1.069	0.901	0.900	1.100
T 6-10	0	1.1	1.032	0.993	0.982	1.100
T 28-27	0	1.1	1.068	0.987	0.973	0.998
QC 10	0	5	0	5.000	5.000	4.065
QC 12	0	5	0	4.570	5.000	0.000
QC 15	0	5	0	4.969	3.070	5.000
QC 17	0	5	0	4.942	5.000	5.000
QC 20	0	5	0	4.337	5.000	0.000
QC 21	0	5	0	5.000	5.000	5.000
QC 23	0	5	0	5.000	5.000	5.000
QC 24	0	5	0	5.000	5.000	0.000
QC 29	0	5	0	2.412	2.508	0.000
PLoss (MW)	-	-	5.8219	2.831	2.853	3.026

Figure 17: Table 9 :

10

Method	Reactive Power Loss (MVAR)	Power	Method Description
HPSO-MFO	-25.335		Hybrid Particle Swarm Optimization-Moth Flame Optimizer
MFO	-25.204		Moth Flame Optimizer
PSO	-23.407		Particle Swarm Optimization
BHBO	-20.152		Black Hole-Based Optimization [6]

Figure 18: Table 10 :

12

Case No.	Elapsed Time (Seconds)		
	MFO	PSO	HPSO-MFO
1	166.2097	250.2674	211.7915
2	191.8238	266.5375	229.6873
3	196.6275	270.3358	243.2919
4	161.6395	248.8739	259.9731
5	173.5987	253.3971	209.4387

Figure 19: Table 12 :

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