

RCD Nuisance Tripping: Who's Guilty and What Needs to be Done?

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Abstract

The reasons for nuisance tripping of residual current devices (RCD) are analyzed in the article and the affect of many external factors is discussed. Solutions are described for avoiding faulty tripping of an RCD.

Index terms— residual current device, RCD, nuisance tripping, harmonic, differential current, leakage current.

1 Introduction

esidual current devices (RCD) are widely used all over the world in households and commercial enterprises as an additional protection against electric shock (RCD with differential tripping currents of up to 30 mA [1, 2]) and as protection from fire, which can result from temperature increases due to current flowing through broken cable insulation and other types of equipment (RCD with tripping currents from 100 to 300 mA [3, 4]).

Since RCD are used so widely, information about their nuisance tripping is in the public domain. It's one thing if power outage occurs in an apartment in a house; this can be easily fixed, by returning the RCD to its initial position. But it's absolutely a different thing if this outage occurs when complex commercial electronic equipment, computers, servers, etc are working. The losses in this case can be tremendous; and these losses can be not only material. Paragraph 7.1.81 of the Operational Codes for Electric Installations (OCEI-7) clearly prohibits installation of RCDs for electric consumers the disconnection of which can result in situations dangerous for consumers (disconnection of fire alarms, and the like). However, it is not always easy to predict the consequences of the disconnection of specific electric receivers wired through an RCD (such as computers, controlling a technological process, special communication devices and alarms, etc.). This is why the problem of nuisance tripping of RCD is very relevant. This topic is discussed in multiple articles found in special technical references [5 -10], it is even mentioned in catalogues of large RCD manufacturers, such as ABB, Siemens, Schneider Electric, Merlin Gerin, Legrand, Eaton, Mueller and others.

Standards [11, 12] describe two major types of an RCD, i.e., B and A. While standard [13] mentions two additional types, i.e., and F. All of them differ in terms of current flowing through the RCD. For example, the AC type RCD is designed for sinusoidal alternating

Author : E-mail : vladimir.gurevich@gmx.net current only; the A type is designed for alternating sinusoidal current and rectifying current imposed to it; the B type is designed for alternating sinusoidal current with a frequency up to 1000 Hz and pulsing, direct or rectified smoothed current; and the F type ("F" stands for frequency) is designed for alternating sinusoidal or pulsing current as well as for non-sinusoidal current, which contains harmonics generated by frequency converters. Many additional types have been "invented" by manufacturers with the purpose of reducing nuisance tripping problems, such as, types U, K, AP-R, SI and others, which are not mentioned in standards. RCD can also be divided into general use devices (type Ggeneral) and selective devices (S-selective). The latter have increased differential trip currents and are equipped with trip delays. They are used in branched cascade networks.

Despite the availability of multiple types of RCDs in the market, the problem of nuisance tripping is still relevant.

2 II.

3 Analysis of Reason for RCD Nuisance Tripping

Let's make it clear from the start: we will not be discussing faulty tripping of RCD as a result of RCD's failures. Rather we will be discussing only nuisance tripping of fully functional RCDs. The reader may ask: Why? If an RCD is fully functional and meets all the requirements set for it, how can it be tripped falsely? The issue is about specific conditions and operational modes which may occur in electric mains as well as those parameters of these mains and modes of operation of electric energy consumers. Due to the high sensitivity of the RCD, the operational modes of the main and consumers characteristics powered through the RCD have a direct impact on the device and often result in its faulty actuation. a) Natural («background») leakage current to the ground through intact insulation of cables and electric loads

It is known that RCD responds to the so-called differential current, which is a difference between the phase current (or a sum of the phase currents in a 3-power network) and current in the neutral. If the current flows to a load through an RCD via a phase wire and returns to the RCD through a neutral wire, the differential current for which the RCD is set up will R XIII Issue XI Version I

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Year amount to zero. If part of the phase current that flows through the RCD is "leaked" to the ground through faulty insulation and does not return to the RCD through a neutral wire, a difference of currents will occur (differential current) to which the RCD responds. The distributed capacities related to ground wires, capacities between coils of transformers and motors related to grounded housings, capacities of multiple filters installed in the supply circuits of almost all types of electronic equipment are the ways through which current may "leak" to the ground. This is actually the current to which an intact RCD should react. According to the standards [14,15] the RCD's trip current may fall in the range of $0.5I_N - I_N$. This means that a functional RCD with a nominal differential tripping current of 30 mA (maximum permitted current to protect people from electric shock) can be tripped at 50% of the nominal current, i.e., at 15 mA. For RCD types " " and " " the real trip current depends also on the pulsing component phase shift and according to standards [11, 12, 14] it falls into the range $0.1I_N - 2 I_N$.

5 b) Distortion of current form in the RCD circuit

The quality of electric power in household and commercial mains tends to deteriorate continuously due to expanding application of non-linear loads, such as powerful voltage regulators, frequency converters, UPS, LED light fixtures, computers, servers, controllers and other low power electronic devices with internal impulse mode power supply that consume non-sinusoidal current from the mains. This distorted current, containing a number of high-frequency harmonics, will flow through RCD as well, see Fig. 1, Table 1.

Past research [5-10] has shown that distorted current flowing through RCDs of electro-magnetic type leads to significant changes in the threshold of its tripping. The effect of high frequency harmonics on the condition of the magnetic core of the internal current transformer of the RCD and its other elements is rather complicated and controversial. In some cases it is possible to speak of the danger of RCD malfunction, whereas in other cases -about reduction of tripping threshold, i.e., the increase of probability of faulty actuations. But high frequency harmonics not only change the RCD's tripping threshold, but also increase the total "background" leakage current through capacities of the mains and consumers. This is why we can find XIII Issue XI Version I

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Year ourselves in a situation when even a specially selected RCD, which can work with distorted currents, may still be tripped erroneously.

7 c) Impact of current impulses in the RCD circuit

Besides harmonics, electric networks of private dwellings and especially networks of commercial enterprises are affected by atmospheric and switching overvoltages. These overvoltages are "cut" by various types of protection elements, such as gas arrestors, voltage-dependent non-linear resistors (varistors) and specific non-linear semiconductor elements. These protection elements are installed directly in the network as separate elements and they are part of internal power supplies of all modern electronic devices. Short (parts of milliseconds) impulses of rather high current (hundreds of Amps) occur when these devices are actuated due to overvoltages and current flow between phase and ground as well as between neutral and ground. In any case this current is actually the differential current to which RCD should react.

As a rule, internal power supplies of electronic devices [16] contain input network filters, which include capacitors as their main elements and which are connected between the phase and the ground as well as between neutral and the ground. When the power supply is switched on, these capacitors produce the current surge between phase and ground to which RCD should react. In addition it should react when the working impulse power supply (this is the main power supply for all modern electronic devices) consumes current from the network

101 in pulses [16]. The crest factor, in other words, is the ratio of peak value to the RMS. Current value, consumed
102 by the load, amounts to 3, while it is 1.41 for a usual sinusoidal signal. This creates additional load for an RCD.

103 8 d) The effect of the direct current level on RCD performance

104 Unlike the above situation (see 2.2) with nonsinusoidal current flowing through an RCD, the expansion of
105 powerful electronic devices (with their frequency converters, voltage regulators, invertors, powerful convertors
106 and variable frequency electric drives) constitute conditions whereby high frequency sinusoidal current of pulse-
107 width modulation and direct or rectified pulsing current flow through RCD connected to circuits with such
108 devices. Normally RCDs of AC, A and even F types are not designed to work in circuits with this current. Since
109 the input element of any RCD is represented by a current transformer with a ferromagnetic core (see Fig. 2), it
110 is obvious that the characteristics of such a transformer will largely depend on the availability of direct current
111 level in the current. In other words the moment when the RCD is actuated will not be determined by its nominal
112 value of differential current, but by random fluctuations of load and leakage current. contact system's release
113 pusher However, even if we select a type B RCD for these purposes, but do not take special measures, type B
114 devices will also be affected by faulty actuations due to the influence of significant impulse current or background
115 leakage current just like RCDs of other types.

116 9 III.

117 What Needs to be Done? In the absence of actual (measured) values of the leakage current, the OCEI (7.1.83)
118 suggests accepting the leakage current for electric consumers based on 0.4 mA for each 1 A of the load current
119 and for wires based on 10 microampere for 1 meter of length of a phase conductor. As an example standard
120 [15] provides typical values of leakage current for several types of electric equipment, see Table 2.

121 This means that one RCD can be connected to 4-5 computers and 1 printer located within several dozens of
122 meters from the switchboard where the RCD is installed. How can we measure the real current of RCD actuation
123 and the real background leakage current flowing through it? There are special devices for this; however, qualified
124 personnel of commercial enterprises and companies can measure this current with a simple device, Figure 3,
125 observing safety requirements. Initially, the RCD trip current is measured (by gradual reduction of resistance of
126 R resistor) while the load is switched off. Then, the same measurement is performed with the load switched on.
127 The difference in measurements will be the sought-for value of the background leakage current. If this value is
128 higher than 10mA, then according to recommendations [15] the loads should be split, i.e., install an additional
129 RCD and split the loads between two of them. This cascade connection of RCD allows elimination of their faulty
130 actuation in a complex network. However, it should be considered that RCD with a trip current above 30 mA
131 cannot be viewed as a reliable protection of people from electric shock. This means that the significant portion of
132 the upstream network does not protect people from electric shock and the RCD is used as a fire protection only.
133 On the other hand, it does not mean that a low power consumer connected through an ordinary plug somewhere
134 upstream cannot be protected by a separate RCD with an actuation current of 30 mA. In this situation the
135 leakage current from all downstream cascades will not flow through this RCD and its faulty actuations can be
136 successfully avoided providing reliable performance without nuisance tripping.

137 In some types of RCD marketed as "super resistant" to nuisance tripping this "resistance" is ensured due
138 to the increase of the minimum level of differential trip current from 0.5 I_N, which is actually not prohibited
139 by standards, to 0.75 - 0.8 I_N. Prevention of the affect of higher harmonics on the RCD is the second option
140 to increase the RCD's resistance to nuisance tripping. It is clear that an RCD designed to work with current
141 containing higher harmonics will behave more predictably compared with devices, which are not intended to
142 work with high frequency current. In fact, this is the reason why special types of RCD (B and F) including
143 special filters and limiting the effect of harmonics were developed. RCD of type F are not manufactured as
144 separate devices, they are manufactured as a type A RCD with expanded frequency characteristics. This is why
145 the marking of this type of RCD usually bears two letters: AF or A-F.

146 Figure ?? : Incorrect (left) and correct (right) connection of non-linear load with special type RCD In the
147 case of non-linear loads present in a network, which condition increases the level of high frequency harmonics
148 and loads, and containing direct components, these loads should be separated from the common network in such
149 a way so that the non-linear current and current containing the direct component do not flow through another
150 RCD, Fig. ??., which will prevent their nuisance tripping.

151 It should be taken into consideration that the increased level of high frequency harmonics in the voltage leads
152 to increase of leakages through capacities of wires and equipment, i.e., the increase of the background current thus
153 making the use of special type RCD inefficient. The increased level of harmonics leads to an increase of voltage
154 drops on elements connected in series (inductance chokes) built into the electronic equipment of network filters.
155 This can result in the increase of high frequency voltage level and leakages to the ground through capacitors of
156 these filters. At the same time past research suggests that electronic RCDs are less sensitive to harmonics than
157 electromechanical RCDs, which may be strange at first sight. This is due to the fact that in an electronic RCD
158 the controlled current containing harmonics is not used directly for actuation of the RCD trip unit, but is only a
159 source of a controlling signal, which is cleared from harmonics, strengthened and converted. In order to influence
160 the RCD trip unit, the energy of an auxiliary power supply is used. Phase voltage of the power network can be

161 used as such a supply. An example of an electronic RCD (designated as U-type) is a device manufactured by
162 Eaton-Moeller company under the brand dRCM-40/4/003-U+.

163 Unfortunately, the use of an electronic RCD (in the standards they are referred to as RCD with dependant
164 power supply, i.e., requiring an auxiliary power supply) is not that simple. The problem is that when the
165 contact in the neutral wire is broken, the RCD will lose its power supply and stop functioning, whereas an
166 electromechanical RCD will actuate and disconnect a consumer due to current imbalance. Due to this, a lot of
167 manufacturers started producing RCDs with a built-in element, which ensures its actuation and disconnection
168 load in the case that the neutral wire is broken (in other words, when the RCD loses its power supply). In their
169 opinion this algorithm was supposed to eliminate an obstacle in the way of using electronic RCDs. However,
170 paragraph 7.1.77 of OCEI-7 prohibits using this RCD, which disconnects a consumer from the mains in the event
171 of voltage outage or voltage dips in inhabited buildings. Why? The author has no reply to this question. And
172 perhaps, not only the author, since V.A. Bulat, Doctor of Science, says the following in his recommendations
173 regarding selection of a correct RCD [17]: XIII Issue XI Version I

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175 Year «Among electronic RCD or differential automatic circuit breakers t the preference should be given to those
176 that have protection from disconnection of neutral conductor -the disconnection can lead to loss of input voltage
177 by RCD which makes them non operable».

178 In some European countries the use of electronic RCDs with dependent power supply in stationary electric
179 mains is not allowed by national standards. French standard NFC 15-100 (§ 531.2.2.2) specifies that they
180 should not be used in electric installations of residential buildings. In Russia the concept that an electronic RCD
181 should not be used to protect people from electric shock was shuffled from one scientific article to another for
182 a long time. It is interesting that there was one quote (about the danger of disconnection of zero wire), that
183 was copied by many authors word by word. However, paragraph .4.14 of the new edition [18] expressly says:
184 «RCD dependant from auxiliary power supply (electronic) and independent (electromechanical) can be used in
185 residential installations as shock hazard protection».

186 There are no restrictions for RCD use in the new edition of OCEI-7 also.

187 The international standard [19] allows using electronic RCDs in two situations:

188 When using an RCD as protection from indirect contact; When using an RCD in network and electric appliances
189 services by qualified personnel. Direct contact means a contact of a person with current conducting parts inside
190 an electric appliance, while indirect contact means a contact of a person with a casing or another part of an
191 electric appliance, which are normally insulated and are under voltage only due to insulation breakage, Fig. 6.
192 It is clear that the probability of RCD working in the latter case is much lower than in the former case, this is
193 why the standard allows using electronic RCD in this case. An example of this special filter is Filter FN3268
194 produced by the Swiss company Schaffner [20]. These filters are intended for nominal load currents of 7, 16, 30,
195 42, 55, 75 Amps for RCDs with a differential current of 30 m and for currents 100, 130, 180 Amps for RCD with
196 differential current of 300mA. They not only prevent the influence of high frequency harmonics on the change
197 of the RCD trip threshold, but also reduce background leakage current, since their own leakage current is much
198 less than the current leaking through capacities of the mains due to high frequency harmonics. This is the reason
199 why these filters can be more efficient in preventing nuisance tripping of RCD than the use of special types RCD.

200 11 c) Prevention of current pulses effect on RCD performance

201 Actually, today it is not a problem to separate short (several milliseconds) current impulses by means of electronic
202 circuits and block the effect of these short impulses. But when talking about very small and affordable devices
203 (RCD) including those of electromechanical type, the only way to protect from such impulses is to use time lag
204 so that impulses with durations less than this time lag could not activate RCD.

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208 According to standards [11, 22], based on actuation time, RCD are distinguished G (general) and S (selective)
209 types. In fact, RCD do not have strict and constant times of actuation. They possess a typical reverse time-
210 to-current feature: the higher is the differential current, the less is the time lag to disconnect the protected
211 circuit, Table 3. In technical literature [21] we come across erroneous interpretations of RCD actuation time
212 and references to three instead of two types of devices, such as immediate action (without time delay), with a
213 little delay (type G) and with increased delay (type S), Table 4.

214 In fact, according to the standards there is no immediate action type device at all. Indeed, for type G RCDs
215 unlike type S the minimum actuation time (in the IEC standard it is called minimum time of non-operation) is
216 not standardized. In other words, theoretically it can be as small as desired.

217 Clearly this very small time of the general type RCD (type G) actuation does not improve its resistance to
218 nuisance tripping, but on the other hand type S RCD are not suitable as human protection devices. Rather, type S
219 are used to ensure selectivity in the upstream cascades of branched electric networks and have minimum actuation
220 currents of 100 -300 mA. This is why many manufacturers produce special type RCDs for differential current of
221 30 mA (i.e., intended to protect people) with a minimal standardized actuation time of 10 msec (this means they
222 should not be actuated even at current impulses of large amplitude and lasting less than 10 msec). Such RCDs
223 are classified as especially resistant to faulty actuation and are marked according to the manufacturer's wish.
224 For example, Siemens marks this RCD as type "K", while the ABB company marks them as «AP-R».

225 15 d) Elimination of direct component effect on RDC perfor- 226 mance

227 To eliminate the effect of a direct component on RCD performance in a network, where the occurrence of this
228 component (and also high frequency sinusoidal current) is possible, the special type B RCDs are used, which
229 have a differential transformer manufactured using special technology. Very small power taken off from such
230 differential transformers makes it difficult to use electromechanical RCDs, which uses this power for relocation
231 of the trip unit. This is why the majority of RCD manufacturers either do not manufacture type
232 B devices at all, or manufacture them in the electronic variant instead of electromechanical. The standard [13]
233 determines the upper limit of the sinusoidal current frequency for which in addition to XIII Issue XI Version I
234 37 () Year e) Correct selection of RCD type is a key to successful prevention of nuisance tripping

235 In real conditions of operation there can be a situation when a certain separate fully intact RCD device working
236 in a group of other RCDs of the same type and installed in the same switchboard will have a trip current rating
237 in the network with similar consumers, which is two times less than the nominal rating (which is accepted by the
238 standards). In situations such as this in the event of the occurrence of some detrimental factors (e.g., harmonics,
239 current impulse, results from impulse overloading and arrester actuation, background leakage current), which do
240 not result in tripping of other RCDs, this unit can be actuated erroneously. Moreover, if the effect of detrimental
241 factors repeats, nuisance tripping of this RCD installed in a group of other RCDs can also repeat itself. To
242 prevent such situations sometimes it is enough to substitute this RCD unit by the similar RCD of the same type,
243 but with actuation current rating higher than that of the RCD which actuated erroneously.

244 In some cases nuisance tripping happens because of accidental combination of events, each of which separately
245 would not result in the faulty actuation of RCD. For example, if there is a certain constant level of harmonics
246 in the circuit, which does not lead to RCD tripping and at the same time there is a powerful current impulse
247 (which alone does not cause actuation), the RCD can be tripped and a consumer will be disconnected. Even
248 such sophisticated and universal units as type B RCD can be susceptible to faulty actuation due to the effect of
249 significant impulse current or background leakage current.

250 To ensure reliable power supply to consumers and prevention of accidental nuisance tripping of RCD in a
251 network with low power quality, the units should be selected in advance (during design stage) and possess a
252 special feature which ensures protection from harmonics, impulse current and background leakage current effect.
253 If low quality of power was not anticipated before and appeared to be low in practice or deteriorated because of
254 substitution (addition) of consumers, the usual RCDs that were installed before (,) should be substituted by
255 special type RCDs (F, B, U, K). Electronic RCDs are more diversified both in terms of design and in terms of
256 functionality, but they have specific restrictions in use, which have been mentioned above.

257 A search for devices, which would satisfy all these requirements among dozens of RCD types manufactured
258 by many companies, returned the following results, Table 5. As a rule, RCDs of the same type and possessing
259 similar parameters are manufactured for nominal currents of 25, 40, 63 in twopole (for single phase mains) and
260 four-pole (for 3-phase mains) designs. In order to save space, Table 4 shows parameters of RCD with nominal
261 current of 40A in a four-pole design only.

262 I regret to say that even the latest version of the main standard on RCD [??11] does not interpret RCD
263 classification accurately in terms of resistance to faulty actuations. For example, according to [??11] the devices
264 with a standard resistance to faulty actuation are type G (general) devices, whereas devices with increased
265 resistance to faulty actuation are type S (selective) devices. It is obvious that type S devices intended for
266 differential current in the range of 100-300 mA and higher will be more resistant to faulty actuations compared
267 with type G devices with actuation currents of 10 -30 mA. But as was mentioned above, type S units cannot
268 be used to protect people from electric shock. This means that according to [??11] there is no RCD resistant to
269 faulty actuation intended to protect people from electric shock at all. It seems that the authors of the major
270 international standard on RCD are comfortable with this situation, since this concept has been there for a long
271 time and is copied from one edition of the standard to another. However, the data presented in Table 5 show
272 inconsistency of the classification offered by the standard. f) Automatic reclosing of RCD as an additional option
273 to improve reliability of power supply to consumers

274 The automatic reclosing (AR) of an RCD cannot be called a means of preventing faulty actuation. It is rather
275 a way to correct the results of nuisance tripping. However, an RCD with AR can be very efficient in solving the
276 problem in those cases, when consumers accept short-time power supply failures. The AR function is easier to
277 implement in some types of electronic RCDs. To return to the initial state an electromechanical RCD needs a

15 D) ELIMINATION OF DIRECT COMPONENT EFFECT ON RDC PERFORMANCE

278 special motor drive, which of course requires a separate auxiliary power supply. Some companies produce AR
279 devices as separate blocks, which are installed close to RCDs of different types and reclosing them after tripping
in the initial state by simulating the action of a person's hand by means of special protruding plastic lever.



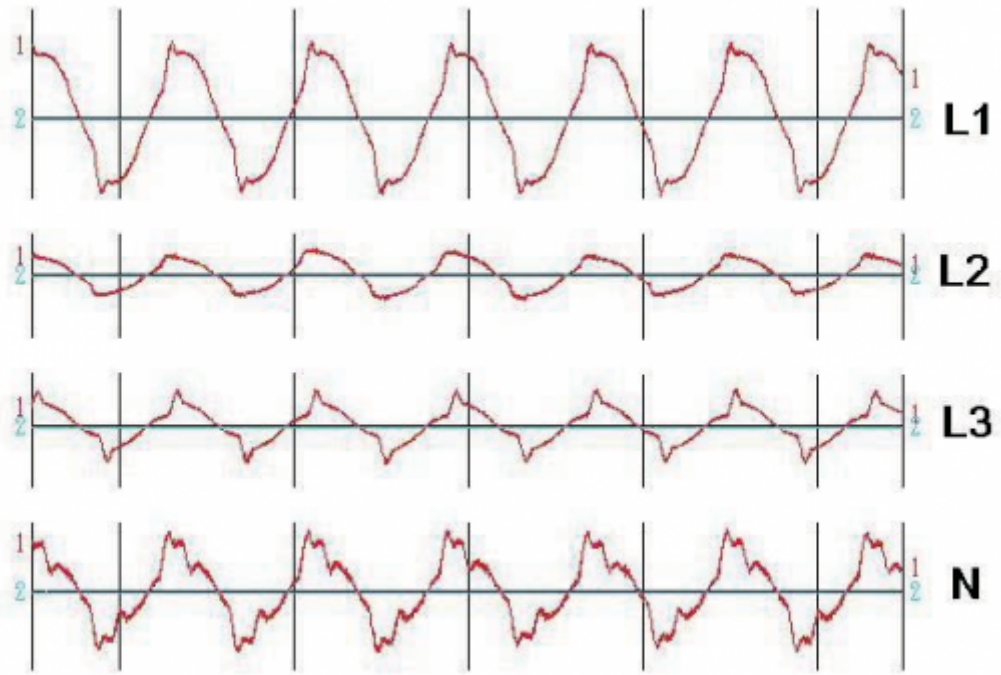
Figure 1: Figure 1 :

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²© 2013 Global Journals Inc. (US) Volume direct, pulsing and alternating current the type B RCD should be employed at 1000 Hz. A lot of manufacturers of this type of device guarantee their operation at frequencies of up to 2000 Hz, whereas for type "B+" devices -up to 20 kHz. Type B RCD is the most universal of all other types of RCDs, but is also the most expensive.RCD Nuisance Tripping: Who's Guilty and what needs to be Done?



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Figure 2: Figure 2 :

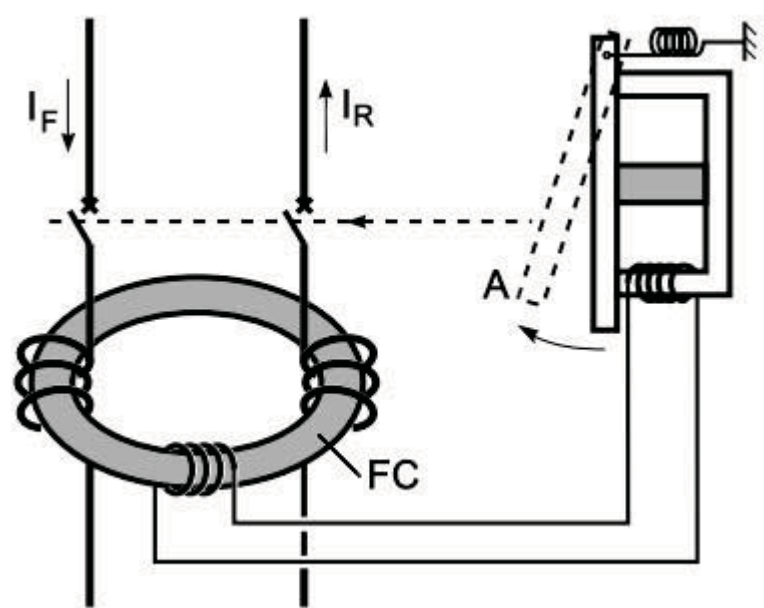


Figure 3:

15 D) ELIMINATION OF DIRECT COMPONENT EFFECT ON RDC PERFORMANCE

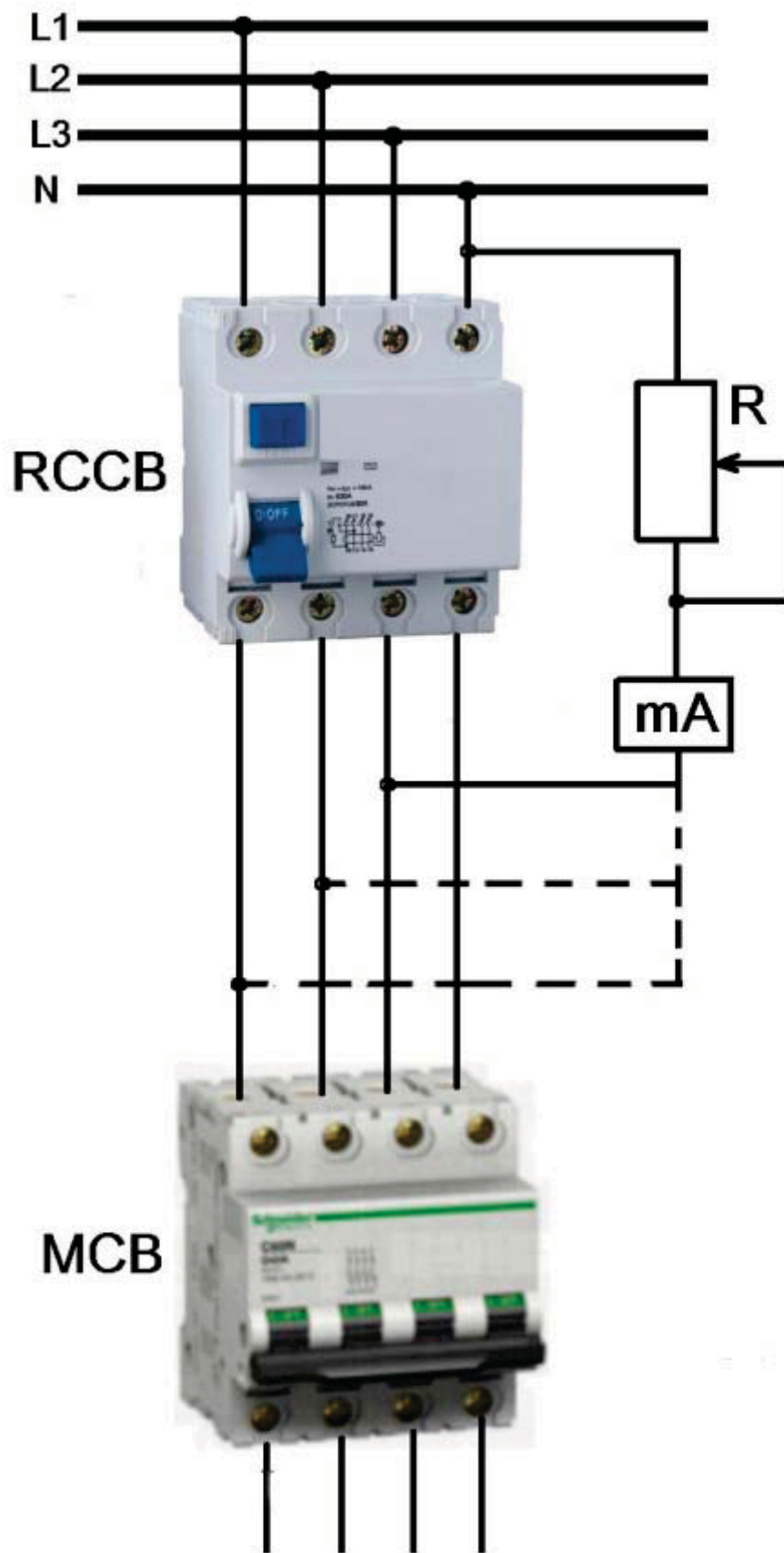


Figure 4: Figure 3 :

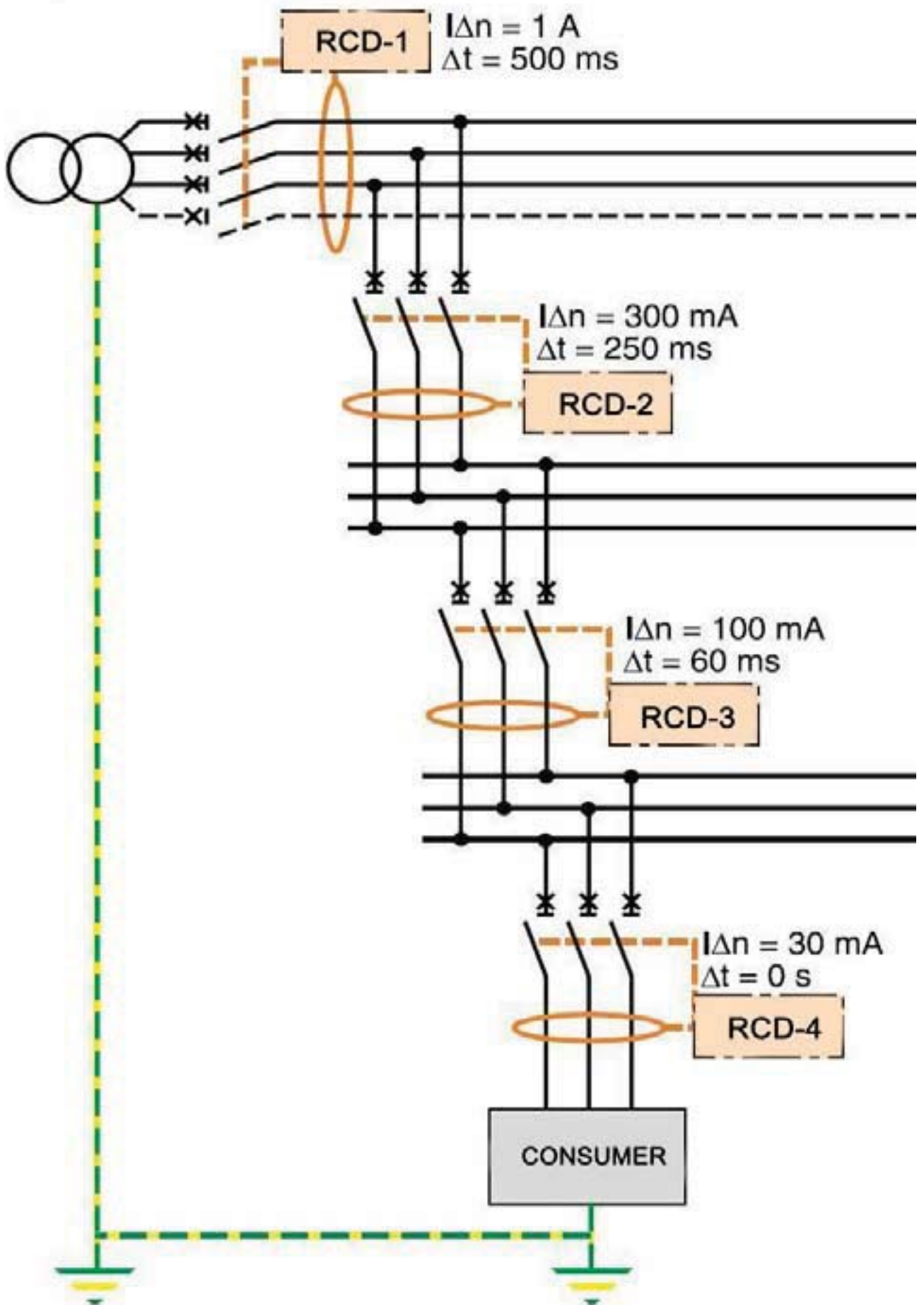
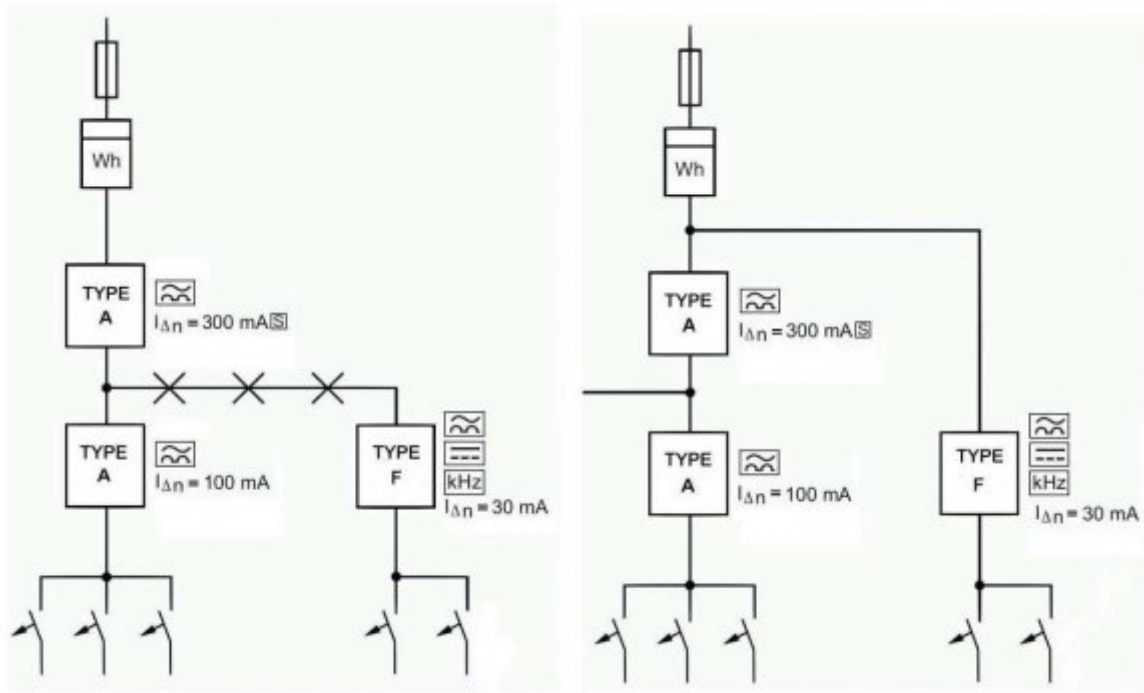


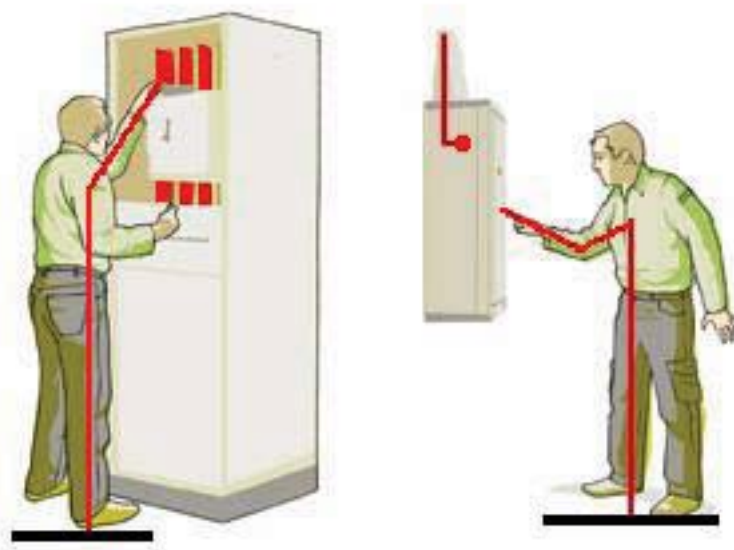
Figure 5: Figure 4 :

15 D) ELIMINATION OF DIRECT COMPONENT EFFECT ON RDC PERFORMANCE



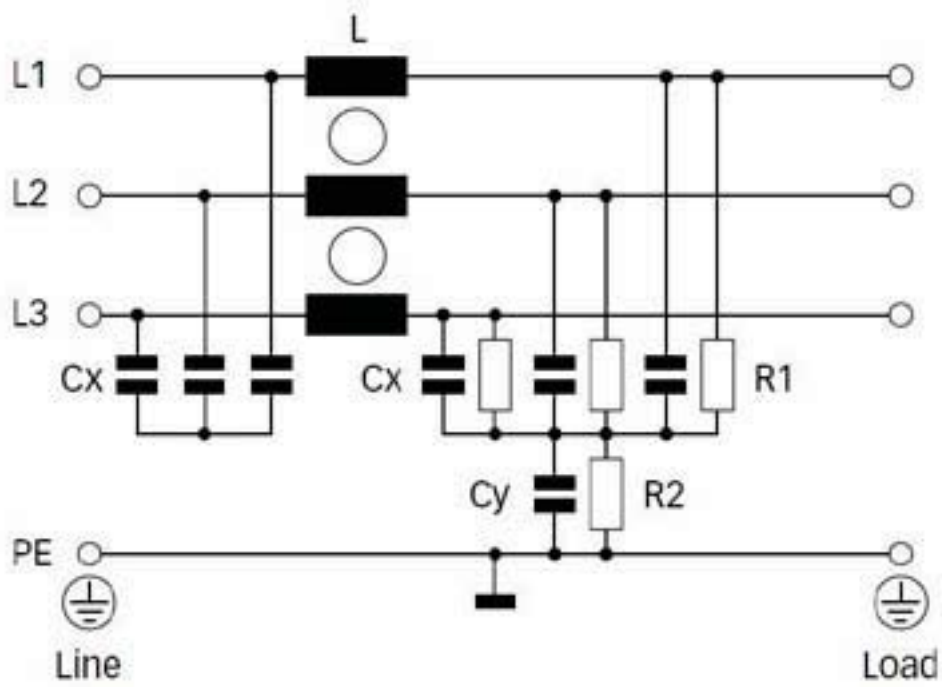
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Figure 6: Figure 6 :



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Figure 7: Figure 7 :



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Figure 8: Figure 8 :

15 D) ELIMINATION OF DIRECT COMPONENT EFFECT ON RDC PERFORMANCE

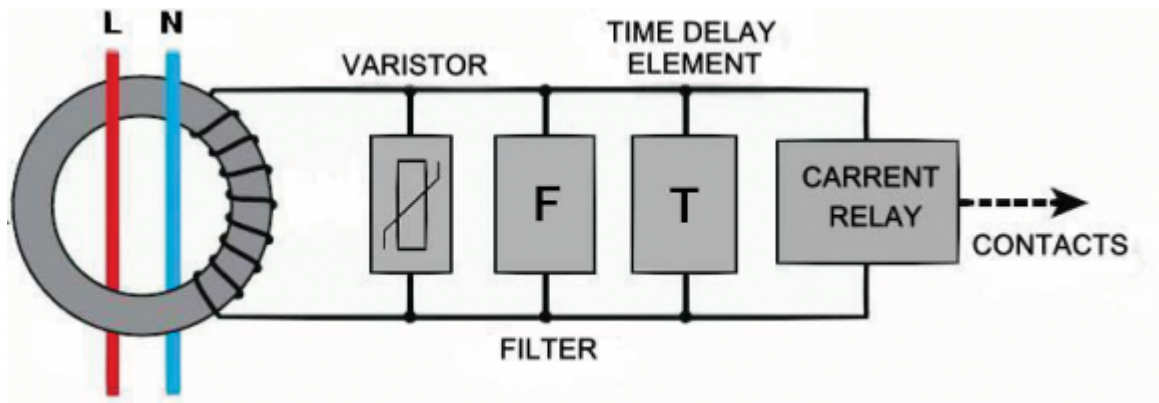


Figure 9:



Figure 10:

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Harmonic's number	L1	Contents of each harmonic in % L3 L2		N
1	100	100	100	100
2	1	0.9	3	1.3
3	14.6	23.7	46.3	58.2
4	0.9	0.9	2.5	1.3
5	22.5	17.3	45.2	26.8
6	0.8	3.2	2.6	4
7	15.2	10.8	34.6	21
THD, %	34.5	33	80	78

Figure 11: Table 1 :

2

electric equipment Electrical appliances kind	Typical leakage current, m
Computers	1 -2
Printers	0.5 -1
Portable domestic electrical appliances	0.5 -0.75
Photocopy machines	0.5 -1.5
Filters	~1.0

Figure 12: Table 2 :

3

rates of differential current according to IEC 61008-1

standard (Table 1)

RCD trip time at variable values of differential
currents I DIFF (rms.), ms

RCD type	RCD trip time at variable values of differential currents I DIFF (rms.), ms						
	Min	Max	2 I DIFF Min	Max	5 I DIFF Min	Max	
G	-	300	-	150	-	40	
S	130	500	60	200	50	150	

Figure 13: Table 3 :

4

RCD type	I = I _n	Time delay, ms at		
		I = 2I _n	I = 5I _n	I = 500 mA
- Common use, without time delay With minimal time delay 10 ms Selective, with minimal time delay 40 ms	<0.3	<0.15	<0.04	<0.04
G	0.01?0.3	0.01?0.15	0.01?0.04	0.01?0.04
S	0.13?0.5	0.06?0.2	0.05?0.15	0.04?0.15

Figure 14: Table 4 :

15 D) ELIMINATION OF DIRECT COMPONENT EFFECT ON RDC PERFORMANCE

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No.	RCD type and manufacturer	Type	Nominal Trip current, I _N		Drive type	Time	
			current, I _N			delay, ms (at I=I _N)	Pole number
1	dRCM-40/4/003-U+ Cat. number 120850 Eaton (Moeller)	U	40	30	electronic	10	4
2	F374-40/0.03 ABB	A- F	40	30	electro- mechanical	10	4
3	F204 A-40/0.03 ABB	AP- R	40	30	electro- mechanical	10	4

Figure 15: Table 5 :

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 21. . - . , . ()
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[Note: RCD]

Figure 16:

282 The ABB Company also supplements their AR devices with a small transformer installed on a DIN-rail close
283 to the RCD, which provides power to AR unit's drive from the supply mains. Some types of various AR devices
284 are shown in Fig. ??.

285 The majority of types of AR devices allow the RCD to return into its initial condition electively: automatically
286 with a small time lag or, remotely, on command. These devices are manufactured by ABB, Schneider Electric,
287 Legrand, Hager, Circutor, Aoelec and others.

288 .1 References Références Referencias